



# Drainage Strategy

22&24 St. Annes Road, London Colney, AL2 1LJ

Reference: 497 -Rev - V1

Date: jun-24

- 1 Introduction
- 2 Site Characteristics
- 3 Discharge Arrangement
- 4 Peak Runoff
- 5 Proposed Sustainable Drainage
- 6 Maintenance and Management Plan

## Appendices

- A Distribution Existing and Proposed Areas
- B Site Characteristics
- C Drainage Calculations
- D Drainage System General Arrangement

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## **Purpose of this report**

- 1.1 The purpose of this statement is to accompany the technical drawings and details showing the proposed Surface Water drainage system as part of the planning application for this development.

## Site Characteristics

- 2.1 The site background is clearly identified through answers to the questions in table 1 below.

Table 1: Site Characteristics . See appendix B for support documentation

TOPIC	QUESTION	ANSWER
<b>Protected species or habitat</b>	Is the site near to designated sites and priority habitats?	No
<b>Flood Plain</b>	Is the site located in the flood plain?	Yes
<b>Soils and Geology</b>	Soil permeability? - See appendix B for results	No
<b>Space constraints</b>	Space for SuDS components?	Yes
<b>Topography</b>	Sited on a flat site?	No
	Sited on a steep slope (5-15%)	Yes
	Sited on a very steep slope (>15%)	No
<b>Groundwater</b>	Is the site at groundwater flood risk?	No
<b>Contaminated land</b>	Are there contaminated soils on site?	Unknown
<b>Source Protection Zone</b>	Is the site within a SPZ 3?	Yes
<b>Runoff characteristics</b>	Is the development in a high risk flooding area?	No

## Existing and Proposed Site

- 2.2 The distribution of catchment areas for existing and proposed site is as per table 2 below. See appendix A for details

Table 2 : Existing and Proposed catchment areas in hectares

Description	Existing Site	Proposed Site
Impermeable Areas	0.030	0.039
Permeable Areas	Connected to Drainage	0.000
	Self Draining Areas	0.025
Areas Draining Away from drainage System	0.065	0.046
<b>Total Development Area</b>	<b>0.120</b>	<b>0.120</b>

- 2.3 It has been assumed that the positively drained areas will have different runoff coefficients depending on the type of surface as follow:

Impermeable Surface	1.0
Permeable Surfaces	0.5
Grass Areas	0.3

## Evaluation of Discharge Point

3.1 The SuDS design takes into account Building Regulations Section H3 and the National Planning Practice Guidance. The aim is to discharge surface water run-off as high up the drainage hierarchy, as reasonably practicable:

1. into the ground (infiltration);
2. to a surface water body;
3. to a surface water sewer, highway drain, or another drainage system;
4. to a combined sewer.

3.2 The discharge point has been evaluated following the NPPG and Building regulations. The findings are in table 3 below.

Table 3: Drainage Hierarchy evaluation

Superficial geology classification	The British Geological Society records show that the superficial deposits are River Terrace Deposits (Undifferentiated) - Sand And Gravel.
Bedrock geology classification	The British Geological Society records of the site show that it is located within the Lewes Nodular Chalk Formation And Seaford Chalk Formation (Undifferentiated) - Chalk.
Landis Top Soil Infiltration	The SOILSCAPE's records of the site show that it is located within an area of freely draining soils.
Groundwater	The British Geological Survey's flood risk susceptibility maps show that the development has potential for groundwater flooding below ground level. Groundwater levels would tend to vary seasonally and are influenced by ground and meteorological conditions and proximity to water features.
Is infiltration feasible?	Infiltration is not possible on this site due to the findings on groundwater and soils within the site.
Is a discharge to a watercourse possible?	There are no watercourses in the proximity to the site.
Is a discharge to a surface water sewer possible?	There is no surface water sewer in the proximity to the site.
Is a discharge to a combined sewer possible?	There is a combined water sewer in the proximity to the site. It is possible to connect to the combined water sewer.

## Existing and Proposed Peak Run-off Calculations

- 4.1 The current site is a Brownfield. The peak runoff rate for the existing site was calculated as per table 4 and discharge rates as per table 5.

Table 4: Peak run-off rate calculation method for existing site

Method Used	Calculation Method
	Report 124 Flood Estimation for Small Catchments method has been used to estimate the site peak flow rates
X	This is a brownfield site, runoff rates are calculated in accordance with best practice simulation modelling and using the modified rational method
	This is a brownfield site where the pre-development drainage isn't known. The runoff rates are calculated using the Greenfield model with soil type 5

- 4.2 The runoff flow produced by the development will be controlled as per table 5.

Table 5: Runoff discharge rate control

Control Used	Description of runoff discharge
	Water will be discharged into the ground via a SuDS as described in table 6 below
	The peak discharge rate has been reduced to Greenfield Qbar flow
	The peak discharge rate has been taken as 0.7 l/s as it is not possible to reduce it to the Greenfield Qbar rate
	The peak discharge rate has been reduced to Brownfield pre-development 1 in 1 flow
X	The peak discharge rate has been reduced by 60% from the existing Brownfield pre-development 1 in 2 flow rate

## Run-off flows

- 4.3 The size of the SuDS has been calculated for all events up to the 1 in 100 including an allowance for climate change of 40%. As per tables above, it is proposed to discharge at a rate of 2.8 l/s. See table 6 for values and appendix C for calculations.

Table 6: Peak discharge rates for SuDS

Return Period Event	Discharge Rate (l/s)			Infiltration Rate (m/hr)
	Existing Greenfield	Existing Brownfield	Proposed	
Qbar	0.20	N/A	N/A	0.0000
1 in 1	0.20	5.50	2.8	0.0000
1 in 2	0.20	7.00	2.8	0.0000
1 in 30	0.50	13.00	2.8	0.0000
1 in 30 + CC	N/A	N/A	2.8	0.0000
1 in 100	0.70	16.60	2.8	0.0000
1 in 100 + CC	N/A	N/A	2.8	0.0000

## Proposed Sustainable Drainage System

- 5.1 The following sustainable drainage systems have been used for this site. The drainage design uses these drainage system through out the site. See table 7 for details.

Table 7: Proposed Drainage System

SuDS Proposed	Feasible	Proposed
Use of green roofs	No	No
Store rainwater for later use	No	No
Use infiltration techniques, for instance soakaways, permeable surfaces	No	No
Attenuate rainwater in ponds or open water features for gradual release	No	No
Attenuate rainwater by storing in tanks or sealed water features for gradual release	Yes	Yes
<b>Discharge Point Proposed</b>		
Discharge rainwater direct to a watercourse	No	No
Discharge rainwater to a surface water sewer/drain	No	No
Discharge rainwater to the combined sewer	Yes	Yes

- 5.2 The location and details of the SuDS can be seen drainage layouts in appendix D. Calculations are in appendix C.
- 5.3 The drainage calculations demonstrate:
- No flooding occurs for the 1 in 30 storm events.
  - Any flooding for the 1 in 100 year + 40% climate change event can be safely contained on site
- 5.4 The proposed drainage strategy presents one possible solution to demonstrate that the development can be sustainably drained, to comply with the requirements of the NPPF. Other solutions may be feasible and may prove to be better suited to the site. These will become apparent during the detailed design stage. The strategy above should not therefore be interpreted as the definitive scheme solution.

### ■ Management of Exceedance Flows

- 5.5 The drainage network has been designed to attenuate surface runoff for all events up to and including the 1% AEP + CC(1 in 100 years). However consideration has been given to what may happen when the design capacity of the surface water drainage network is exceeded. Surface water will flow to the lowest points within the site. The flood risk to the buildings would therefore remain low. See appendix D.



## Maintenance and Management plan responsibility

6.1 The SuDS will be maintained by The Owner the property

## Maintenance and Management plan for proposed SuDS

6.2 The maintenance and Management Plan Guidance from the SuDS Manual, CIRIA C753 (CIRIA, 2015) is to be followed for the effective maintenance of the proposed SuDS techniques outlined above. The maintenance for SuDS structures are as follow:

INLETS, OUTLETS, CONTROLS AND INSPECTION CHAMBERS	
Regular Maintenance	Frequency
<b>Inlets, outlets and surface control structures</b>	
Inspect surface structures removing obstructions and silt as necessary. Check there is no physical damage.	Monthly
Strim vegetation 1m min. surround to structures and keep hard aprons free from silt and debris	Monthly
<b>Inspection chambers and below ground control chambers</b>	
Remove cover and inspect ensuring water is flowing freely and that the exit route for water is unobstructed. Remove debris and silt.	Annually
Undertake inspection after leaf fall in autumn	
<b>Occasional Maintenance</b>	
Check topsoil levels are 20mm above edges of baskets and chambers to avoid mower damage	As necessary
<b>Remedial work</b>	<b>Frequency</b>
Unpack stone in basket features and unblock or repair and repack stone as design detail as necessary.	As required
Repair physical damage if necessary.	As required

Operation and maintenance requirements for attenuation storage tanks		
Maintenance schedule	Required action	Typical frequency
Regular maintenance	Inspect and identify any areas that are not operating correctly. If required, take remedial action	Monthly for 3 months, then annually
	Remove debris from the catchment surface (where it may cause risks to performance)	Monthly
	For systems where rainfall infiltrates into the tank from above, check surface of filter for blockage by sediment, algae or other matter; remove and replace surface infiltration medium as necessary.	Annually
	Remove sediment from pre-treatment structures and/or internal forebays	Annually, or as required
Remedial actions	Repair/rehabilitate inlets, outlet, overflows and vents	As required
Monitoring	Inspect/check all inlets, outlets, vents and overflows to ensure that they are in good condition and operating as designed	Annually
	Survey inside of tank for sediment build-up and remove if necessary	Every 5 years or as required




# Appendix A

Drawing Scale Bar			
Drawing scale	Line length	Drawing scale	Line length
1:5	= 0.25 metres	1:200	= 10.0 metres
1:10	= 0.5 metres	1:250	= 12.5 metres
1:20	= 1.0 metres	1:500	= 25.0 metres
1:25	= 1.25 metres	1:1000	= 50.0 metres
1:50	= 2.5 metres	1:1250	= 62.5 metres
1:100	= 5.0 metres	1:2500	= 125 metres

Measure length of line above for checking of scale

GENERAL NOTES

KEY

-  PERMEABLE AREAS
-  IMPERMEABLE AREAS
-  STUDY AREA

Rev	Details	Date	By	CHK

Drawing Status:  
**PRELIMINARY**

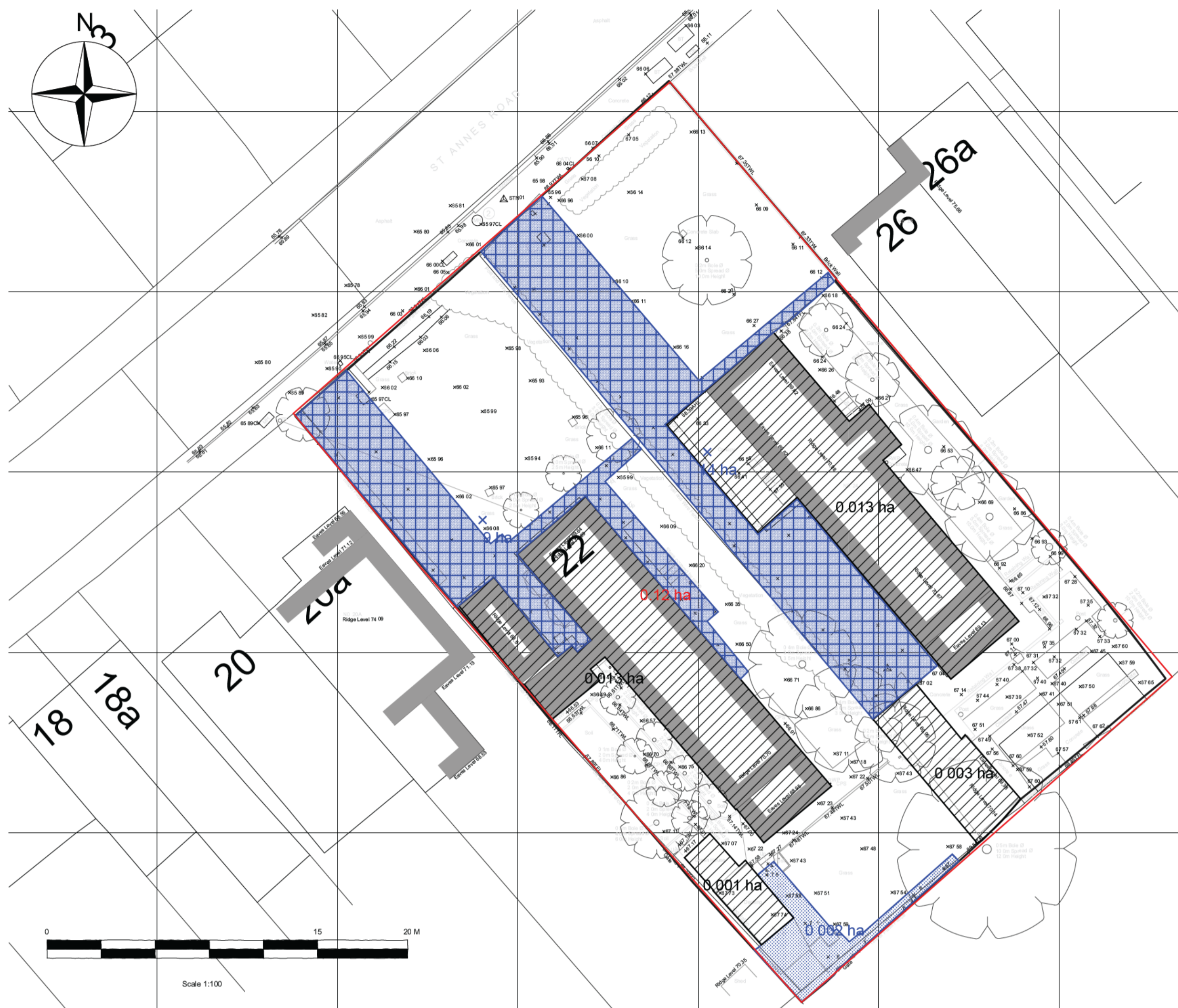


Client:

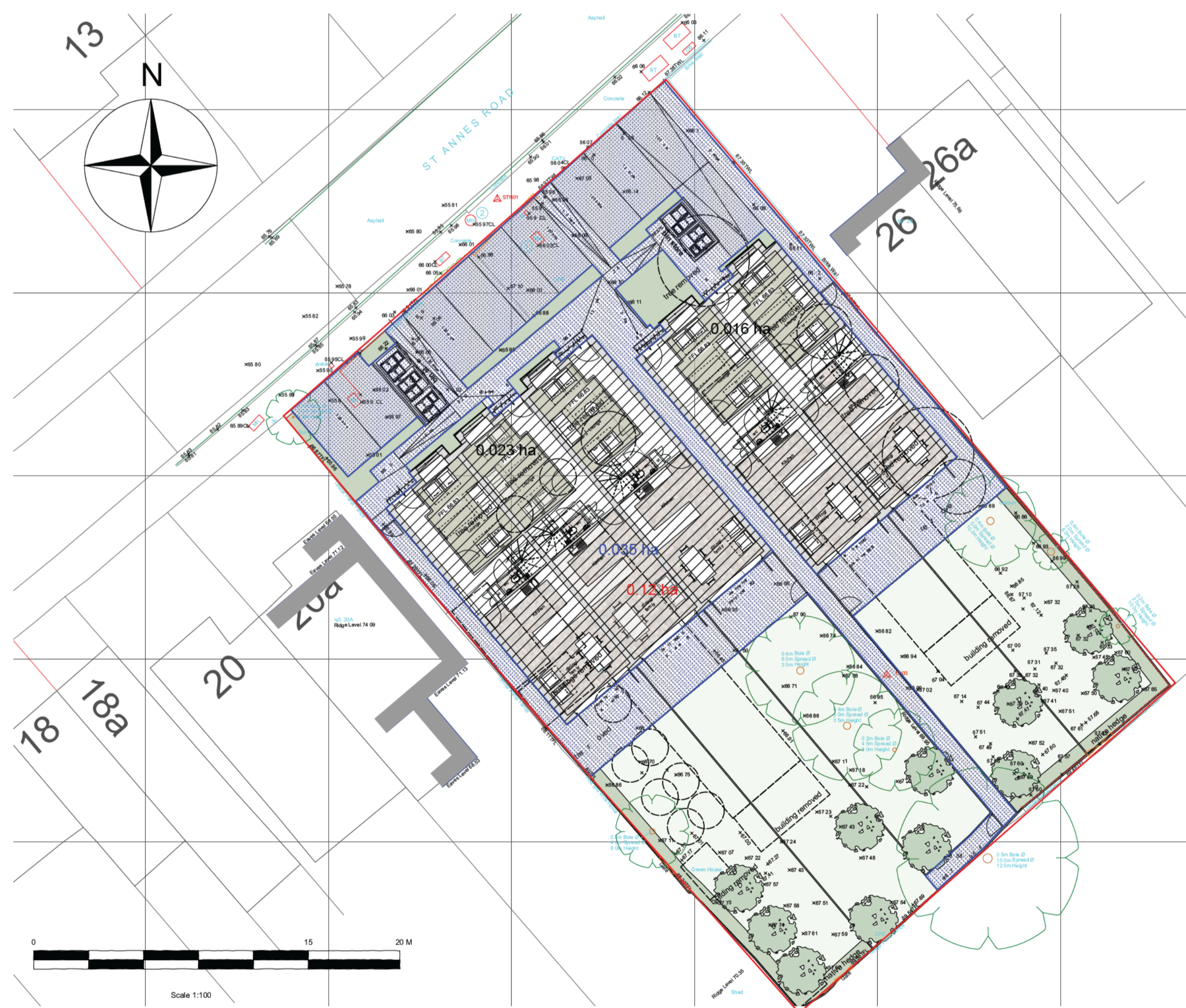
Project:  
22&24 St. Annes Road, London Colney, AL2 1LJ

Drawing:  
Existing and Proposed Areas  
Permeable and Impermeable

Print Size	Project No.	Drawing No.	Revision
A1	0497	002	P1



EXISTING SITE 1:200



PROPOSED SITE 1:200



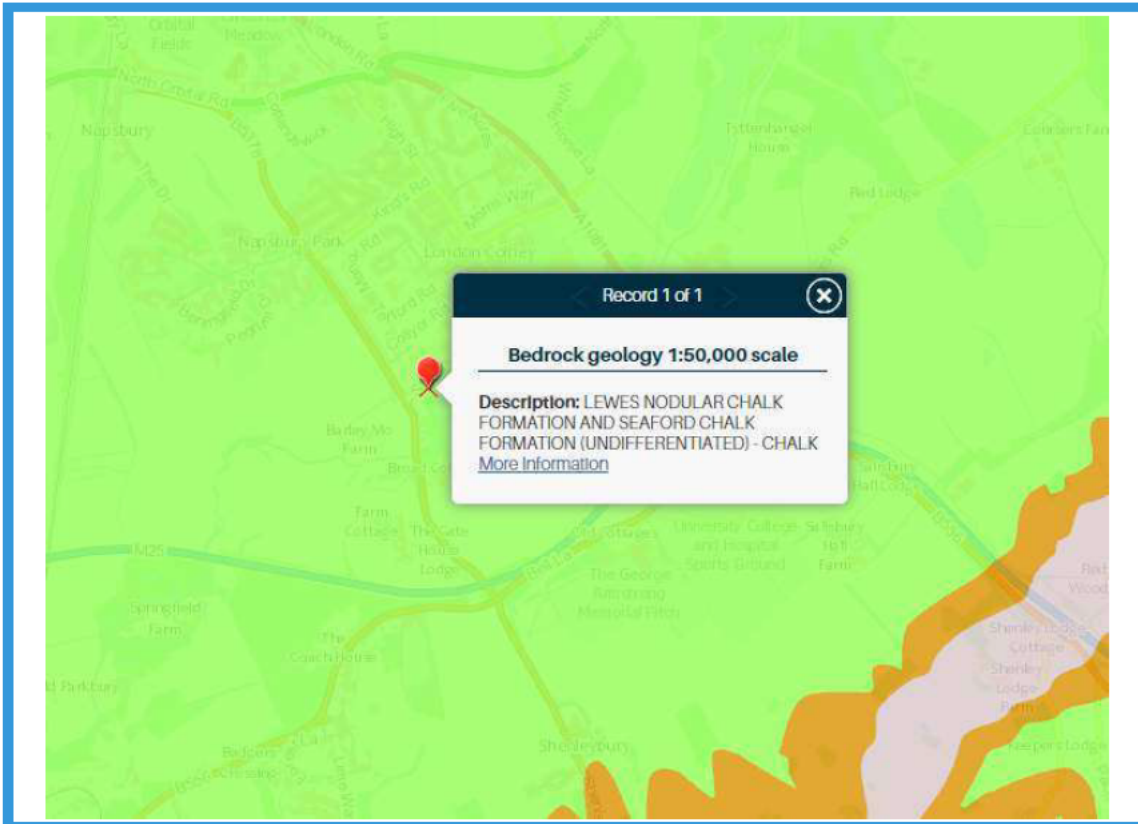
# Appendix B

# SITE GEOLOGY

**GEOINDEX  
ONSHORE**



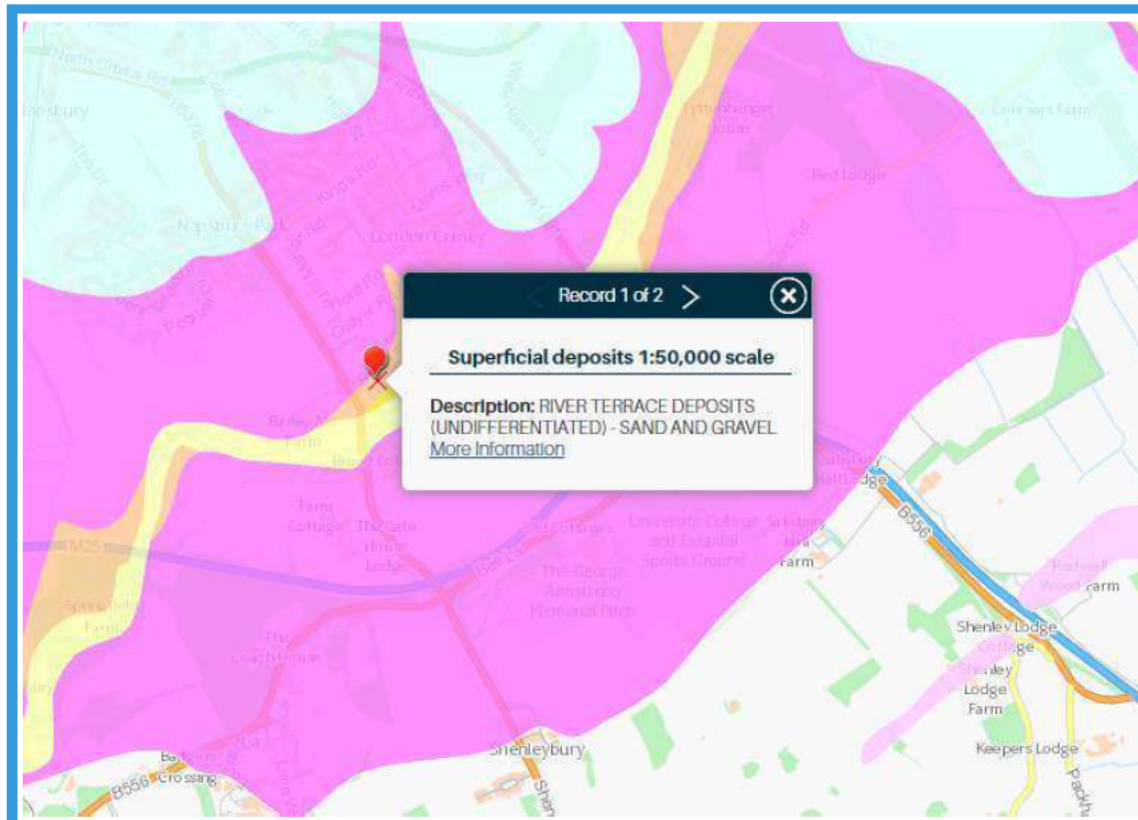
**GEOLOGY - BEDROCK - LEWES NODULAR CHALK FORMATION AND SEAFORD CHALK FORMATION (UNDIFFERENTIATED) - CHALK**



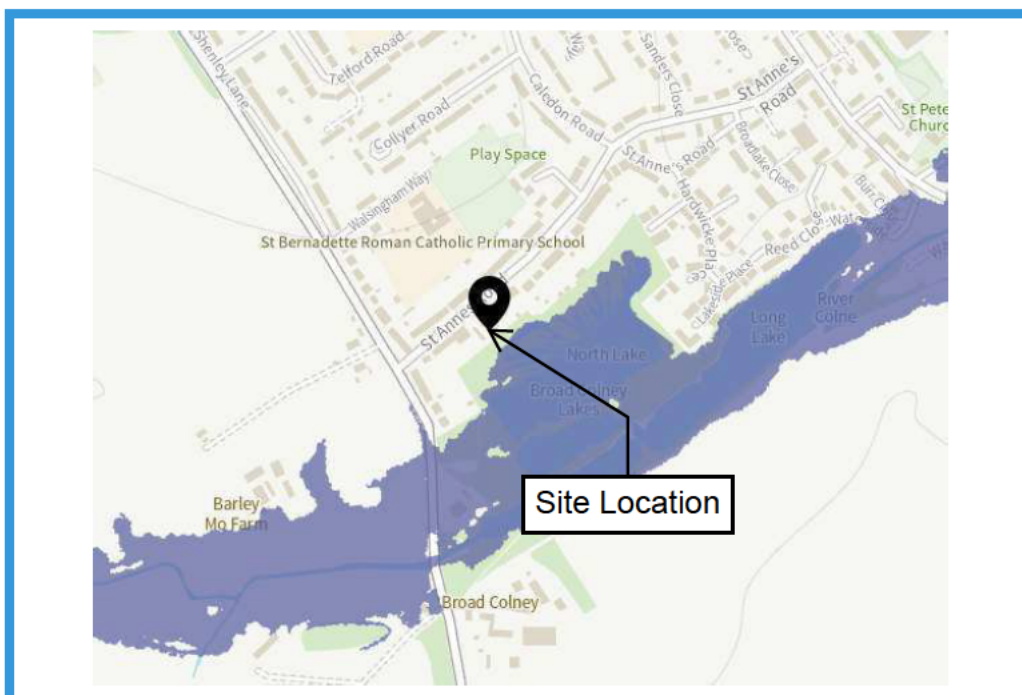
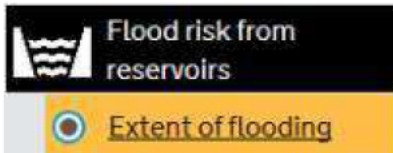
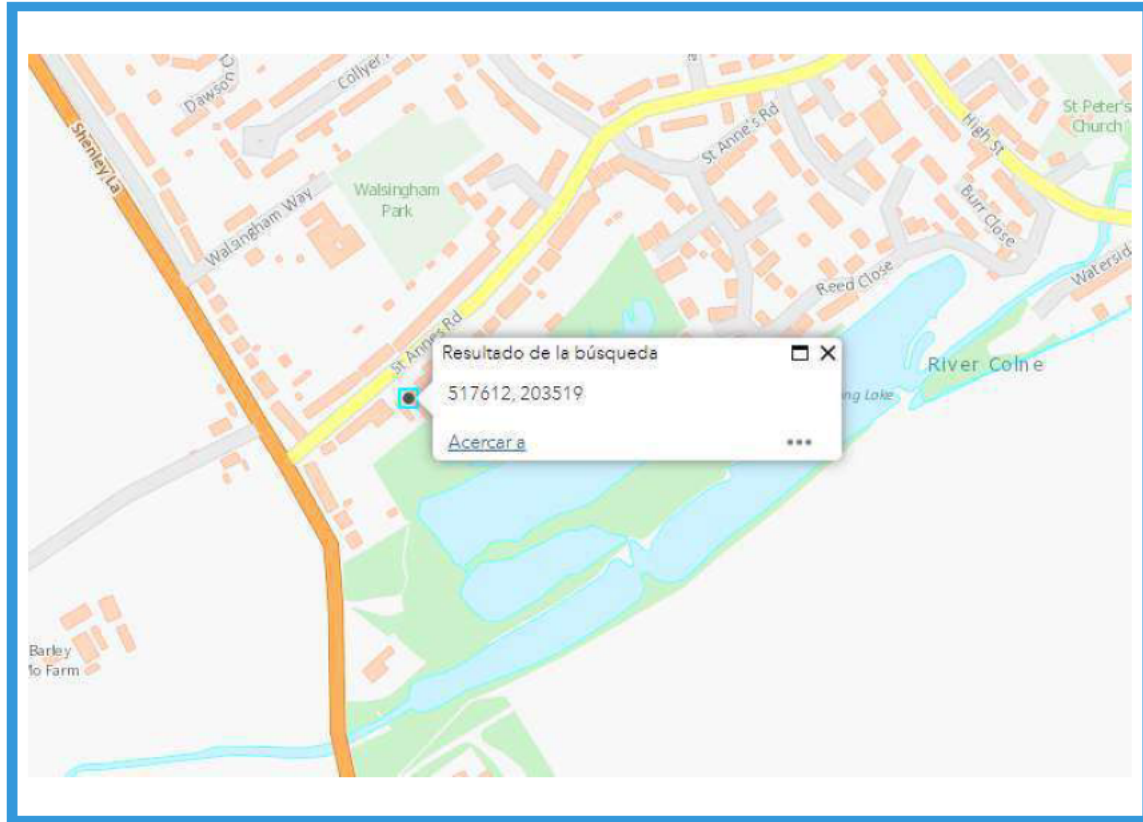
**GEOINDEX  
ONSHORE**




**GEOLOGY - SUPERFICIAL DEPOSITS - RIVER TERRACE DEPOSITS (UNDIFFERENTIATED) - SAND AND GRAVEL**




## Main River Map

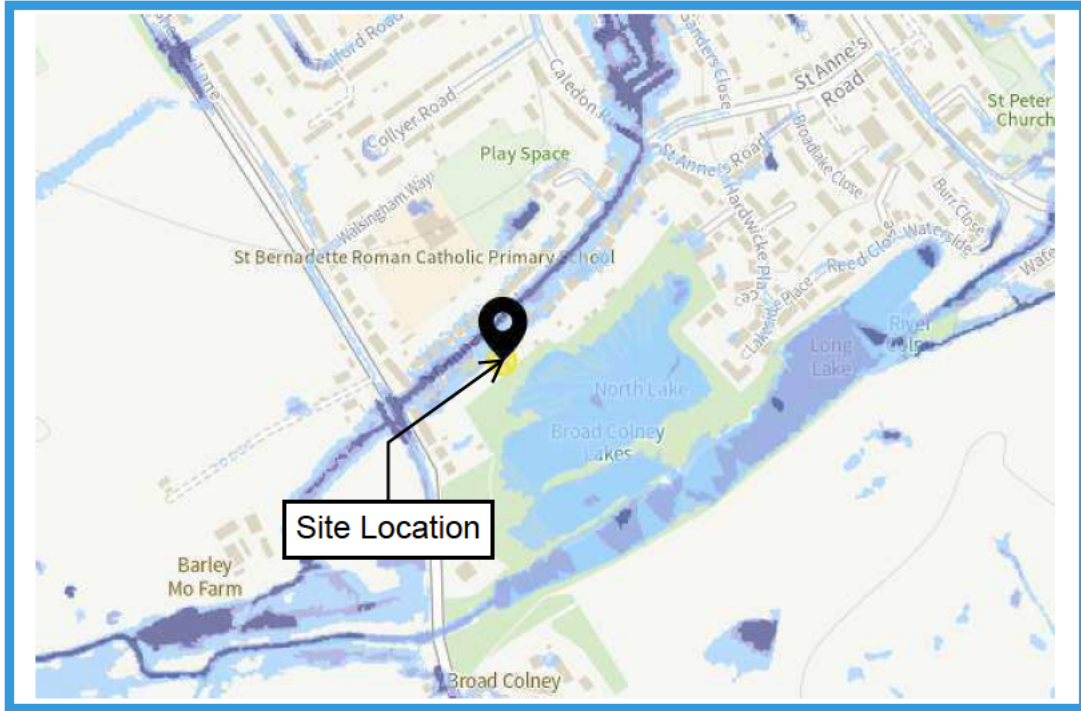


# SITE SURFACE WATER FLOOD RISK

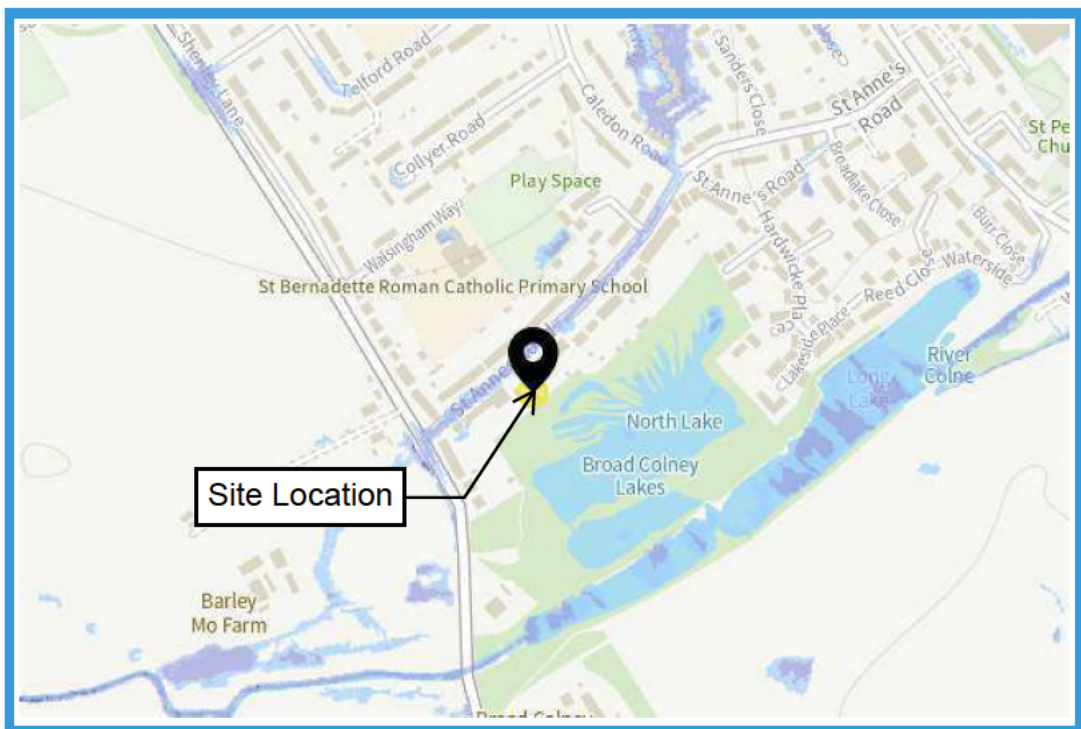
 **Flood risk from surface water**

 **Extent of flooding**

High risk means a chance of flooding greater than 3.3% (1:30)  
 Medium risk means a chance of flooding of btw 1% (1:100) and 3.3%  
 Low risk means a chance of flooding of btw 0.1% (1:1000) and 1%  
 Flooding from surface water is difficult to predict as rainfall location and volume are difficult to forecast. In addition, local features can greatly affect the chance and severity of flooding



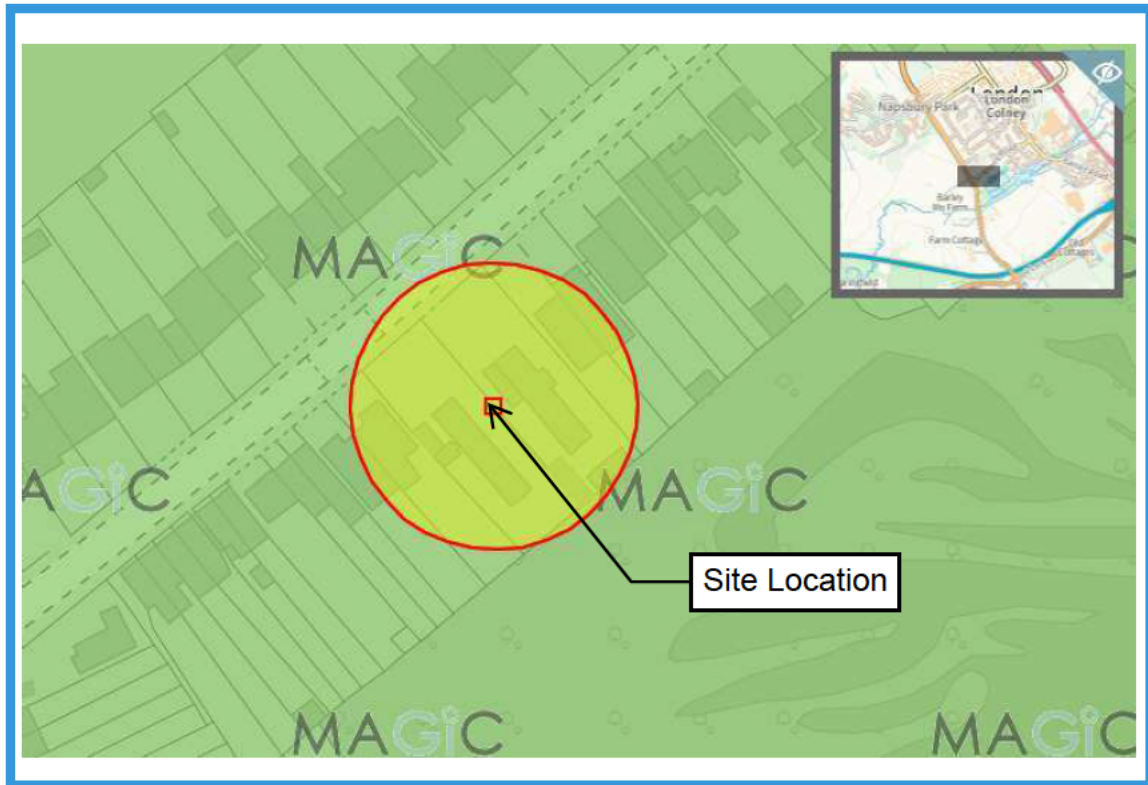
-  **High risk**  
More than 3.3% chance each year
-  **Medium risk**  
Between 1% and 3.3% chance each year
-  **Low risk**  
Between 0.1% and 1% chance each year



-  **Above 90cm**
-  **30cm to 90cm**
-  **Below 30cm**



# MAGIC RESULTS



**Site Check Results** [X]

Site Check Report Report generated on Mon Jun 17 2024  
**You selected the location:** Centroid Grid Ref: TL17610351  
The following features have been found in your search area:

Source Protection Zones merged (England)	
Zone	3
Zone	2

Aquifer Designation Map (Bedrock) (England)	
Typology	Principal

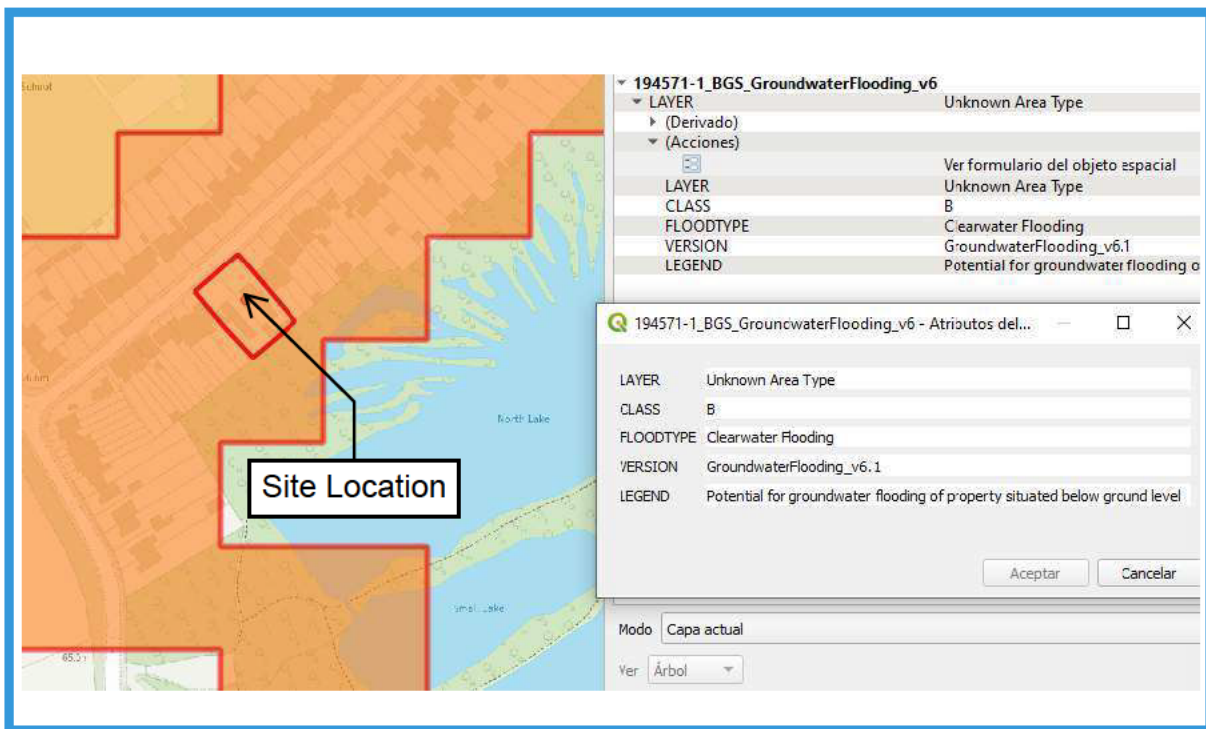
Aquifer Designation Map (Superficial Drift) (England)	
Typology	Secondary A

OK Cancel Export to CSV Print

# SOILSCAPES MAP



# GROUND WATER FLOOD RISK



# Flood map for planning

Your reference  
<Unspecified>

Location (easting/northing)  
517612/203517

Created  
18 Jun 2024 5:15

**Your selected location is in flood zone 3, an area with a high probability of flooding.**

## This means:

- you must complete a flood risk assessment for development in this area
- you should follow the Environment Agency's standing advice for carrying out a flood risk assessment (see [www.gov.uk/guidance/flood-risk-assessment-standing-advice](http://www.gov.uk/guidance/flood-risk-assessment-standing-advice))

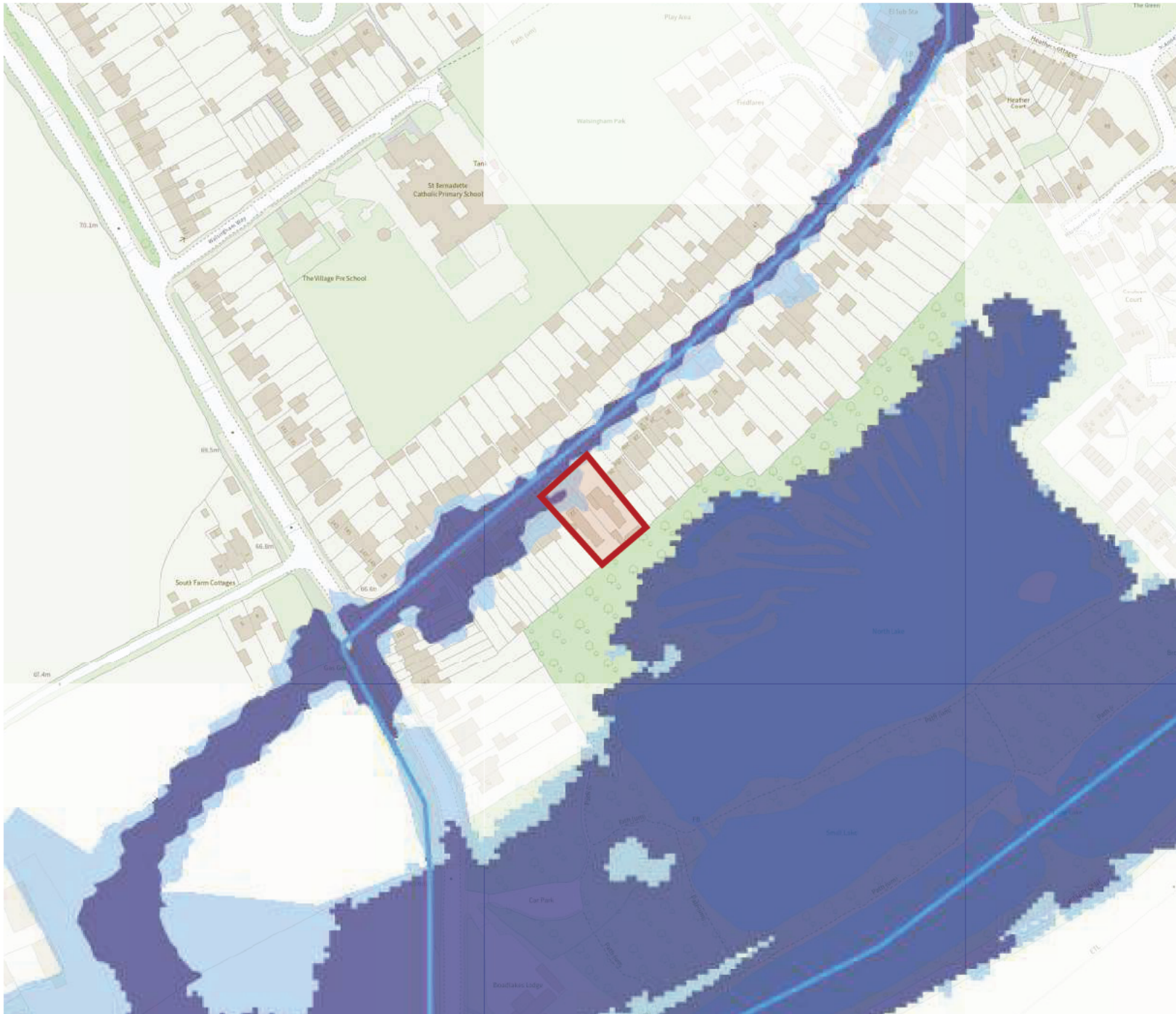
## Notes

The flood map for planning shows river and sea flooding data only. It doesn't include other sources of flooding. It is for use in development planning and flood risk assessments.

This information relates to the selected location and is not specific to any property within it. The map is updated regularly and is correct at the time of printing.

Flood risk data is covered by the Open Government Licence which sets out the terms and conditions for using government data. <https://www.nationalarchives.gov.uk/doc/open-government-licence/version/3/>

Use of the address and mapping data is subject to Ordnance Survey public viewing terms under Crown copyright and database rights 2022 OS 100024198. <https://flood-map-for-planning.service.gov.uk/os-terms>



<Unspecified>

517612/203517

1:2500

18 Jun 2024 5:15



Site Check Report Report generated on Mon Jun 17 2024  
**You selected the location:** Centroid Grid Ref: TL17610351  
 The following features have been found in your search area:

#### SSSI Impact Risk Zones - to assess planning applications for likely impacts on SSSIs/SACs/SPAs & Ramsar sites (England)

**1. DOES PLANNING PROPOSAL FALL INTO ONE OR MORE OF 2. IF YES, CHECK THE CORRESPONDING DESCRIPTION(S) BELOW. LPA SHOULD CONSULT THE CATEGORIES BELOW? NATURAL ENGLAND ON LIKELY RISKS FROM THE FOLLOWING:**

##### All Planning Applications

##### Infrastructure

Airports, helipads and other aviation proposals.

##### Wind & Solar Energy

##### Minerals, Oil & Gas

Oil & gas exploration/extraction.

##### Rural Non Residential

##### Residential

##### Rural Residential

##### Air Pollution

Livestock & poultry units with floorspace > 500m<sup>2</sup>, slurry lagoons & digestate stores > 750m<sup>2</sup>, manure stores > 3500t.

##### Combustion

##### Waste

##### Composting

##### Discharges

##### Water Supply

##### Notes 1

##### Notes 2

##### GUIDANCE - How to use the Impact Risk Zones

[/Metadata for magic/SSSI IRZ User Guidance MAGIC.pdf](#)

#### Source Protection Zones merged (England)

Zone 3

Zone 2

#### Aquifer Designation Map (Bedrock) (England)

Typology Principal

#### Aquifer Designation Map (Superficial Drift) (England)

Typology Secondary A

#### Soilscape (England)

##### Reference

6

##### Name

FREELY DRAINING SLIGHTLY ACID LOAMY SOILS

##### Main Surface Texture Class

LOAMY

##### Natural Drainage Type

FREELY DRAINING

##### Natural Fertility

LOW

##### Characteristic Semi-natural Habitats

NEUTRAL AND ACID PASTURES AND DECIDUOUS WOODLANDS; ACID COMMUNITIES SUCH AS BRACKEN AND GORSE IN THE UPLANDS

##### Main Land Cover

ARABLE AND GRASSLAND

##### Hyperlink

[/Metadata for magic/soilscape\\_summary.pdf](#)

#### Areas of Outstanding Natural Beauty (England)

No Features found

#### Limestone Pavement Orders (England)

No Features found

#### Local Nature Reserves (England) - points

No Features found

#### Local Nature Reserves (England)

No Features found

#### Moorland Line (England)

No Features found

#### National Nature Reserves (England) - points

No Features found

**National Nature Reserves (England)**  
No Features found

**National Parks (England)**  
No Features found

**Ramsar Sites (England) - points**  
No Features found

**Ramsar Sites (England)**  
No Features found

**Proposed Ramsar Sites (England) - points**  
No Features found

**Proposed Ramsar Sites (England)**  
No Features found

**Sites of Special Scientific Interest Units (England) - points**  
No Features found

**Sites of Special Scientific Interest Units (England)**  
No Features found

**Sites of Special Scientific Interest (England) - points**  
No Features found

**Sites of Special Scientific Interest (England)**  
No Features found

**Special Areas of Conservation (England) - points**  
No Features found

**Special Areas of Conservation (England)**  
No Features found

**Possible Special Areas of Conservation (England) - points**  
No Features found

**Possible Special Areas of Conservation (England)**  
No Features found

**Special Protection Areas (England) - points**  
No Features found

**Special Protection Areas (England)**  
No Features found

**Potential Special Protection Areas (England) - points**  
No Features found

**Potential Special Protection Areas (England)**  
No Features found

**Biosphere Reserves (England) - points**  
No Features found

**Biosphere Reserves (England)**  
No Features found

**Less Favoured Areas (England)**  
No Features found

**Nitrate Vulnerable Zones 2017 Designations (England)**  
No Features found

**Wild Bird General Licence Protected Sites Condition Zone (England)**  
No Features found

# Appendix C



**Simulation Settings**

Rainfall Methodology	FSR	Drain Down Time (mins)	240
FSR Region	England and Wales	Additional Storage (m <sup>3</sup> /ha)	0.0
M5-60 (mm)	20.000	Check Discharge Rate(s)	✓
Ratio-R	0.400	1 year (l/s)	0.2
Summer CV	1.000	2 year (l/s)	0.2
Winter CV	1.000	30 year (l/s)	0.5
Analysis Speed	Normal	100 year (l/s)	0.7
Skip Steady State	x	Check Discharge Volume	x

**Storm Durations**

15 | 30 | 60 | 120 | 180 | 240 | 360 | 480 | 600 | 720 | 960 | 1440

Return Period (years)	Climate Change (CC %)	Additional Area (A %)	Additional Flow (Q %)
1	0	0	0
2	0	0	0
30	0	0	0
30	40	0	0
100	0	0	0
100	40	0	0

**Pre-development Discharge Rate**

Site Makeup	Greenfield	Growth Factor 30 year	2.40
Greenfield Method	IH124	Growth Factor 100 year	3.19
Positively Drained Area (ha)	0.120	Betterment (%)	0
SAAR (mm)	673	QBar	0.2
Soil Index	2	Q 1 year (l/s)	0.2
SPR	0.30	Q 2 year (l/s)	0.2
Region	6	Q 30 year (l/s)	0.5
Growth Factor 1 year	0.85	Q 100 year (l/s)	0.7
Growth Factor 2 year	0.88		





**Simulation Settings**

Rainfall Methodology	FSR	Drain Down Time (mins)	240
FSR Region	England and Wales	Additional Storage (m <sup>3</sup> /ha)	0.0
M5-60 (mm)	20.000	Check Discharge Rate(s)	✓
Ratio-R	0.400	1 year (l/s)	5.5
Summer CV	1.000	2 year (l/s)	7.0
Winter CV	1.000	30 year (l/s)	13.0
Analysis Speed	Normal	100 year (l/s)	16.6
Skip Steady State	x	Check Discharge Volume	x

**Storm Durations**

15 | 30 | 60 | 120 | 180 | 240 | 360 | 480 | 600 | 720 | 960 | 1440

Return Period (years)	Climate Change (CC %)	Additional Area (A %)	Additional Flow (Q %)
1	0	0	0
2	0	0	0
30	0	0	0
30	40	0	0
100	0	0	0
100	40	0	0

**Pre-development Discharge Rate**

Site Makeup	Brownfield	Betterment (%)	0
Brownfield Method	MRM	Q 1 year (l/s)	5.5
Contributing Area (ha)	0.030	Q 2 year (l/s)	7.0
PIMP (%)	100	Q 30 year (l/s)	13.0
CV	1.000	Q 100 year (l/s)	16.6
Time of Concentration (mins)	6.00		

**Design Settings**

Rainfall Methodology	FSR	Maximum Time of Concentration (mins)	30.00
Return Period (years)	2	Maximum Rainfall (mm/hr)	50.0
Additional Flow (%)	0	Minimum Velocity (m/s)	1.00
FSR Region	England and Wales	Connection Type	Level Soffits
M5-60 (mm)	20.000	Minimum Backdrop Height (m)	0.200
Ratio-R	0.400	Preferred Cover Depth (m)	1.200
CV	1.000	Include Intermediate Ground	✓
Time of Entry (mins)	6.00	Enforce best practice design rules	✓

**Circular Link Type**

Shape	Circular	Auto Increment (mm)	75
Barrels	1	Follow Ground	x

**Available Diameters (mm)**

100 | 150

**Nodes**

Name	Area (ha)	T of E (mins)	Cover Level (m)	Diameter (mm)	Easting (m)	Northing (m)	Depth (m)
Development	0.043	6.00	66.100	1200	0.047	50.000	0.700
Tank			66.000		26.620	50.000	1.100
Outfall			66.000	1200	50.396	50.350	1.500

**Links (Input)**

Name	US Node	DS Node	Length (m)	ks (mm) / n	US IL (m)	DS IL (m)	Fall (m)	Slope (1:X)	Dia (mm)	T of C (mins)	Rain (mm/hr)
1.000	Development	Tank	20.000	0.600	65.400	64.900	0.500	40.0	150	6.21	50.0
1.001	Tank	Outfall	20.000	0.600	64.900	64.500	0.400	50.0	150	6.44	50.0

**Pipeline Schedule**

Link	Length (m)	Slope (1:X)	Dia (mm)	Link Type	US CL (m)	US IL (m)	US Depth (m)	DS CL (m)	DS IL (m)	DS Depth (m)
1.000	20.000	40.0	150	Circular	66.100	65.400	0.550	66.000	64.900	0.950
1.001	20.000	50.0	150	Circular	66.000	64.900	0.950	66.000	64.500	1.350

Link	US Node	Dia (mm)	Node Type	MH Type	DS Node	Dia (mm)	Node Type	MH Type
1.000	Development	1200	Manhole	Adoptable	Tank		Junction	
1.001	Tank		Junction		Outfall	1200	Manhole	Adoptable

**Manhole Schedule**

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connections	Link	IL (m)	Dia (mm)
Development	0.047	50.000	66.100	0.700	1200				
						0	1.000	65.400	150

**Manhole Schedule**

Node	Easting (m)	Northing (m)	CL (m)	Depth (m)	Dia (mm)	Connections	Link	IL (m)	Dia (mm)
Tank	26.620	50.000	66.000	1.100		1	1.000	64.900	150
						0	1.001	64.900	150
Outfall	50.396	50.350	66.000	1.500	1200	1	1.001	64.500	150

**Simulation Settings**

Rainfall Methodology	FSR	Drain Down Time (mins)	240
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M5-60 (mm)	20.000	Check Discharge Rate(s)	✓
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Summer CV	1.000	2 year (l/s)	7.0
Winter CV	1.000	30 year (l/s)	13.0
Analysis Speed	Normal	100 year (l/s)	16.6
Skip Steady State	x	Check Discharge Volume	x

**Storm Durations**

15 | 30 | 60 | 120 | 180 | 240 | 360 | 480 | 600 | 720 | 960 | 1440

Return Period (years)	Climate Change (CC %)	Additional Area (A %)	Additional Flow (Q %)
1	0	0	0
2	0	0	0
30	0	0	0
30	40	0	0
100	0	0	0
100	40	0	0

**Pre-development Discharge Rate**

Site Makeup	Brownfield	Time of Concentration (mins)	6.00
Brownfield Method	MRM	Betterment (%)	0
Contributing Area (ha)	0.030	Q 1 year (l/s)	
PIMP (%)	100	Q 30 year (l/s)	
CV	1.000	Q 100 year (l/s)	

**Node Tank Online Orifice Control**

Flap Valve	x	Invert Level (m)	64.900	Diameter (m)	0.035
Downstream Link	1.001	Design Depth (m)	1.100	Discharge Coefficient	0.600
Replaces Downstream Link	✓	Design Flow (l/s)	2.8		

**Node Tank Depth/Area Storage Structure**

Base Inf Coefficient (m/hr)	0.00000	Safety Factor	2.0	Invert Level (m)	64.900
Side Inf Coefficient (m/hr)	0.00000	Porosity	0.95	Time to half empty (mins)	192

Depth (m)	Area (m <sup>2</sup> )	Inf Area (m <sup>2</sup> )	Depth (m)	Area (m <sup>2</sup> )	Inf Area (m <sup>2</sup> )	Depth (m)	Area (m <sup>2</sup> )	Inf Area (m <sup>2</sup> )	Depth (m)	Area (m <sup>2</sup> )	Inf Area (m <sup>2</sup> )
0.000	54.0	0.0	0.200	54.0	0.0	0.400	54.0	0.0	0.401	0.0	0.0

**Approval Settings**

Node Size	x	Coordinates	x	Full Bore Velocity	x	Time to Half Empty	✓
Node Losses	x	Crossings	x	Proportional Velocity	x	Return Period (years)	10
Link Size	x	Cover Depth	x	Surcharged Depth	x	Discharge Rates	x
Link Length	x	Backdrops	x	Flooding	x	Discharge Volume	x

**Rainfall**

Event	Peak Intensity (mm/hr)	Average Intensity (mm/hr)	Event	Peak Intensity (mm/hr)	Average Intensity (mm/hr)
1 year 15 minute summer	109.521	30.991	2 year 600 minute winter	7.576	3.033
1 year 15 minute winter	76.857	30.991	2 year 720 minute summer	9.878	2.647
1 year 30 minute summer	71.439	20.215	2 year 720 minute winter	6.639	2.647
1 year 30 minute winter	50.133	20.215	2 year 960 minute summer	8.113	2.136
1 year 60 minute summer	48.435	12.800	2 year 960 minute winter	5.374	2.136
1 year 60 minute winter	32.179	12.800	2 year 1440 minute summer	5.891	1.579
1 year 120 minute summer	30.053	7.942	2 year 1440 minute winter	3.959	1.579
1 year 120 minute winter	19.966	7.942	30 year 15 minute summer	268.706	76.035
1 year 180 minute summer	23.233	5.979	30 year 15 minute winter	188.566	76.035
1 year 180 minute winter	15.102	5.979	30 year 30 minute summer	174.929	49.499
1 year 240 minute summer	18.475	4.882	30 year 30 minute winter	122.757	49.499
1 year 240 minute winter	12.274	4.882	30 year 60 minute summer	116.589	30.811
1 year 360 minute summer	14.169	3.646	30 year 60 minute winter	77.459	30.811
1 year 360 minute winter	9.210	3.646	30 year 120 minute summer	70.438	18.615
1 year 480 minute summer	11.185	2.956	30 year 120 minute winter	46.797	18.615
1 year 480 minute winter	7.431	2.956	30 year 180 minute summer	53.298	13.715
1 year 600 minute summer	9.182	2.511	30 year 180 minute winter	34.645	13.715
1 year 600 minute winter	6.274	2.511	30 year 240 minute summer	41.604	10.995
1 year 720 minute summer	8.203	2.199	30 year 240 minute winter	27.641	10.995
1 year 720 minute winter	5.513	2.199	30 year 360 minute summer	31.221	8.034
1 year 960 minute summer	6.768	1.782	30 year 360 minute winter	20.295	8.034
1 year 960 minute winter	4.483	1.782	30 year 480 minute summer	24.324	6.428
1 year 1440 minute summer	4.949	1.326	30 year 480 minute winter	16.160	6.428
1 year 1440 minute winter	3.326	1.326	30 year 600 minute summer	19.756	5.404
2 year 15 minute summer	141.566	40.058	30 year 600 minute winter	13.498	5.404
2 year 15 minute winter	99.345	40.058	30 year 720 minute summer	17.490	4.687
2 year 30 minute summer	91.753	25.963	30 year 720 minute winter	11.754	4.687
2 year 30 minute winter	64.388	25.963	30 year 960 minute summer	14.215	3.743
2 year 60 minute summer	61.301	16.200	30 year 960 minute winter	9.416	3.743
2 year 60 minute winter	40.727	16.200	30 year 1440 minute summer	10.161	2.723
2 year 120 minute summer	37.449	9.897	30 year 1440 minute winter	6.829	2.723
2 year 120 minute winter	24.880	9.897	30 year +40% CC 15 minute summer	376.189	106.449
2 year 180 minute summer	28.672	7.378	30 year +40% CC 15 minute winter	263.992	106.449
2 year 180 minute winter	18.637	7.378	30 year +40% CC 30 minute summer	244.900	69.298
2 year 240 minute summer	22.636	5.982	30 year +40% CC 30 minute winter	171.860	69.298
2 year 240 minute winter	15.039	5.982	30 year +40% CC 60 minute summer	163.225	43.136
2 year 360 minute summer	17.235	4.435	30 year +40% CC 60 minute winter	108.443	43.136
2 year 360 minute winter	11.203	4.435	30 year +40% CC 120 minute summer	98.613	26.061
2 year 480 minute summer	13.550	3.581	30 year +40% CC 120 minute winter	65.516	26.061
2 year 480 minute winter	9.003	3.581	30 year +40% CC 180 minute summer	74.617	19.202
2 year 600 minute summer	11.088	3.033	30 year +40% CC 180 minute winter	48.503	19.202

**Rainfall**

Event	Peak Intensity (mm/hr)	Average Intensity (mm/hr)	Event	Peak Intensity (mm/hr)	Average Intensity (mm/hr)
30 year +40% CC 240 minute summer	58.245	15.393	100 year 600 minute winter	17.376	6.956
30 year +40% CC 240 minute winter	38.697	15.393	100 year 720 minute summer	22.452	6.017
30 year +40% CC 360 minute summer	43.710	11.248	100 year 720 minute winter	15.089	6.017
30 year +40% CC 360 minute winter	28.413	11.248	100 year 960 minute summer	18.166	4.784
30 year +40% CC 480 minute summer	34.053	8.999	100 year 960 minute winter	12.033	4.784
30 year +40% CC 480 minute winter	22.624	8.999	100 year 1440 minute summer	12.896	3.456
30 year +40% CC 600 minute summer	27.658	7.565	100 year 1440 minute winter	8.667	3.456
30 year +40% CC 600 minute winter	18.898	7.565	100 year +40% CC 15 minute summer	488.233	138.153
30 year +40% CC 720 minute summer	24.485	6.562	100 year +40% CC 15 minute winter	342.620	138.153
30 year +40% CC 720 minute winter	16.456	6.562	100 year +40% CC 30 minute summer	320.551	90.705
30 year +40% CC 960 minute summer	19.901	5.240	100 year +40% CC 30 minute winter	224.948	90.705
30 year +40% CC 960 minute winter	13.183	5.240	100 year +40% CC 60 minute summer	214.603	56.713
30 year +40% CC 1440 minute summer	14.225	3.812	100 year +40% CC 60 minute winter	142.577	56.713
30 year +40% CC 1440 minute winter	9.560	3.812	100 year +40% CC 120 minute summer	129.587	34.246
100 year 15 minute summer	348.738	98.681	100 year +40% CC 120 minute winter	86.094	34.246
100 year 15 minute winter	244.728	98.681	100 year +40% CC 180 minute summer	97.729	25.149
100 year 30 minute summer	228.965	64.789	100 year +40% CC 180 minute winter	63.526	25.149
100 year 30 minute winter	160.677	64.789	100 year +40% CC 240 minute summer	75.977	20.078
100 year 60 minute summer	153.288	40.510	100 year +40% CC 240 minute winter	50.477	20.078
100 year 60 minute winter	101.841	40.510	100 year +40% CC 360 minute summer	56.677	14.585
100 year 120 minute summer	92.562	24.461	100 year +40% CC 360 minute winter	36.841	14.585
100 year 120 minute winter	61.496	24.461	100 year +40% CC 480 minute summer	43.979	11.622
100 year 180 minute summer	69.806	17.964	100 year +40% CC 480 minute winter	29.219	11.622
100 year 180 minute winter	45.376	17.964	100 year +40% CC 600 minute summer	35.604	9.738
100 year 240 minute summer	54.269	14.342	100 year +40% CC 600 minute winter	24.327	9.738
100 year 240 minute winter	36.055	14.342	100 year +40% CC 720 minute summer	31.433	8.424
100 year 360 minute summer	40.484	10.418	100 year +40% CC 720 minute winter	21.125	8.424
100 year 360 minute winter	26.315	10.418	100 year +40% CC 960 minute summer	25.432	6.697
100 year 480 minute summer	31.414	8.302	100 year +40% CC 960 minute winter	16.847	6.697
100 year 480 minute winter	20.871	8.302	100 year +40% CC 1440 minute summer	18.055	4.839
100 year 600 minute summer	25.431	6.956	100 year +40% CC 1440 minute winter	12.134	4.839

**Results for 1 year Critical Storm Duration. Lowest mass balance: 99.54%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m <sup>3</sup> )	Flood (m <sup>3</sup> )	Status
15 minute summer	Development	10	65.456	0.056	6.8	0.0635	0.0000	OK
180 minute summer	Tank	120	64.989	0.089	2.6	4.5598	0.0000	OK
15 minute summer	Outfall	1	64.500	0.000	0.5	0.0000	0.0000	OK

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m <sup>3</sup> )	Discharge Vol (m <sup>3</sup> )
15 minute summer	Development	1.000	Tank	6.9	1.883	0.244	0.0910	
180 minute summer	Tank	Orifice	Outfall	0.7				7.2

**Results for 2 year Critical Storm Duration. Lowest mass balance: 99.54%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m <sup>3</sup> )	Flood (m <sup>3</sup> )	Status
15 minute summer	Development	10	65.463	0.063	8.8	0.0718	0.0000	OK
120 minute summer	Tank	88	65.010	0.110	4.3	5.6649	0.0000	OK
15 minute summer	Outfall	1	64.500	0.000	0.6	0.0000	0.0000	OK

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m <sup>3</sup> )	Discharge Vol (m <sup>3</sup> )
15 minute summer	Development	1.000	Tank	8.9	1.955	0.315	0.1186	
120 minute summer	Tank	Orifice	Outfall	0.8				7.9

**Results for 30 year Critical Storm Duration. Lowest mass balance: 99.54%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m <sup>3</sup> )	Flood (m <sup>3</sup> )	Status
15 minute summer	Development	10	65.489	0.089	16.7	0.1004	0.0000	OK
180 minute summer	Tank	128	65.118	0.218	5.9	11.1877	0.0000	SURCHARGED
15 minute summer	Outfall	1	64.500	0.000	0.9	0.0000	0.0000	OK

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m <sup>3</sup> )	Discharge Vol (m <sup>3</sup> )
15 minute summer	Development	1.000	Tank	16.8	2.123	0.597	0.2291	
180 minute summer	Tank	Orifice	Outfall	1.1				16.5



**Results for 30 year +40% CC Critical Storm Duration. Lowest mass balance: 99.54%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m <sup>3</sup> )	Flood (m <sup>3</sup> )	Status
15 minute summer	Development	10	65.511	0.110	23.4	0.1250	0.0000	OK
120 minute winter	Tank	110	65.215	0.315	7.8	16.1809	0.0000	SURCHARGED
15 minute summer	Outfall	1	64.500	0.000	1.1	0.0000	0.0000	OK

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m <sup>3</sup> )	Discharge Vol (m <sup>3</sup> )
15 minute summer	Development	1.000	Tank	23.5	2.173	0.834	0.2957	
120 minute winter	Tank	Orifice	Outfall	1.4				19.6

**Results for 100 year Critical Storm Duration. Lowest mass balance: 99.54%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m <sup>3</sup> )	Flood (m <sup>3</sup> )	Status
15 minute summer	Development	10	65.505	0.105	21.7	0.1183	0.0000	OK
180 minute summer	Tank	132	65.194	0.294	7.8	15.0971	0.0000	SURCHARGED
15 minute summer	Outfall	1	64.500	0.000	1.1	0.0000	0.0000	OK

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m <sup>3</sup> )	Discharge Vol (m <sup>3</sup> )
15 minute summer	Development	1.000	Tank	21.8	2.166	0.774	0.2791	
180 minute summer	Tank	Orifice	Outfall	1.3				20.9

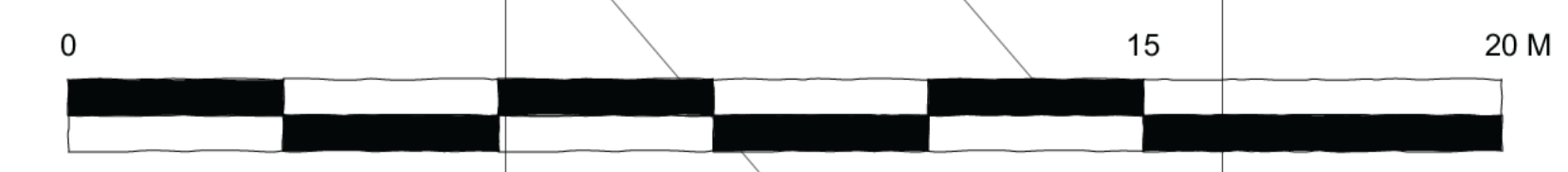
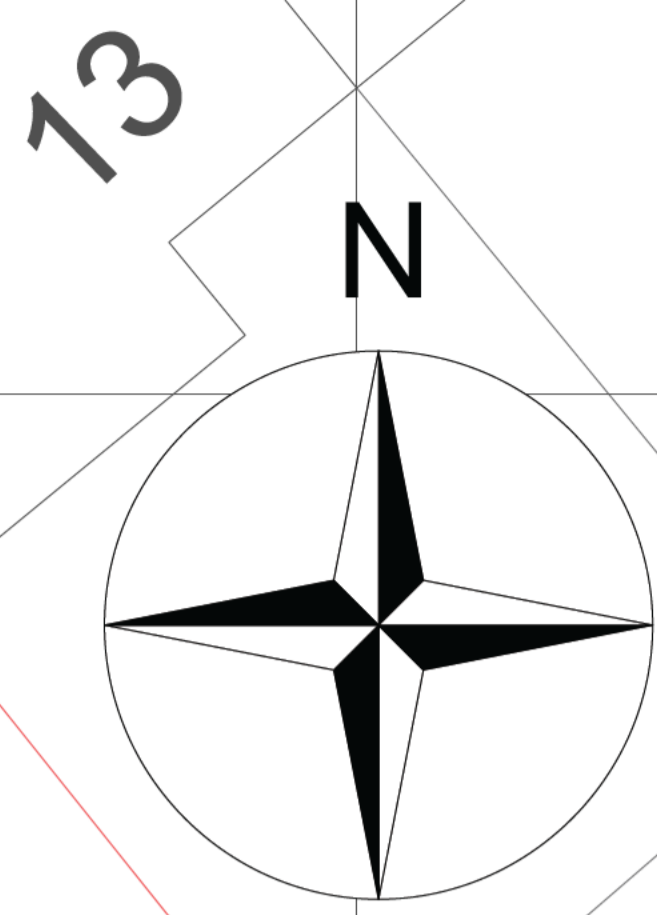
**Results for 100 year +40% CC Critical Storm Duration. Lowest mass balance: 99.54%**

Node Event	US Node	Peak (mins)	Level (m)	Depth (m)	Inflow (l/s)	Node Vol (m <sup>3</sup> )	Flood (m <sup>3</sup> )	Status
15 minute summer	Development	12	65.670	0.270	30.4	0.3054	0.0000	SURCHARGED
180 minute summer	Tank	128	65.665	0.765	10.9	20.5457	0.0000	SURCHARGED
15 minute summer	Outfall	1	64.500	0.000	1.3	0.0000	0.0000	OK

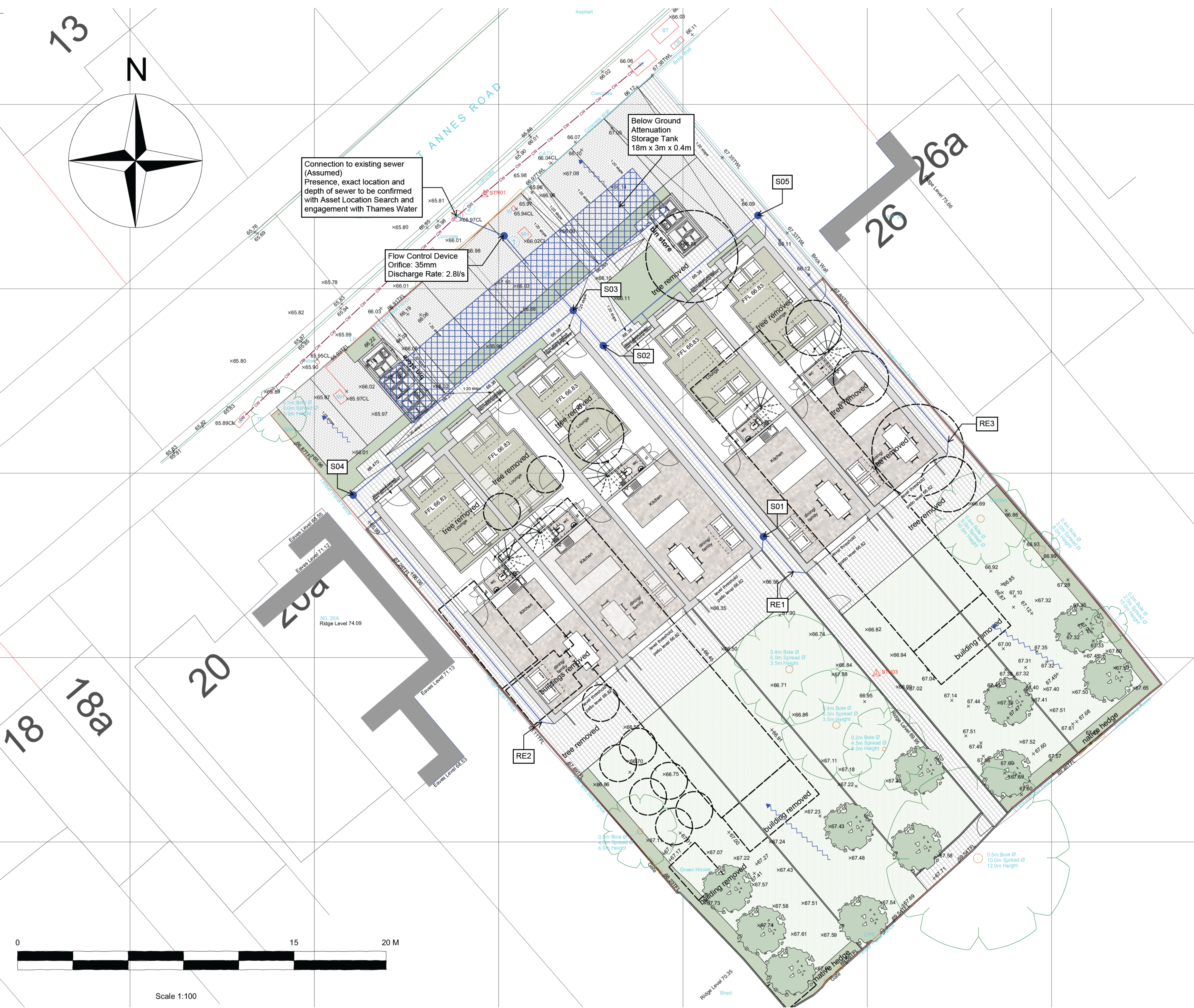
  

Link Event (Upstream Depth)	US Node	Link	DS Node	Outflow (l/s)	Velocity (m/s)	Flow/Cap	Link Vol (m <sup>3</sup> )	Discharge Vol (m <sup>3</sup> )
15 minute summer	Development	1.000	Tank	29.6	2.181	1.051	0.3521	
180 minute summer	Tank	Orifice	Outfall	2.2				27.9

# Appendix D



Scale 1:100



Connection to existing sewer (Assumed)  
Presence, exact location and depth of sewer to be confirmed with Asset Location Search and engagement with Thames Water

Flow Control Device  
Orifice: 35mm  
Discharge Rate: 2.8l/s

Below Ground  
Attenuation  
Storage Tank  
18m x 3m x 0.4m

Do not scale from this drawing. Refer to figured dimensions only. RIDA Reports Ltd registered in England and Wales No. 10590566. This drawing is copyright of RIDA Reports Ltd.

Drawing Scale Bar			
Drawing scale	Line length	Drawing scale	Line length
1:5	= 0.25 metres	1:200	= 10.0 metres
1:10	= 0.5 metres	1:250	= 12.5 metres
1:20	= 1.0 metres	1:500	= 25.0 metres
1:25	= 1.25 metres	1:1000	= 50.0 metres
1:50	= 2.5 metres	1:1250	= 62.5 metres
1:100	= 5.0 metres	1:2500	= 125 metres

Measure length of line above for checking of scale

- GENERAL NOTES**
- All dimensions are in millimetres and levels in m AOD unless stated otherwise.
  - Do not scale. If in any doubt, consult Engineer.
  - Read in conjunction with the architects and engineers schedule drawings.
  - Check inverts and sizes of existing pipes prior to the commencement of any work. Report any discrepancies to the engineer and await instructions.
  - The location of services is shown as indicative. This drawing should be read in conjunction with the utilities drawings. No warranty to their accuracy can be given. The contractor shall take all necessary measures to satisfy himself as to the location of the existing services and connection points. Excavation should be undertaken in compliance with HSG47.

**KEY**

- Proposed Surface Water Sewer Pipe
- Exceedance Flows
- Permeable Surface as per architect's details  
Sub-base 350mm Type 3
- Silt Trap
- Existing Combined Water Sewer Pipe

P2	Updated Design	22.08.24	AGCARD
Rev	Details	Date	By / Ctd

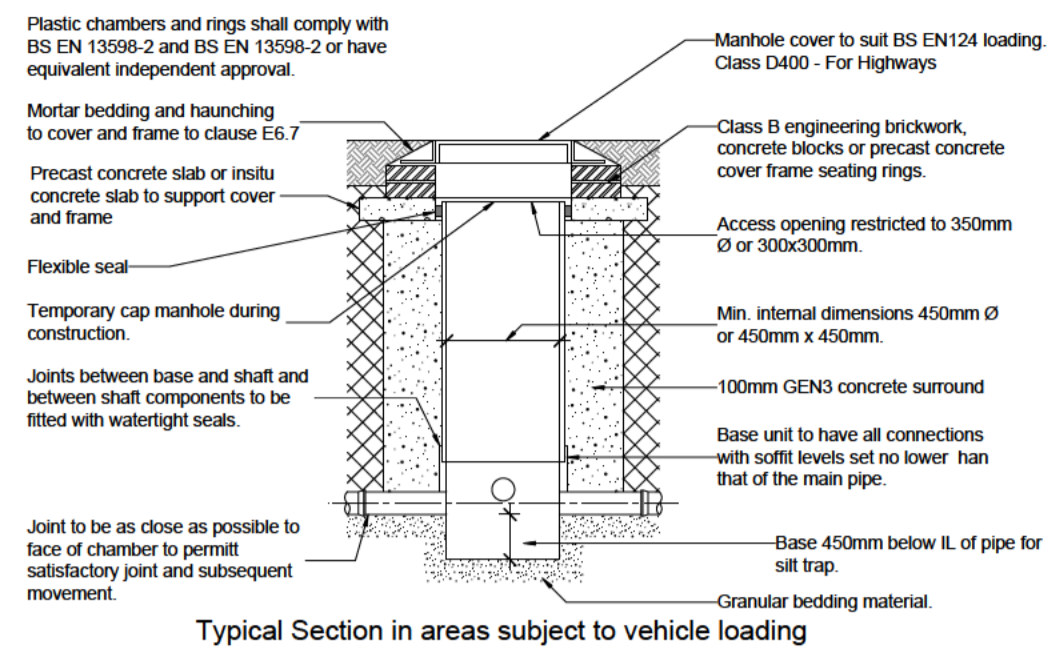
Drawing Status: **PRELIMINARY**



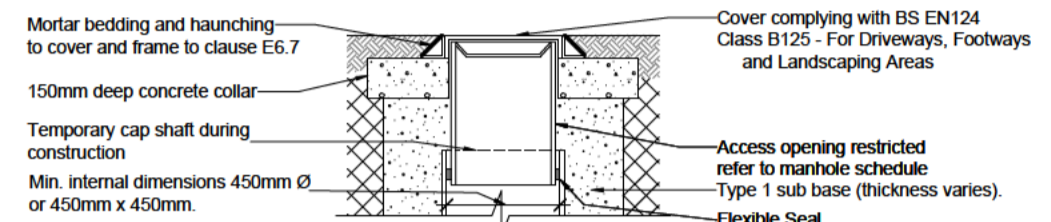
Client: \_\_\_\_\_  
Project: 22&24 St. Annes Road, London Colney, AL2 1LJ  
Drawing: Proposed Drainage Strategy

Drawing Scale Bar			
Drawing scale	Line length	Drawing scale	Line length
1:5	= 0.25 metres	1:200	= 10.0 metres
1:10	= 0.5 metres	1:250	= 12.5 metres
1:20	= 1.0 metres	1:500	= 25.0 metres
1:25	= 1.25 metres	1:1000	= 50.0 metres
1:50	= 2.5 metres	1:1250	= 62.5 metres
1:100	= 5.0 metres	1:2500	= 125 metres

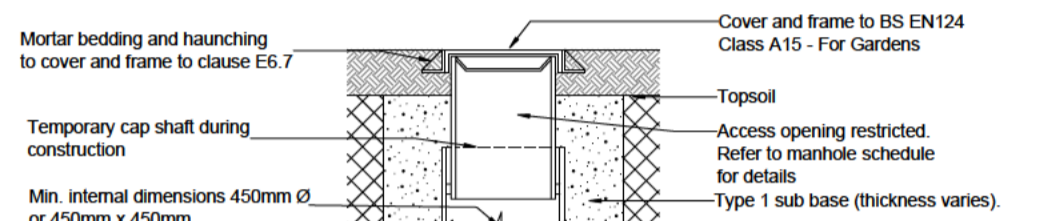
Measure length of line above for checking of scale



Typical Section in areas subject to vehicle loading



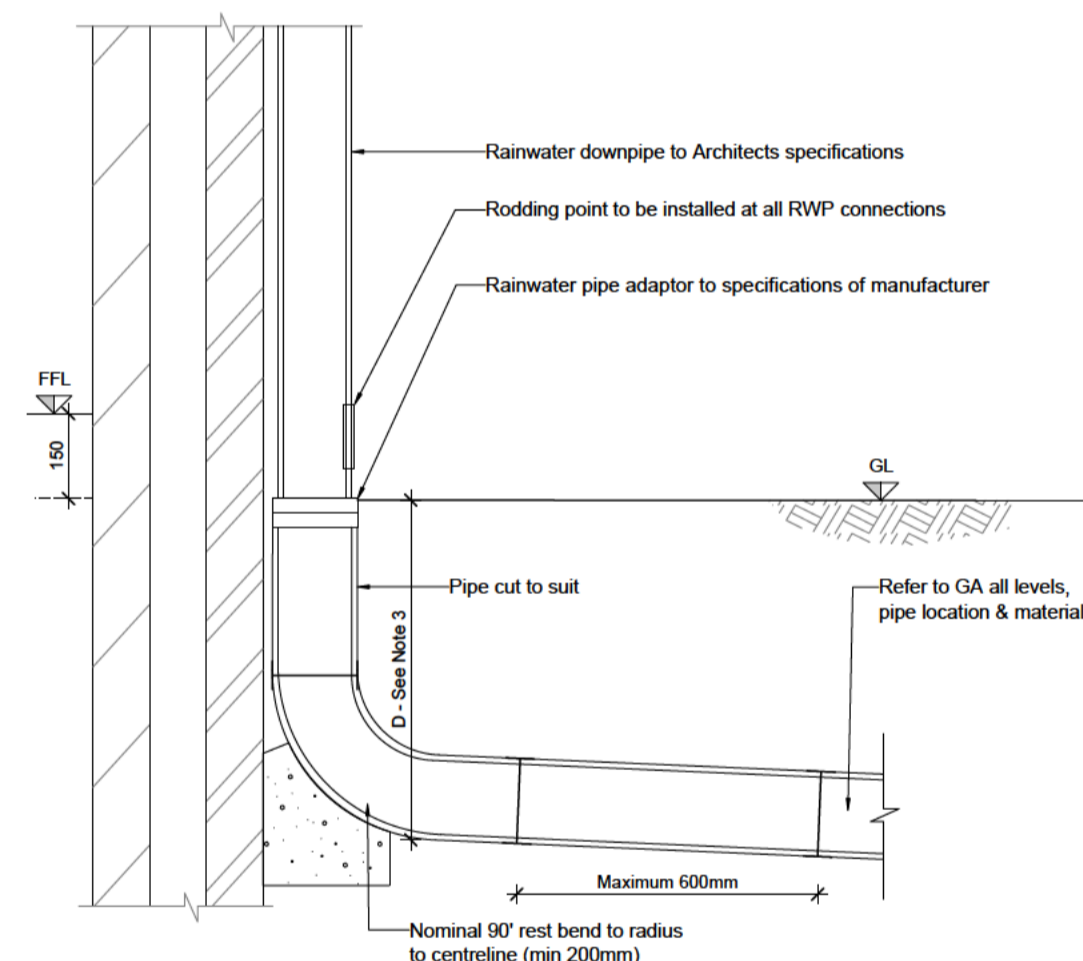
Sited in domestic driveways or footways



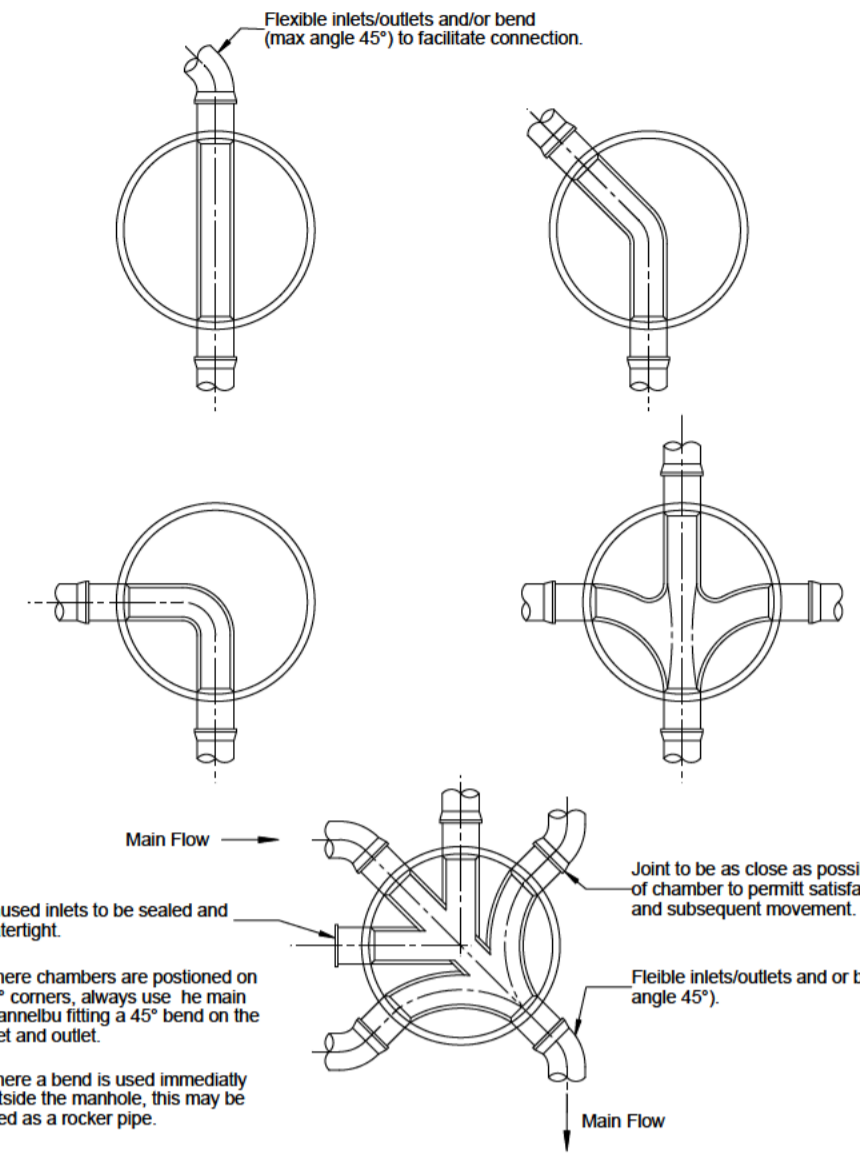
Sited in private garden - No loading

Notes:  
1. Refer to drawing 8193 for base layouts.

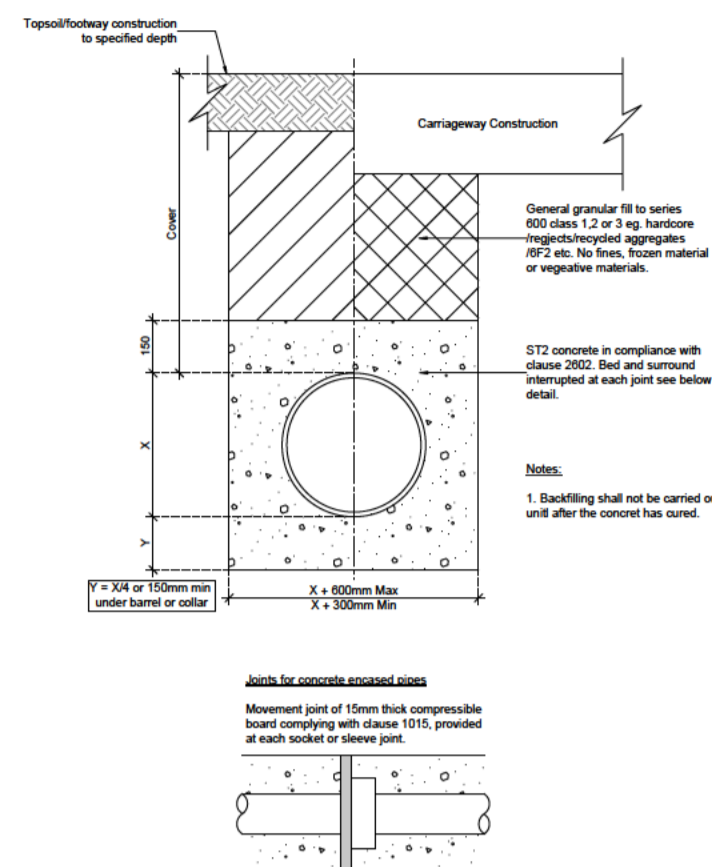
Silt Trap Plastic



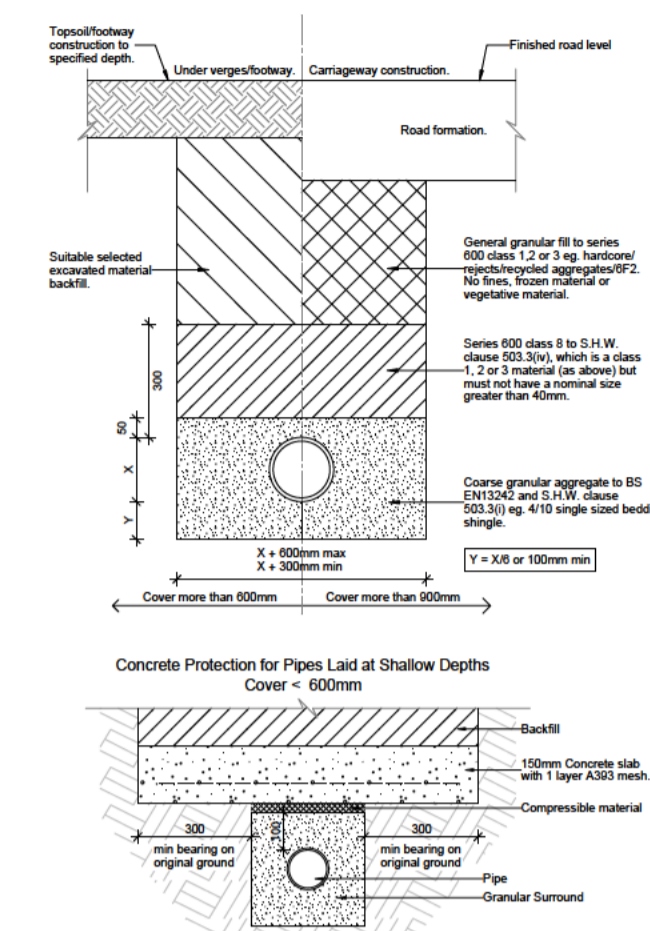
8251 - External Rainwater Pipe Connection Detail



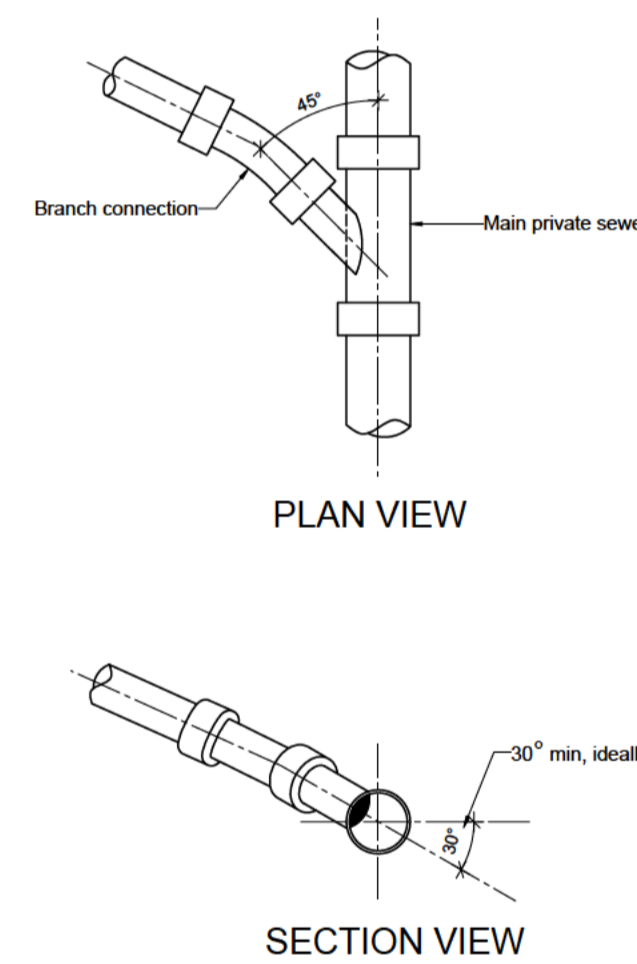
Chamber Type 3 Base Layouts



Pipe Bedding Detail Type Z

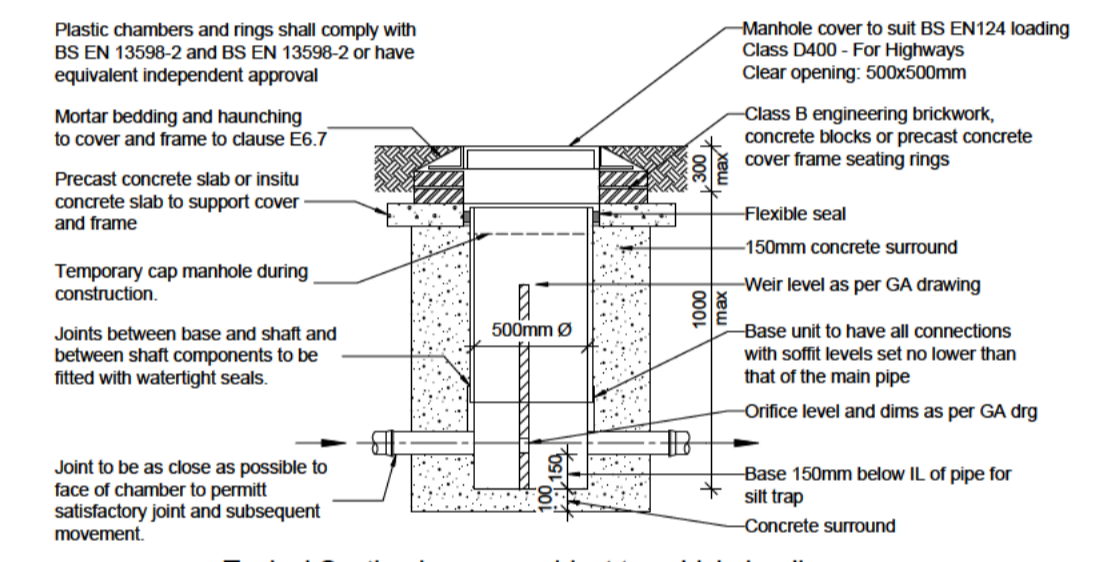


Pipe Bedding Detail Type S

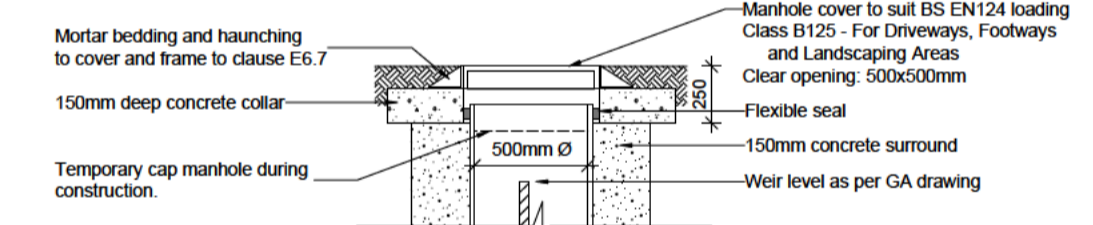


NOTES:  
1. The vertical angle between the connecting pipe and the horizontal should be greater than 0° and not more than 60°.  
2. Where the connection is being made to a sewer with a nominal internal diameter of 300mm or less, connections should be made using 45° angle, or 50° angle, curved square junctions.  
3. Connections made with junction fittings should be made by cutting the existing pipe, inserting the junction fitting and jointing with flexible repair couplings or slip couplers.

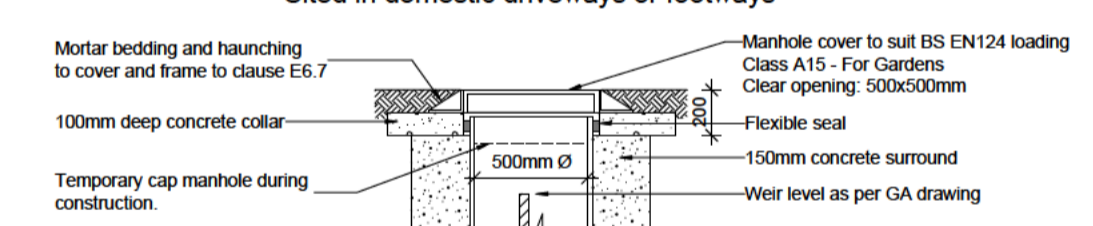
Lateral Connection to private sewer



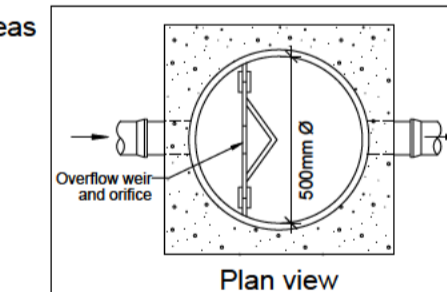
Typical Section in areas subject to vehicle loading



Sited in domestic driveways or footways

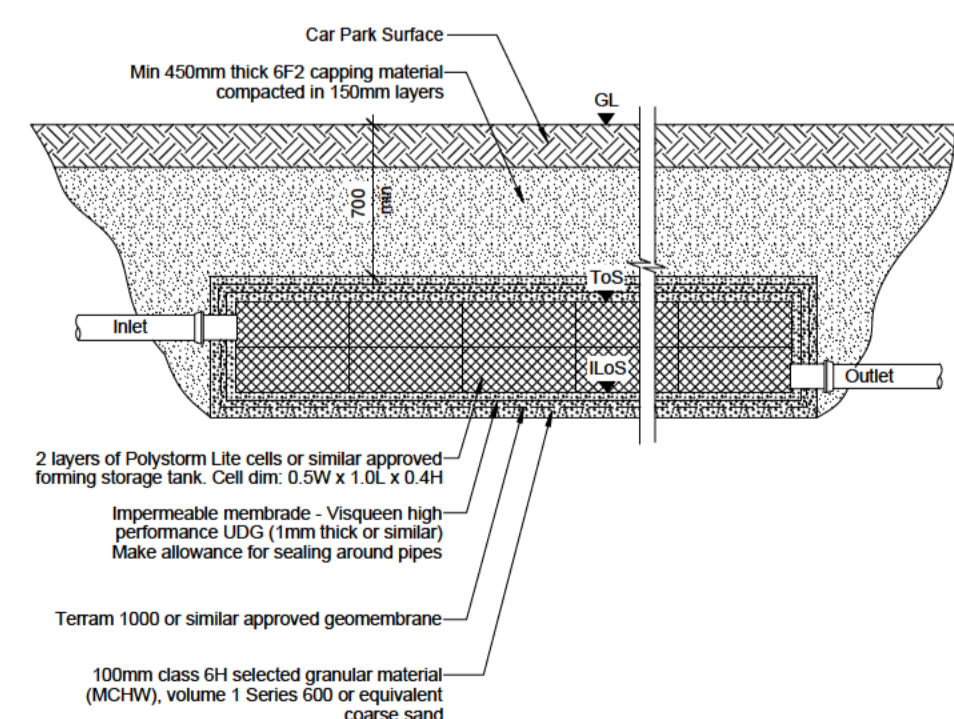


Sited in soft landscaped areas



NOTES:  
1. Refer to GA drg for pipe layout.  
2. Chamber can be fabricated by Selet Environmental UK.

Flow Control -Orifice Plate - Plastic - Type 3



NOTES:  
1. Permeable modular storage cell with 95% minimum void ratio. Ultimate compressive strength of 400kN/m² minimum. Resistant to chemicals likely to be found in rain water and durability of a minimum of 40 years.  
2. Dimensions as applicable to the manufacturers recommendations for given storage requirement UNO.  
3. Air Vents should be provided as per suppliers recommendations  
4. See GA drgs for pipe sizes and layout and IL, ILoS, ToS, GL levels.

Cellular Attenuation System - Landscape Area

GENERAL NOTES

Rev	Details	Date	By	Ctd
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Drawing Status:  
**PRELIMINARY**



Client:  
  
Project:  
22&24 St.Annes Road, London Colney, AL2 1LJ  
Drawing:  
Standard Details