

Construction Noise and Vibration Monthly Report – January 2022

Birmingham City

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Non-Technical Summary

This Noise and Vibration Monitoring Report fulfils HS2 Limited's commitment detailed in the Environmental Minimum Requirements (EMRs), Annex 1, Code of Construction Practice, to present the results of noise and vibration monitoring carried out within Birmingham City during the month of January 2022.

Within this period monitoring was undertaken at the following worksites:

- Noise monitoring was undertaken in the vicinity of the Curzon Street worksite (ref.: CS), where material deliveries and storage, movement of concrete barriers, installation of turnstiles, piling works for ground investigations, excavation and backfilling works, general maintenance works on the platform area, stockpiling, water treatment plant operations, concrete pouring, breakout works and removal of arising stockpiles off-site were underway.
- Noise and vibration monitoring was undertaken in the vicinity of the Twisted Oak Stables worksite (ref.: TOS), where concrete pours, deliveries of tunnel boring machine components, asphaltting of site haul road and installations of bell mouths were underway.
- Noise and vibration monitoring was undertaken in the vicinity of the Washwood Heath Depot worksite (ref.: WWHD), where obstruction removal and platform construction, lining works, brook diversion works, deliveries of water treatment plants, boreholes, bentonite plant operations, construction of diaphragm wall, breakout and crushing works and site widening works and batching plant operations were underway.
- Noise monitoring was undertaken in the vicinity of the SAS13 Bridge Replacement worksite in Washwood Heath (ref.: SAS13), where construction abutment, including steel fixing, shuttering, concrete pouring, laying aggregate, and installation of the bridge deck were underway.

Further works, where monitoring did not take place, were also undertaken at:

- Erskine Street (water utility works);
- Bromford Tunnel and Saltley Viaduct (power utility works);
- Curzon Street (power utility works); and
- Duddleson Mill (water and power utility works).

The HS2 threshold levels for significant noise impacts, which are defined in Information Paper E23 (<https://www.gov.uk/government/publications/hs2-information-papers-environment>), was exceeded on one occasion due to HS2 works during the reporting period.

There were no exceedances of trigger levels as defined in Section 61 consents during the reporting period at any monitoring position.

One complaint was received during the monitoring period. A description of complaint, the results of investigation and any actions taken are detailed in Table 8 of this report..

Abbreviations and Descriptions

The abbreviations, descriptions and project terminology used within this report can be found in Table 1.

Table 1: Table of Abbreviations

Acronym/Term	Definition
$L_{Aeq,T}$	See equivalent continuous sound pressure level
Ambient sound	A description of the all-encompassing sound at a given location and time which will include sound from many sources near and far. Ambient sound can be quantified in terms of the equivalent continuous sound pressure level, $L_{pAeq,T}$
Decibel(s), or dB	Between the quietest audible sound and the loudest tolerable sound there is a million to one ratio in sound pressure (measured in Pascal (Pa)). Because of this wide range, a level scale called the decibel (dB) scale, based on a logarithmic ratio, is used in sound measurement. Audibility of sound covers a range of approximately 0-140dB.
Decibel(s) A-weighted, or dB(A)	The human ear system does not respond uniformly to sound across the detectable frequency range and consequently instrumentation used to measure sound is weighted to represent the performance of the ear. This is known as the 'A weighting' and is written as 'dB(A)'.
Equivalent continuous sound pressure level, or $L_{Aeq,T}$	An index used internationally for the assessment of environmental sound impacts. It is defined as the notional unchanging level that would, over a given period of time (T), deliver the same sound energy as the actual time-varying sound over the same period. Hence fluctuating sound levels can be described in terms of an equivalent single figure value, typically expressed as a decibel level.
Exclusion of data	Measurement of noise levels can be affected by weather conditions such as prolonged periods of rain, winds speeds higher than 5m/s and snow/ice ground cover. Noise levels measured during these periods are considered not representative of normal noise conditions at the site and, for the purposes of this report, are excluded from the assessment of exceedances and calculation of typical noise levels and are also greyed out in charts. Identifiable incongruous noise and vibration events not attributable to HS2 construction noise are also excluded.
Façade	A facade noise level is the noise level 1m in front of a large reflecting surface. The effect of reflection, is to produce a slightly higher (typically +3 dB) sound level than it would be if the reflecting surface was not there.
Free-field	A free-field noise level is the noise level measured at a location where no reflective surfaces, other than the ground, lies within 3.5 metres of the microphone position.
LOAEL	Lowest Observed Adverse Effect Level - the level above which adverse effects on health and quality of life can be detected.
Peak particle velocity, or PPV	Instantaneous maximum velocity reached by a vibrating element as it oscillates about its rest position. The PPV is a simple indicator of perceptibility and risk of damage to structures due to vibration. It is usually measured in mm/s.
SOAEL	Significant Observed Adverse Effect Level - the level above which significant adverse effects on health and quality of life occur.
Sound pressure level	The parameter by which sound levels are measured in air. It is measured in decibels. The threshold of hearing has been set at 0dB, while the threshold of pain is approximately 120dB. Normal speech is approximately 60dB at a distance of 1 metre and a change of 3dB in a time varying sound signal is commonly regarded as being just detectable. A change of 10dB is subjectively twice, or half, as loud.
Vibration dose value, or VDV	An index used to evaluate human exposure to vibration in buildings. While the PPV provides information regarding the magnitude of single vibration events, the VDV provides a measure of the total vibration experienced over a specified period of time (typically 16h daytime and 8h night-time). It takes into account the magnitude, the number and the duration of vibration events and can be used to quantify exposure to continuous, impulsive, occasional and intermittent vibration. The vibration dose value is measured in $m/s^{1.75}$.

1 Introduction

- 1.1.1 HS2 is required to undertake noise (and vibration) monitoring as necessary to comply with the requirements of the High Speed Rail (London-West Midlands) Environmental Minimum Requirements, including specifically Annex 1: Code of Construction Practice, in addition to any monitoring requirements arising from conditions imposed through consents under Section 61 of the Control of Pollution Act, 1974 or through Undertakings & Assurances given to third parties. Such monitoring may be undertaken for the following purposes:
- monitoring the impact of construction works;
 - to investigate complaints, incidents and exceedance of trigger levels; or
 - monitoring the effectiveness of noise and vibration control measures.
- 1.1.2 Monitoring data and interpretive reports are to be provided to each relevant local authority on a monthly basis and shall include a summary of the construction activities occurring, the data recorded over the monitoring period, any complaints received, any periods in exceedance of agreed trigger levels, the results of any investigations and any actions taken or mitigation measures implemented. This report provides vibration data, and interpretation thereof, for monitoring carried out by HS2 within Birmingham City for the period 1st to 31st January 2022.
- 1.1.3 Construction sites in the local authority area where monitoring was undertaken during this period include:
- Curzon Street worksite ref.: CS (see plan 1 in Appendix A) where work activities included:
 - material deliveries and storage;
 - movement of concrete barriers;
 - installation of turnstiles;
 - piling works for ground investigations;
 - excavation works and reinstatement of piling platform;
 - general maintenance works on the platform area and stockpiling;
 - water treatment plant operations;
 - concrete pouring;
 - breakout works of student accommodation foundations;
 - backfilling works; and

- removal of arising stockpiles off-site.
- Twisted Oak Stables worksite, ref.: TOS (see plan 3 in Appendix A) where work activities included:
 - pouring of concrete slabs;
 - deliveries of tunnel boring machine components;
 - Asphalting of the site haul road; and
 - installation of bell mouths.
- Washwood Heath Depot worksite, ref.: WWHD (see plan 2 in Appendix A) where work activities included:
 - removal of obstructions and construction of work platform;
 - lining works of attenuation ponds;
 - works for brook diversion, including removal of obstructions and piling mat construction;
 - deliveries of water treatment plants;
 - delineations of boreholes;
 - bentonite plant operations;
 - construction of the diaphragm wall;
 - breakout works;
 - site widening works, including bailey bridge relocation and compound pond works; and
 - batching plant operations.
- SAS13 Bridge Replacement worksite, ref.: SAS13 (see plan 3 in Appendix A) where work activities included:
 - ongoing construction of abutment, including steel fixing, construction of shuttering and concrete pouring;
 - laying aggregate; and
 - installation of the bridge deck, including steel fixing, installing glass reinforced plastic (GRP) panels and shuttering.

1.1.4 Further work where monitoring did not take place, were also undertaken at the following locations:

- Erskine Street (water utility works);
- Bromford Tunnel and Saltley Viaduct (power utility works);
- Curzon Street (power utility works); and
- Duddlestone Mill (water and power utility works).

1.1.5 The applicable standards, guidance, and monitoring methodology is outlined in the construction noise and vibration monitoring methodology report which can be found at the following location <https://www.gov.uk/government/collections/monitoring-the-environmental-effects-of-hs2>. Noise and vibration monitoring reports for previous months can also be found at this location.

1.2 Measurement Locations

1.2.1 Six noise and three vibration monitoring installations were active in January in the Birmingham City area. Table 2 summarises the position of noise and vibration monitoring installations within the Birmingham City area in January 2022.

1.2.2 Maps showing the position of noise and vibration monitoring installations are presented in Appendix B.

Table 2: Monitoring Locations

Worksite Reference	Measurement Reference	Address
Curzon Street (CS)	CS-N1	Curzon Street, Birmingham
Twisted Oak Stables (TOS)	TOS-N1	B4118-Birmingham Road, Water Orton, Birmingham
	TOS-V1	B4118-Birmingham Road, Water Orton, Birmingham
Washwood Heath Depot (WWHD)	WWHD-N1	Drews Lane, Birmingham
	WWHD-V1	Drews Lane, Birmingham
	WWHD-N2	Common Lane, Birmingham
	WWHD-V2	Common Lane, Birmingham
SAS13 Bridge Replacement (SAS13)	SAS13-N1 (East)	Taroni Avenue, off Aston Church Road, Birmingham
	SAS13-N2 (West)	Heartlands Parkway, Nechells, Birmingham

2 Summary of Results

2.1 Summary of Measured Noise and Vibration Levels

- 2.1.1 Table 3 presents a summary of the measured noise levels at each monitoring location over the reporting period. The $L_{Aeq,T}$ is presented for each of the relevant time periods averaged over the calendar month, along with the highest single period $L_{Aeq,T}$ that was found to occur within the month.

Table 3: Summary of Measured dB L_{Aeq} Data over the Monitoring Period

Worksite Reference	Measurement Reference	Site Address	Free-field or Façade measurement	Weekday Average L _{Aeq,T} (highest day L _{Aeq,T})					Saturday Average L _{Aeq,T} (highest day L _{Aeq,T})					Sunday / Public Holiday Average L _{Aeq,T} (highest day L _{Aeq,T})	
				0700 - 0800	0800 - 1800	1800 - 1900	1900 - 2200	2200 - 0700	0700 - 0800	0800 - 1300	1300 - 1400	1400 - 2200	2200 - 0700	0700 - 2200	2200 - 0700
CS	CS-N1	Curzon Street, Birmingham	Free-field	65.7 (66.9)	67.7 (69.8)	65.7 (68.1)	64.0 (67.2)	61.4 (66.2)	61.7 (63.2)	64.9 (66.0)	64.9 (66.2)	64.6 (66.8)	61.4 (64.4)	63.3 (69.4)	60.9 (64.4)
TOS	TOS-N1	B4118-Birmingham Road, Water Orton	Free-field	66.5 (69.5)	68.1 (77.5)	65.6 (70.5)	64.9 (69.5)	63.5 (69.2)	64.5 (68.5)	69.0 (71.0)	66.1 (69.2)	65.4 (69.8)	61.2 (65.6)	66.0 (70.1)	63.2 (68.0)
WWHD	WWHD-N1	Drews Lane, Birmingham	Free-field	59.0 (62.5)	61.4 (63.6)	56.7 (60.4)	56.8 (60.5)	55.7 (70.2)	54.0 (58.5)	55.5 (60.1)	55.7 (59.5)	55.4 (60.0)	51.8 (56.6)	54.1 (60.3)	55.5 (62.5)
	WWHD-N2	Common Lane, Birmingham	Free-field	56.4 (63.5)	58.2 (62.8)	53.9 (59.3)	54.7 (68.7)	53.9 (70.8)	50.1 (56.9)	51.8 (55.2)	53.5 (57.9)	53.8 (57.9)	50.6 (54.8)	51.4 (57.9)	51.5 (61.0)
SAS13	SAS13-N1 (East)	Taroni Avenue, off Aston Church Road	Free-field	63.4 (67.1)	67.1 (69.6)	67.1 (69.6)	65.7 (69.4)	62.3 (71.7)	61.0 (d63.3)	64.7 (67.4)	67.0 (69.1)	67.7 (73.5)	64.8 (74.8)	65.8 (72.9)	62.2 (67.7)
	SAS13-N2 (West)	Heartlands Parkway, Nechells	Free-field	58.8 (61.9)	61.2 (64.2)	60.3 (63.2)	59.5 (61.6)	56.5 (67.5)	55.3 (58.5)	58.3 (60.6)	60.2 (62.1)	60.3 (62.2)	57.8 (67.1)	59.1 (63.5)	56.9 (64.0)

- 2.1.2 Table 4 presents a summary of the measured vibration levels at each monitoring location over the reporting period. The highest component PPV measured during periods of works along any axis is presented in the table.

Table 4: Summary of Measured Component PPV Data over the Monitoring Period

Worksite Reference	Measurement Reference	Monitor Address	Highest PPV measured in any axis, mm/s
TOS	TOS-V1	B4118-Birmingham Road, Water Orton, Birmingham	5.95 (X-axis)*
WWHD	WWHD-V1	Drews Lane, Birmingham	3.72 (X-axis)*
WWHD	WWHD-V2	Common Lane, Birmingham	1.54 (Y-axis)

* Higher vibration levels are due to machinery working near to the monitoring equipment. The nearest sensitive receptor is further away and therefore the levels at the receptor will be lower.

- 2.1.3 Appendix C presents graphs of the noise and vibration monitoring data over the month for each of the measurement locations. Noise data presented consists of the hourly L_{Aeq} values and, where relevant, the $L_{Aeq,T}$ values (where the time period T has been taken to be the averaging period as specified in Table 1 of HS2 Information Paper E23). Vibration data presented consist of hourly PPV values. The full data set for the monitoring equipment can be found at the following location:
<https://data.gov.uk/dataset/24542ae7-dd44-444f-b259-871c4cc43b5e/environmental-monitoring-data>.

2.2 Exceedances of the LOAEL and SOAEL

- 2.2.1 The lowest observed adverse effect level (LOAEL) is defined in the Planning Practice Guidance – Noise (PPG) as the level above which "noise starts to cause small changes in behaviour and/or attitude, e.g. turning up volume of television; speaking more loudly; where there is no alternative ventilation, having to close windows for some of the time because of the noise. Potential for some reported sleep disturbance. Affects the acoustic character of the area such that there is a perceived change in the quality of life".
- 2.2.2 The significant observed adverse effect level (SOAEL) is defined in the 'Planning Practice Guidance – Noise' as the level above which "noise causes a material change in behaviour and/or attitude, e.g. avoiding certain activities during periods of intrusion; where there is no alternative ventilation, having to keep windows closed most of the time because of the noise. Potential for sleep disturbance resulting in difficulty in getting to sleep, premature awakening and difficulty in getting back to sleep. Quality of life diminished due to change in acoustic character of the area."

- 2.2.3 HS2 Phase One Information Paper E23: Control of Construction Noise and Vibration sets out the LOAELs and SOAELs for construction noise.
- 2.2.4 Where reported construction noise levels exceed the LOAEL and SOAEL, relevant periods will be identified. Summary statistics to evaluate ongoing qualification for noise insulation and temporary rehousing are also presented where relevant.
- 2.2.5 Table 5 presents a summary of recorded exceedances of the LOAEL and SOAEL at each measurement location over the reporting period, including the number of exceedances during each time period.

Table 5: Summary of Exceedances of LOAEL and SOAEL

Worksite Reference	Measurement Reference	Site Address	Day (Weekday, Saturday, Sunday, Night)	Time period	Number of exceedances of LOAEL	Number of exceedances of SOAEL
CS	CS-N1*	Curzon Street, Birmingham	All days	All periods	No exceedance	No exceedance
TOS	TOS-N1*	B4118-Birmingham Road, Water Orton, Birmingham	Weekdays	0800-1800	1	1
WWHD	WWHD-N1*	Drews Lane, Birmingham	All days	All periods	No exceedance	No exceedance
WWHD	WWHD-N2*	Common Lane, Birmingham	All days	All periods	No exceedance	No exceedance
SAS13	SAS13-N1 (East)*	Taroni Avenue, off Aston Church Road, Birmingham	All days	All periods	No exceedance	No exceedance
SAS13	SAS13-N2 (West)*	Heartlands Parkway, Nechells, Birmingham	All days	All periods	No exceedance	No exceedance

* A distance correction has been applied when calculating exceedances of the LOAEL and SOAEL.

- 2.2.6 One exceedance of the LOAEL was recorded across the Twisted Oak Stables worksite during working core hours.
- 2.2.7 For the purpose of assessing eligibility for noise insulation or temporary rehousing, multiple exceedances of the SOAEL in a 24-hour period would be counted as a single

exceedance during that day. Over the reporting period, the overall number of SOAEL exceedances at each measurement location is shown in Table 6 and may be lower than the total sum of individual exceedances reported in Table 5 for each location.

Table 6: Summary of Total Exceedances of SOAEL

Worksite Reference	Measurement Reference	Monitor Address	Total of SOAEL exceedances in the month
TOS	TOS-N1	B4118-Birmingham Road	1

- 2.2.8 One exceedance of the SOAEL was recorded across the Twisted Oak Stables worksite during one weekday core hours period.

2.3 Exceedances of Trigger Level

- 2.3.1 Table 7 provides a summary of exceedances of the S61 trigger vibration levels determined to be due to HS2 related construction vibration measured during the reporting period, along with the findings of any investigation.

Table 7: Summary of Exceedances of Trigger Levels

Complaint Reference Number (if applicable)	Worksite Reference	Date and Time Period	Identified Source	Results of Investigation (including noise monitoring results)	Actions Taken
-	-	-	-	-	-

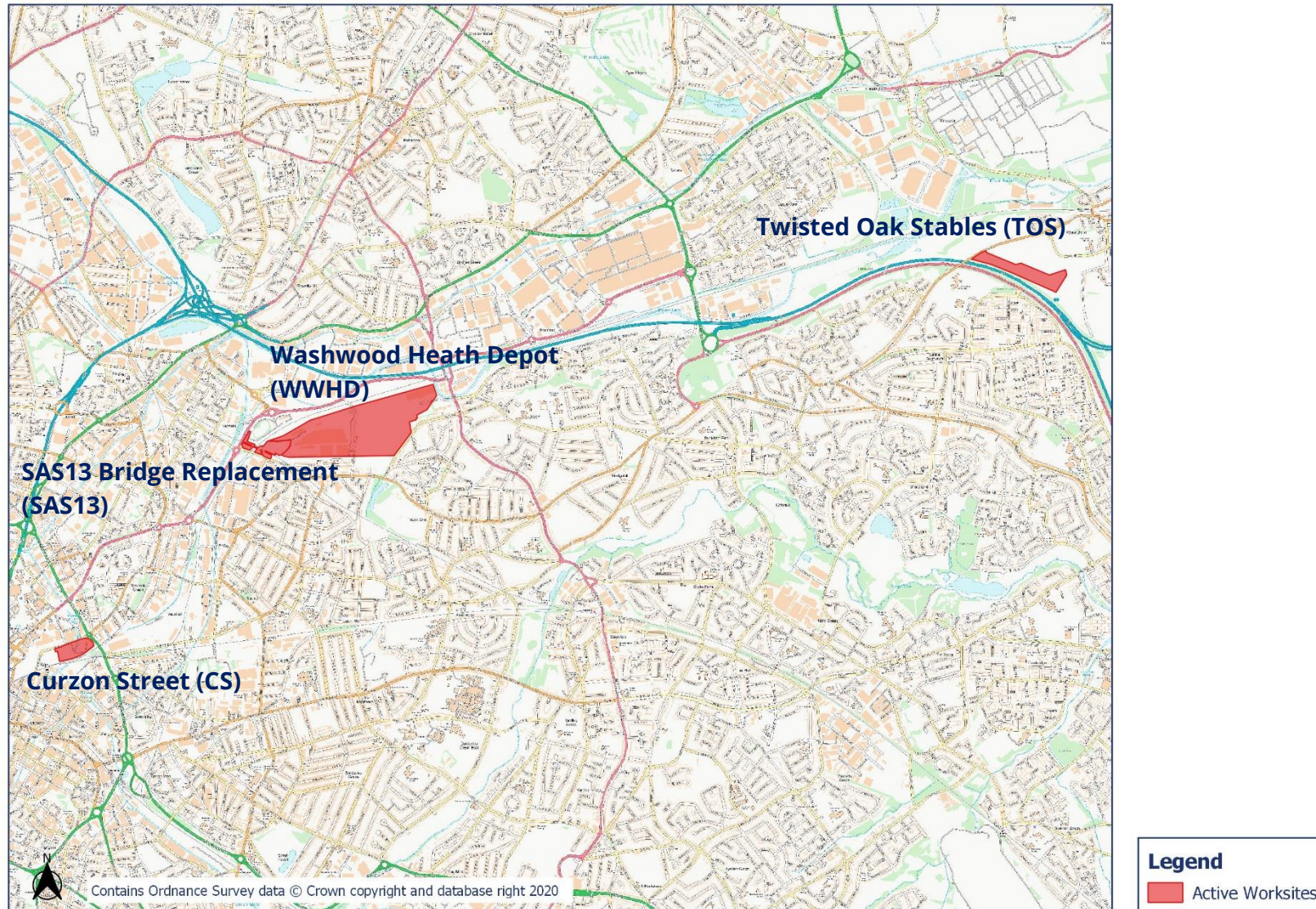
2.4 Complaints

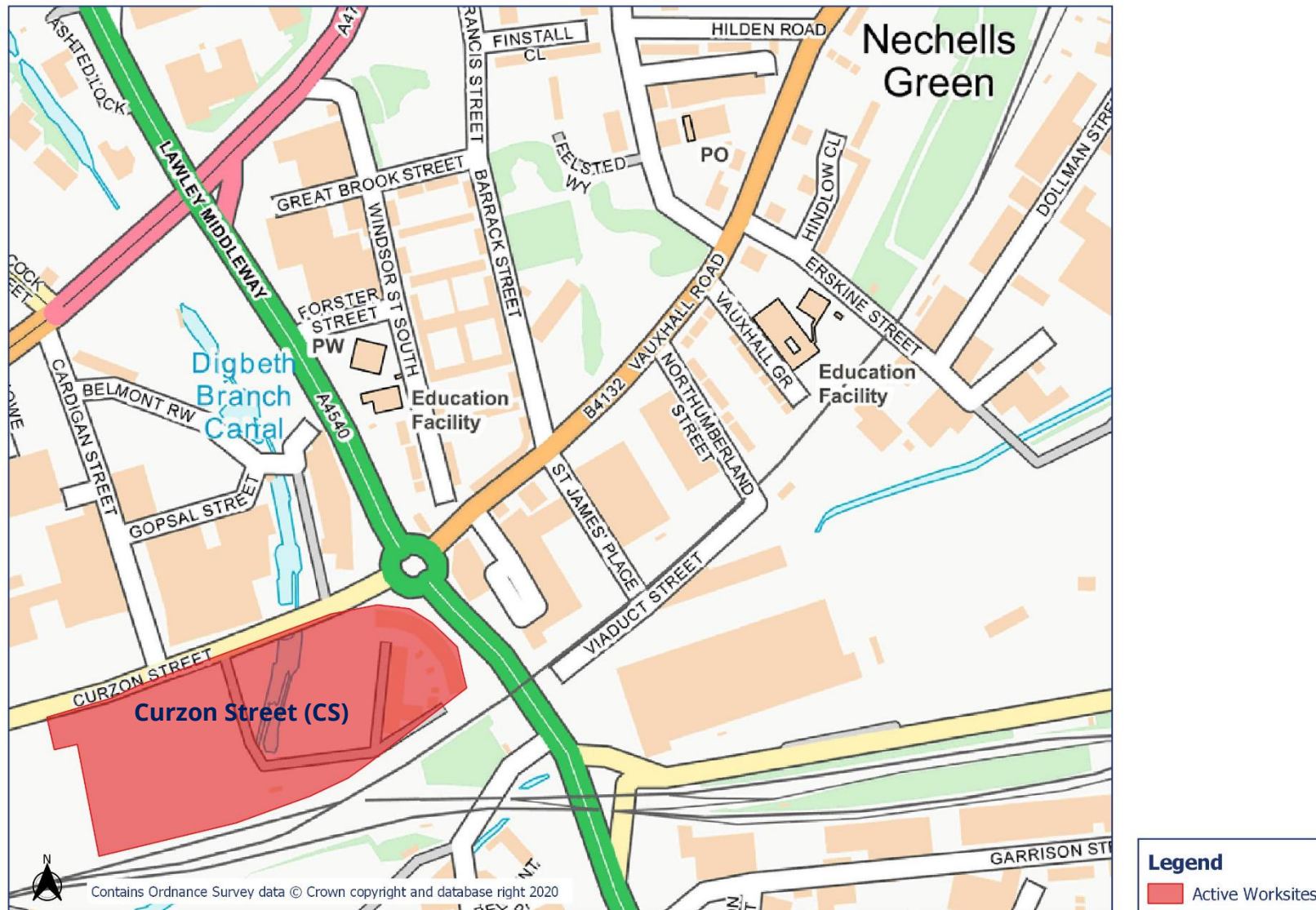
- 2.4.1 Table 8 provides a summary of complaint information related to noise and vibration received during the reporting period, along with the findings of any investigation.

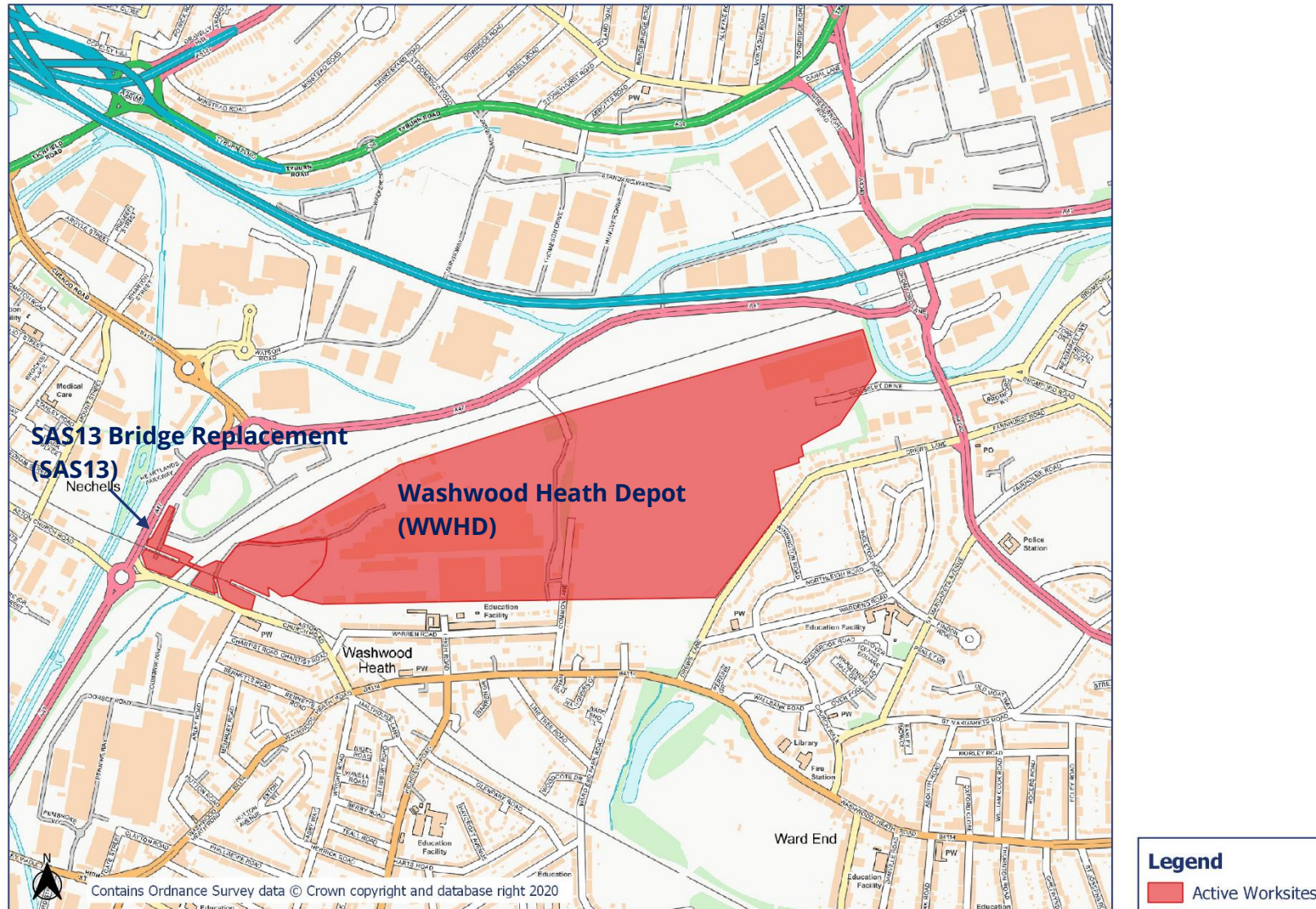
Table 8: Summary of Complaints

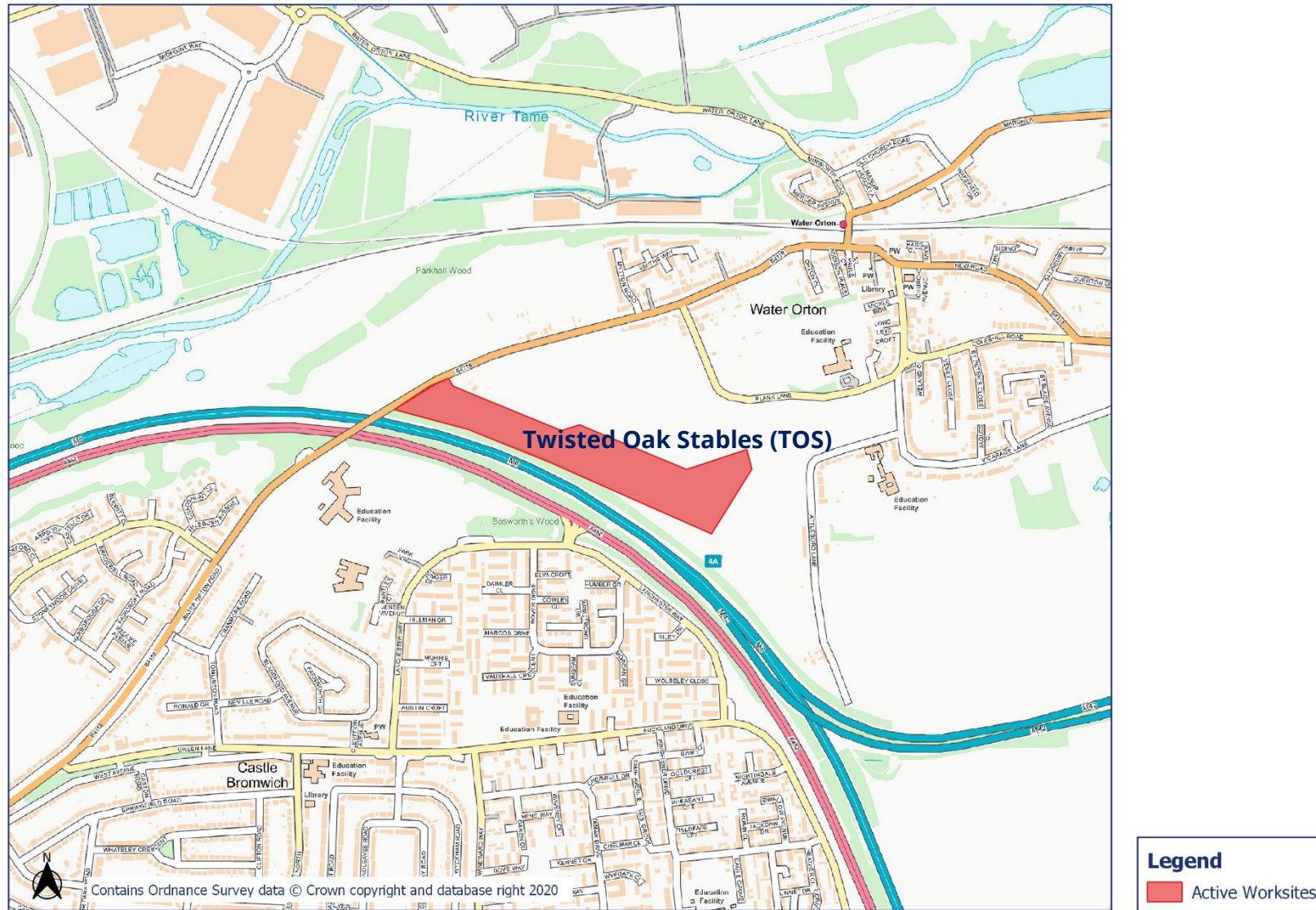
Complaint Reference Number	Worksite Reference	Description of Complaint	Results of Investigation	Actions Taken
HS2-22-43240-C	WWHD	Complaint regarding noise disturbance due to alarms going on during evening and early hours.	On-going	On-going

Appendix A Site Locations

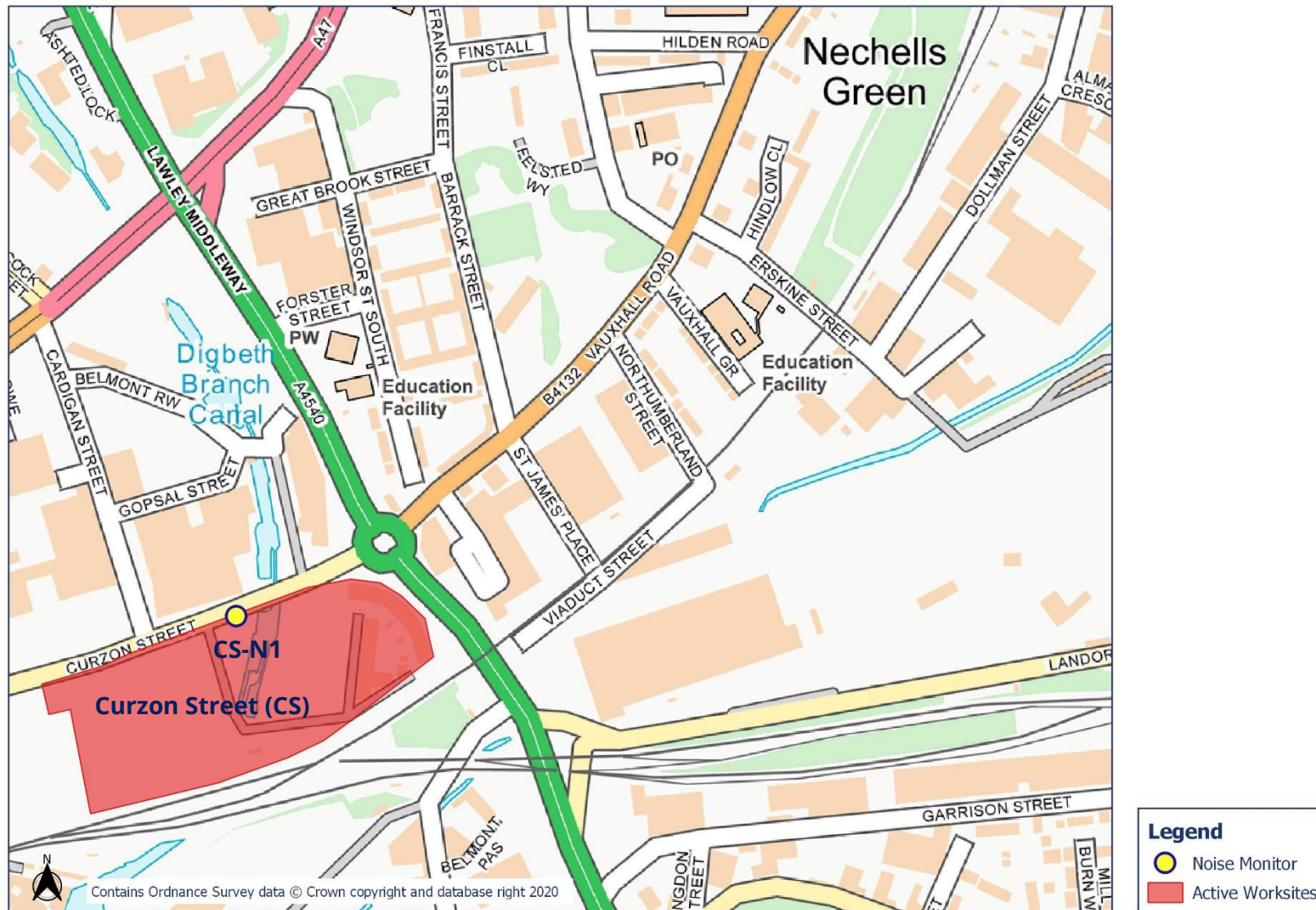


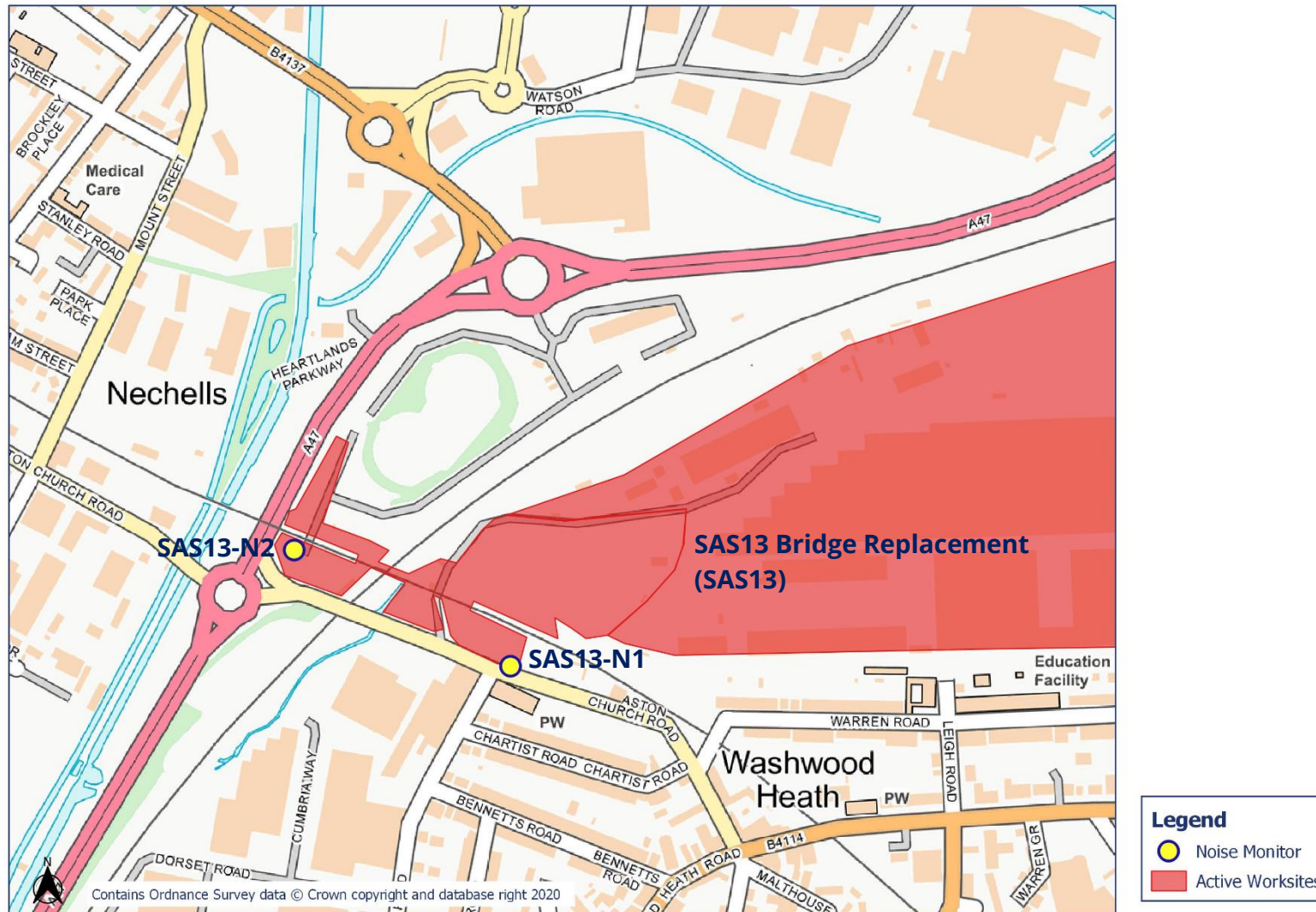


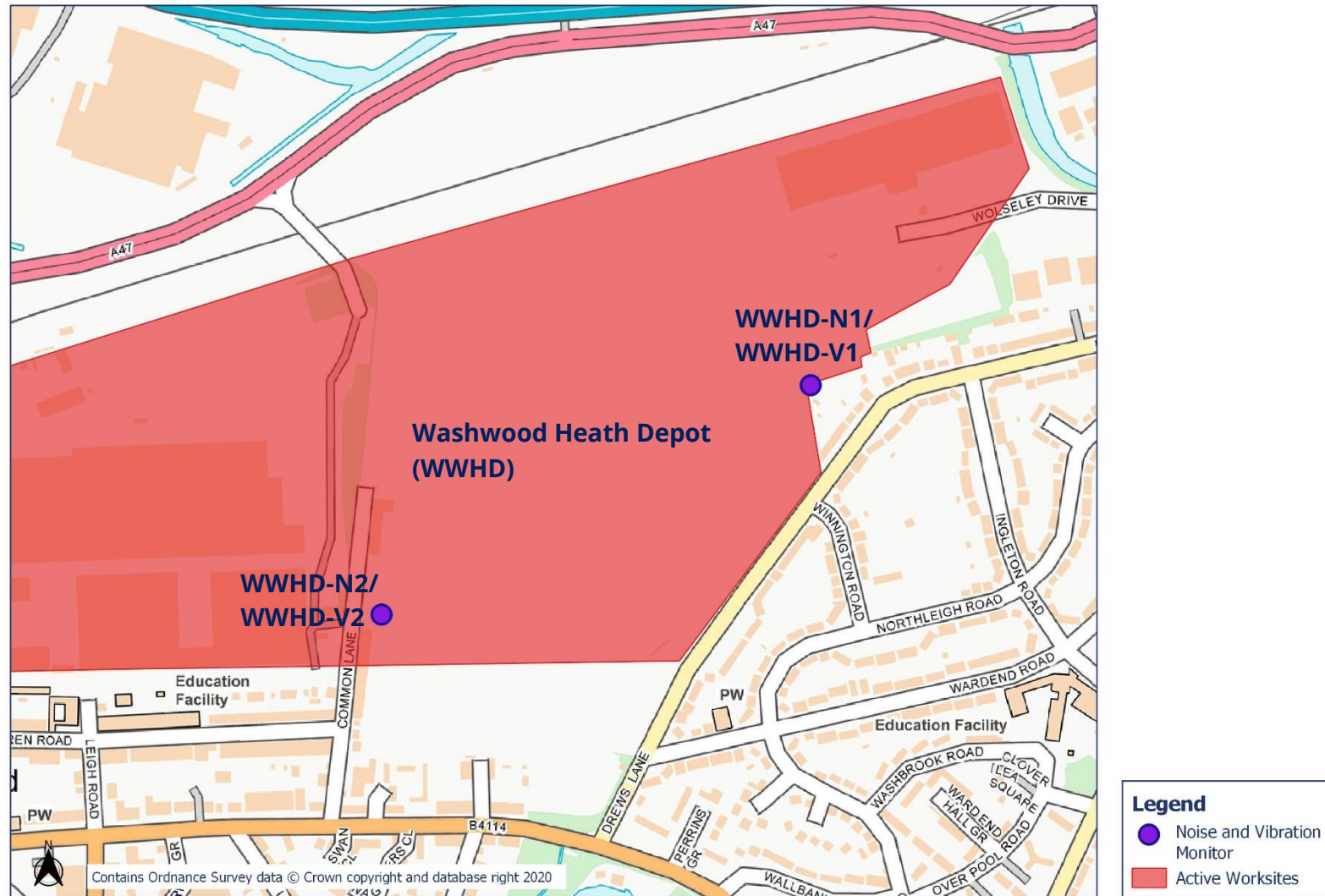


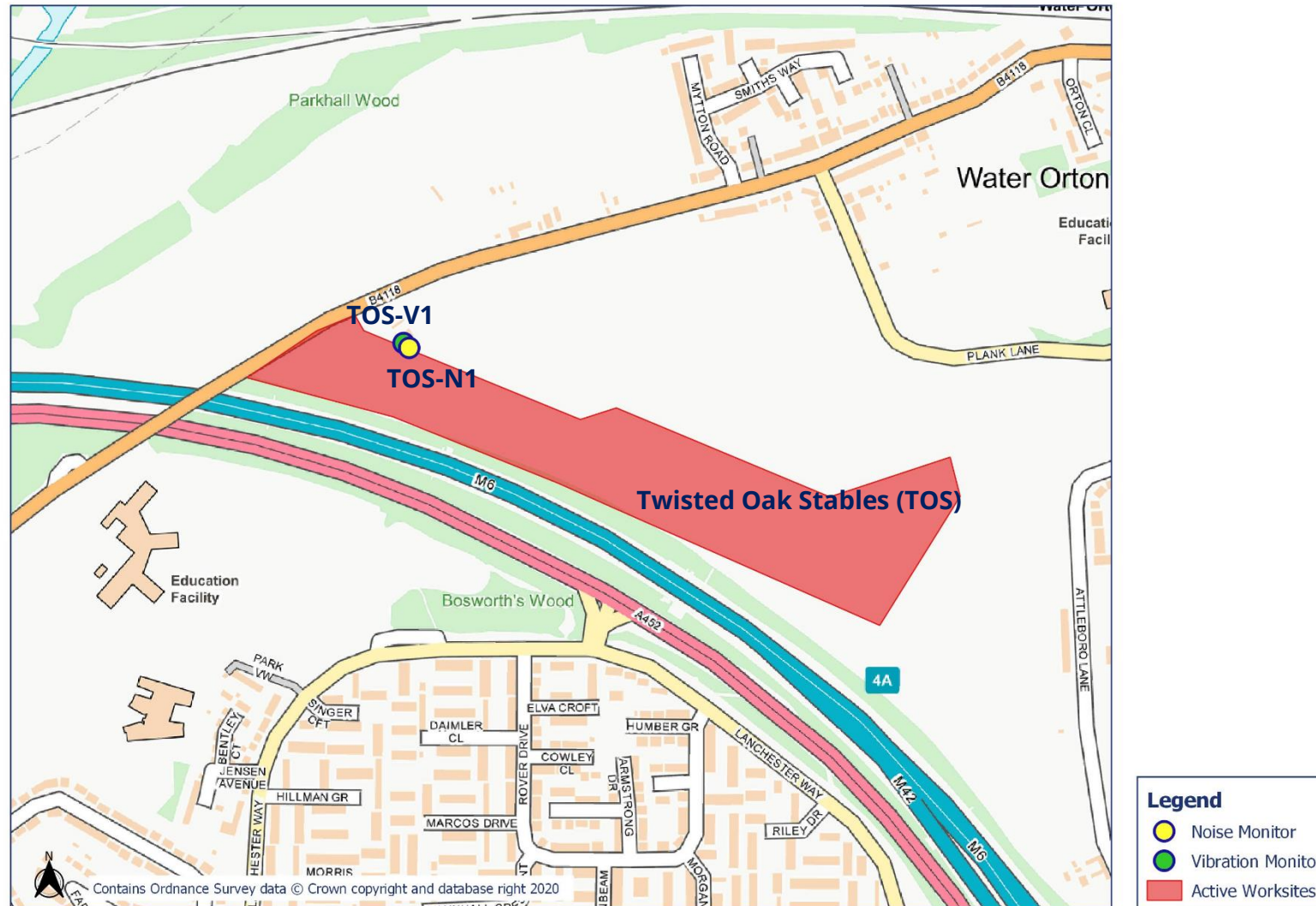


Appendix B Monitoring Locations







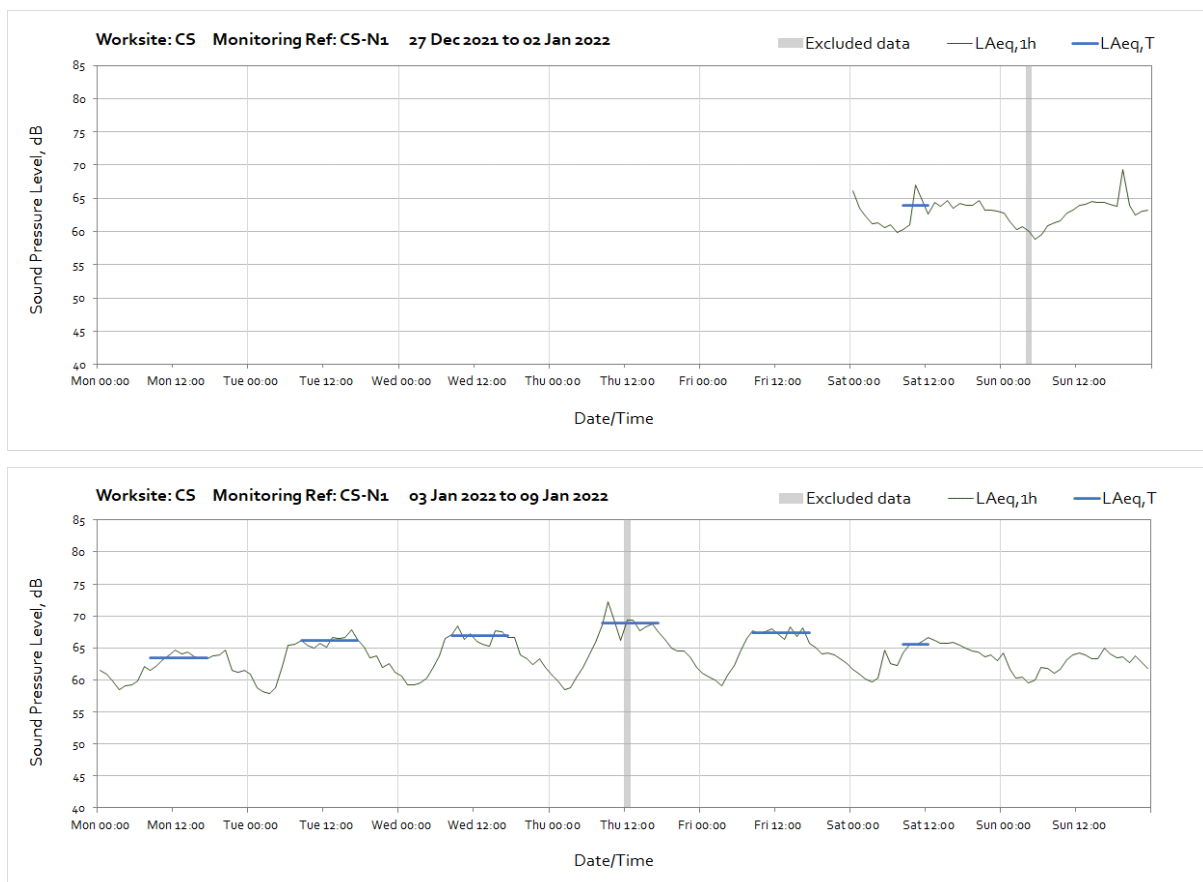


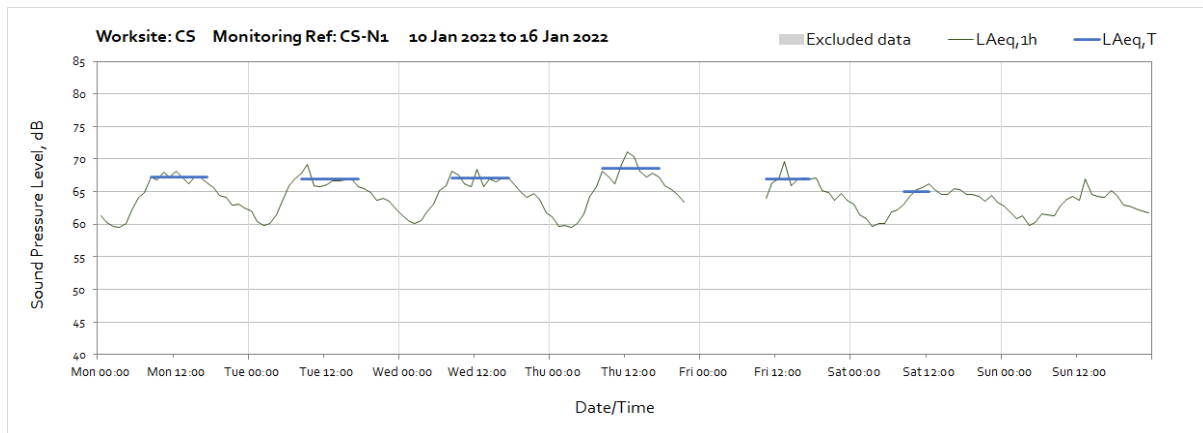
Appendix C Data

Noise

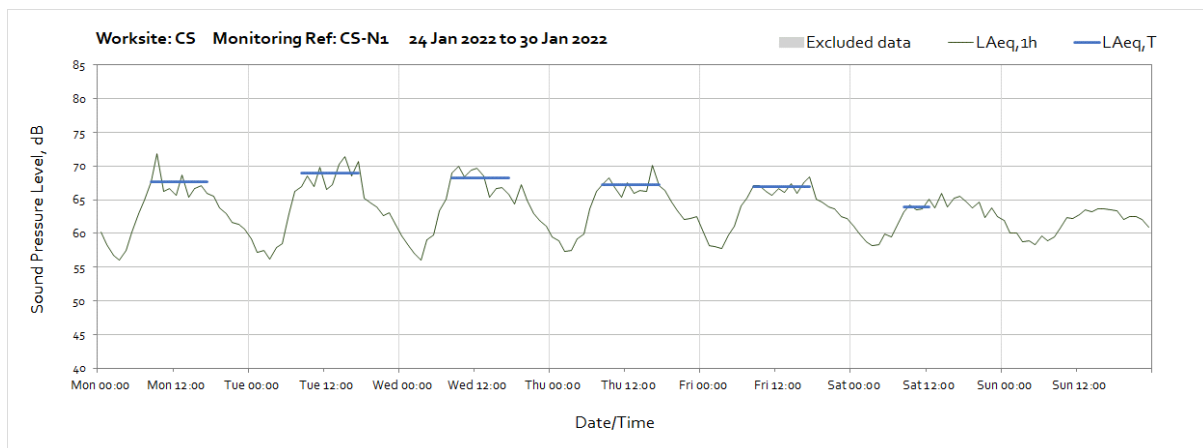
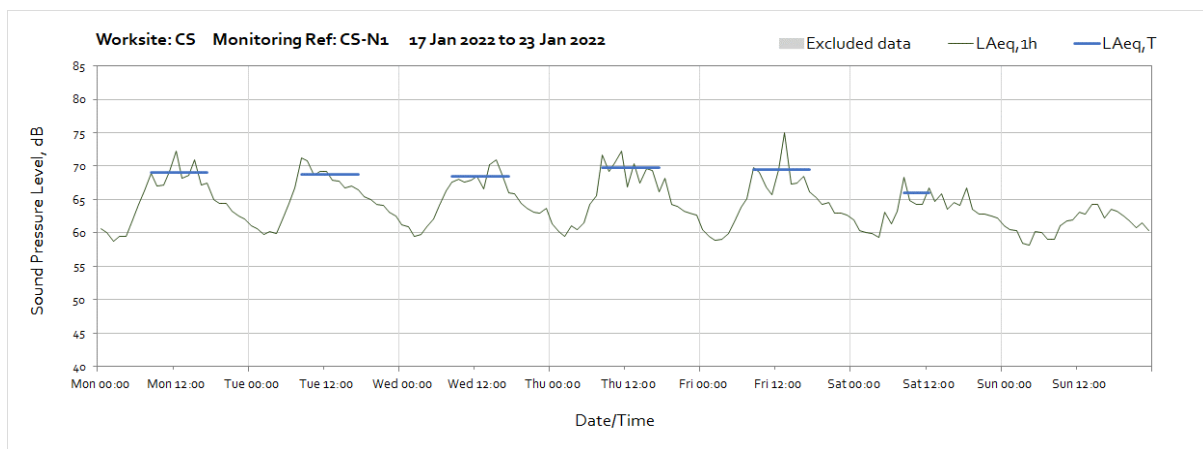
The following graphs show the hourly measured ambient noise level $L_{Aeq,1h}$ and, where relevant, the averaged noise level $L_{Aeq,T}$ values, where the time period T is as specified in Table 1 of HS2 Information Paper E23. Periods with adversely weather affected noise levels are greyed out and have been excluded from the calculation of the $L_{Aeq,T}$ values in Table 3 of the main report.

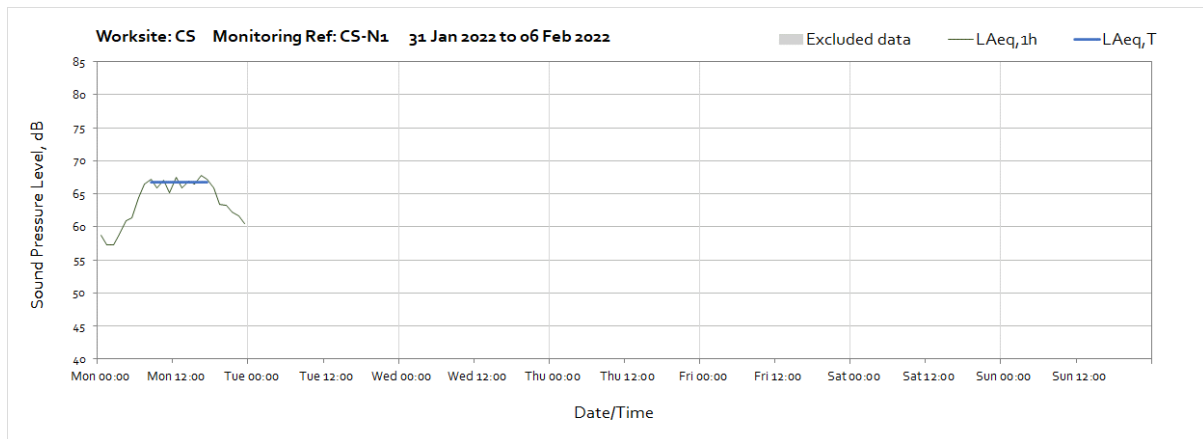
Worksite: Curzon Street (CS) – Monitoring Ref: CS-N1



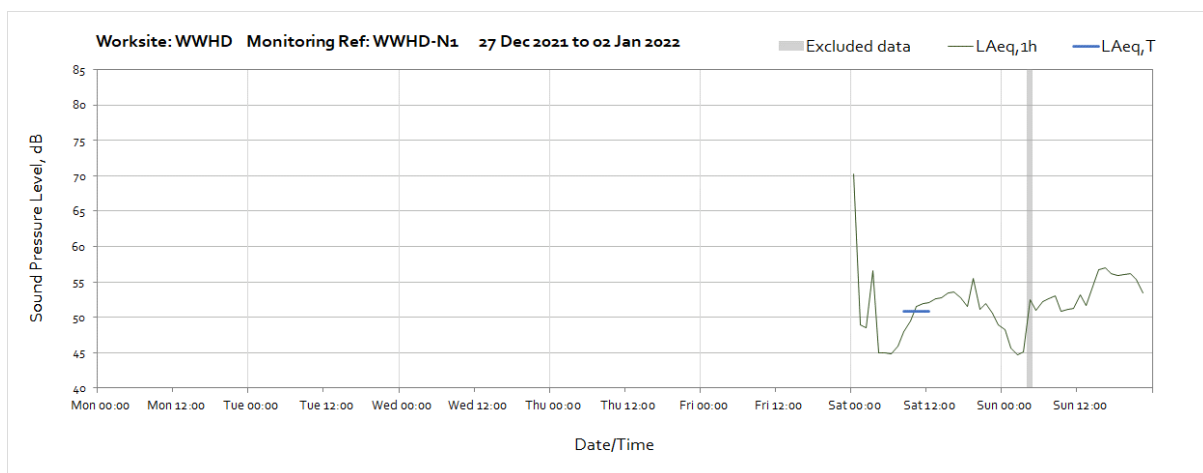


Note: Missing data between 22:00 on Thursday 13th and 10:00 on Friday 14th January 2022 was due to battery falling below required voltage limit caused by prolonged insufficient sunlight.

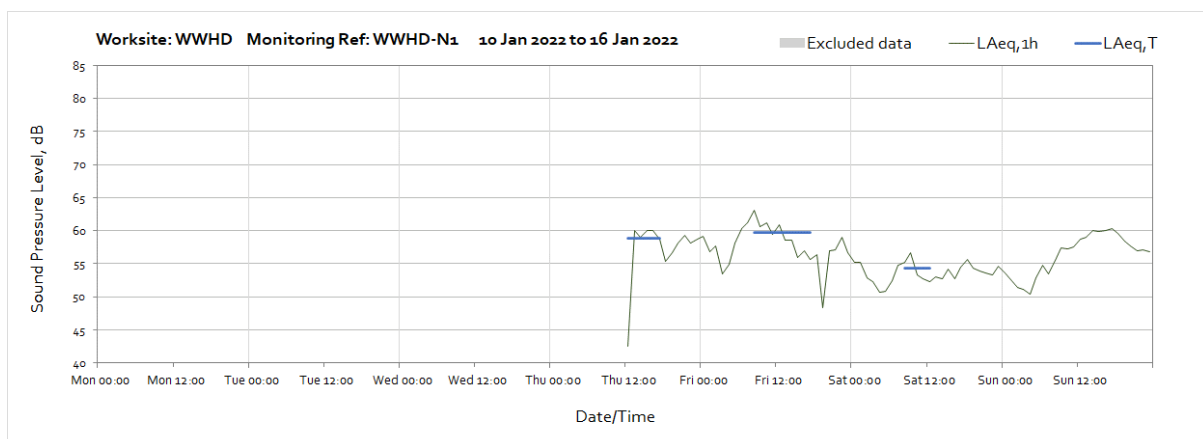




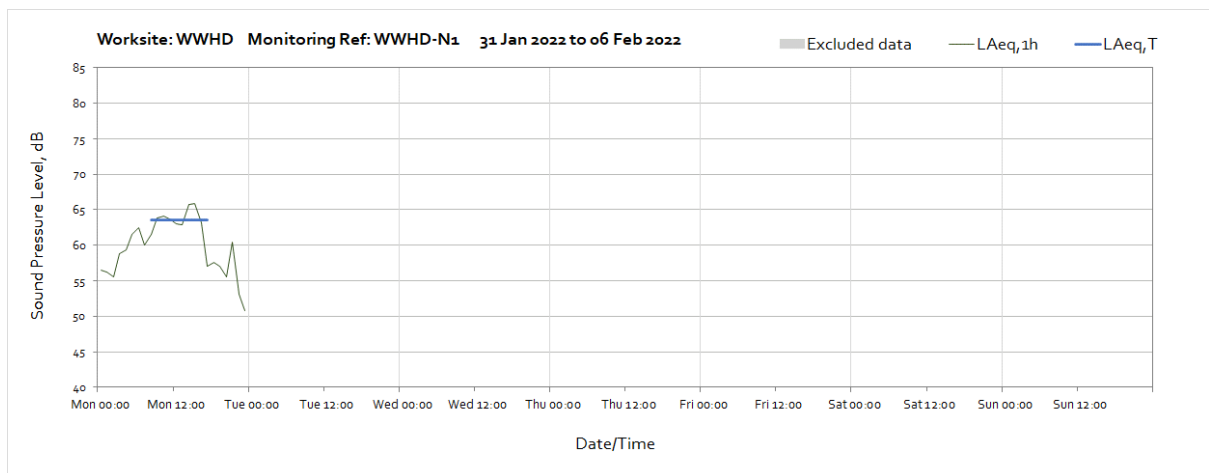
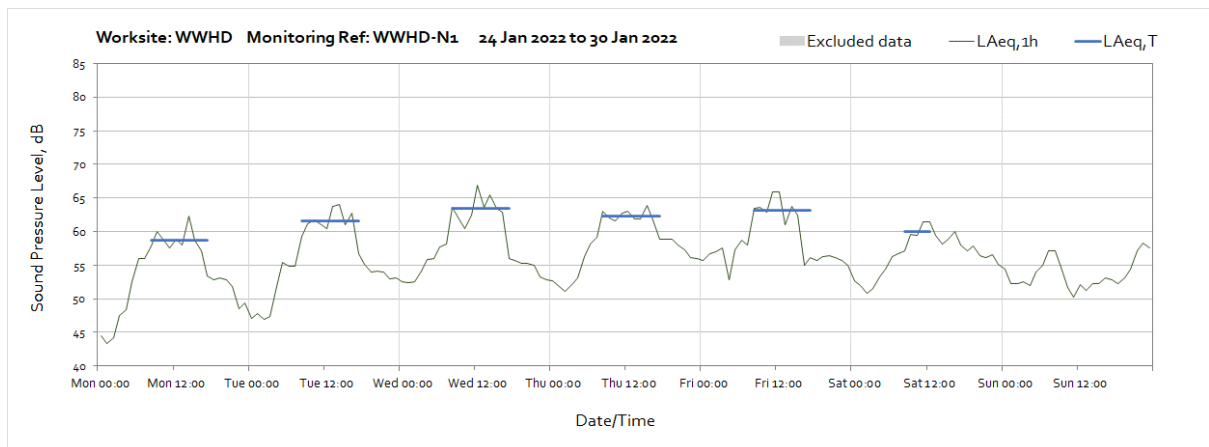
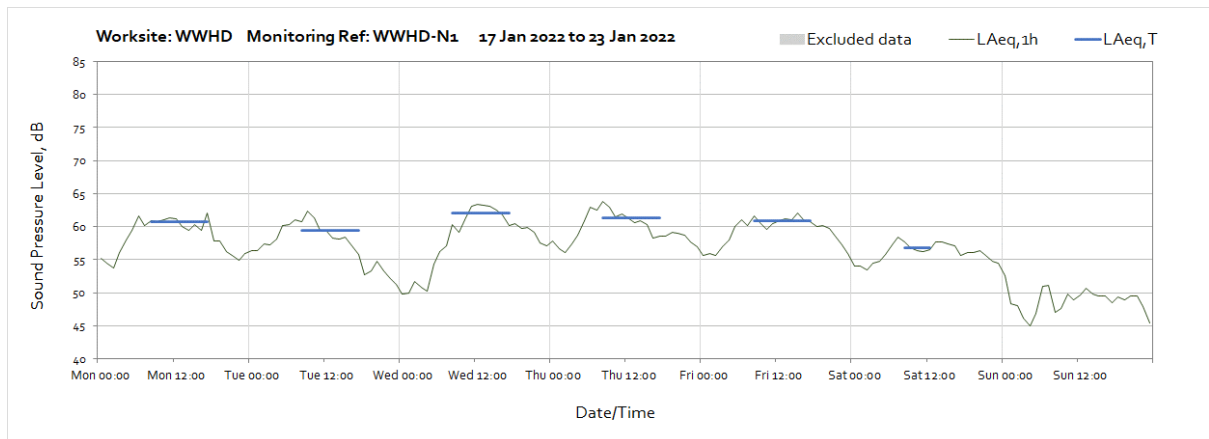
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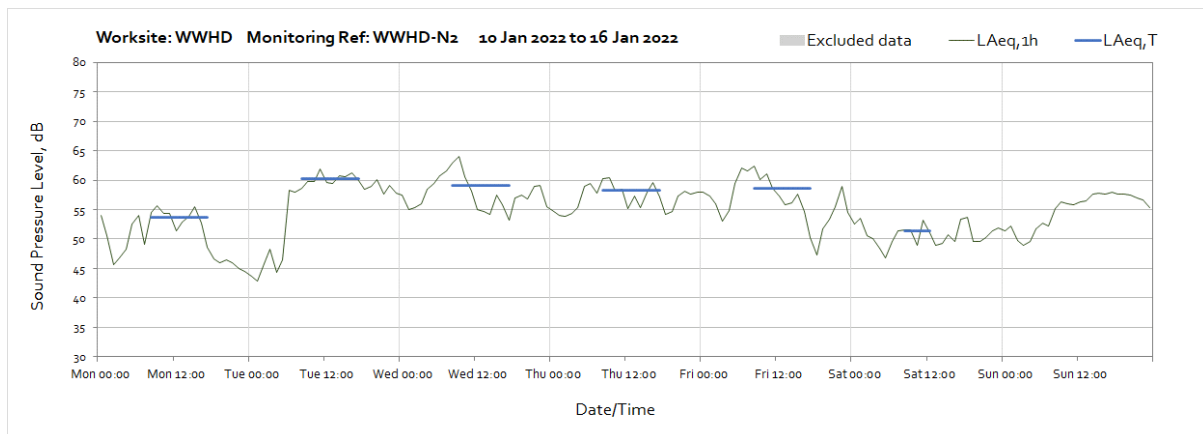
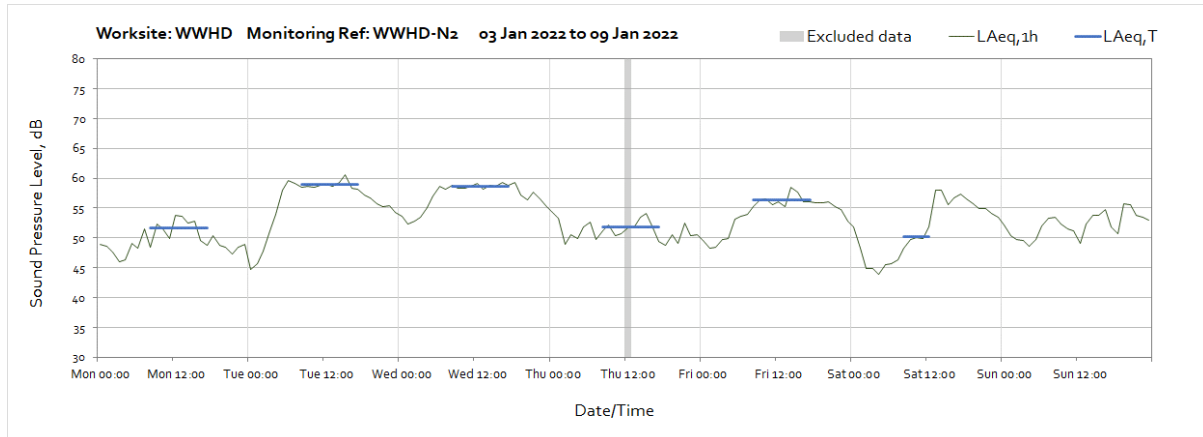
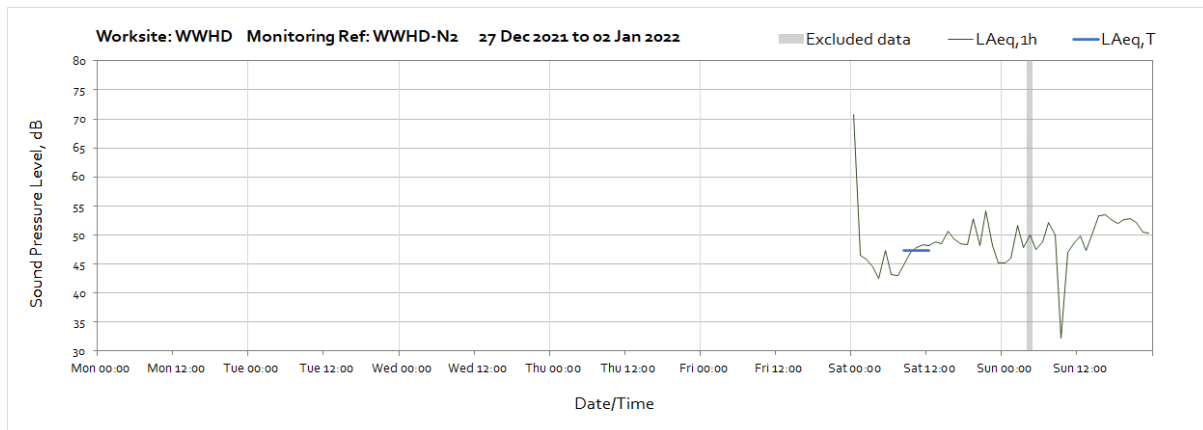
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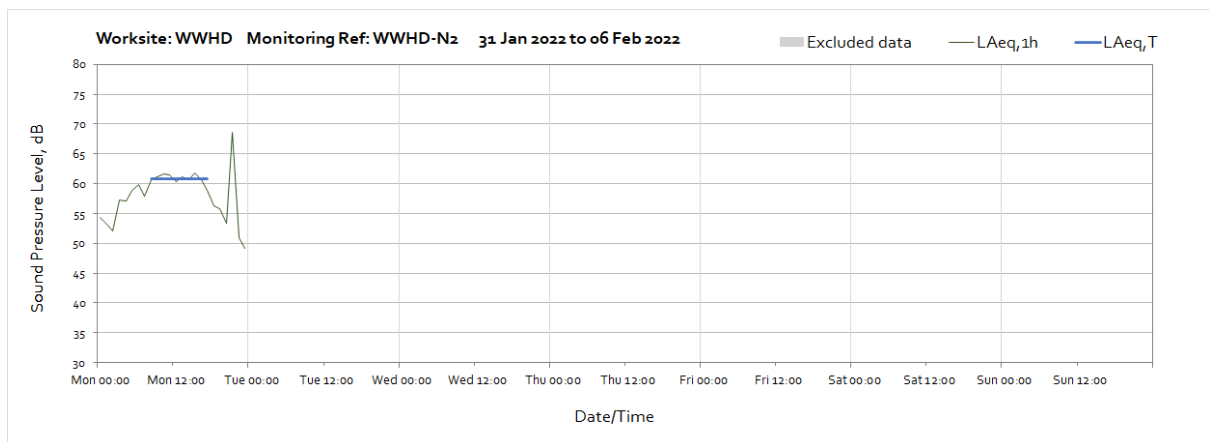
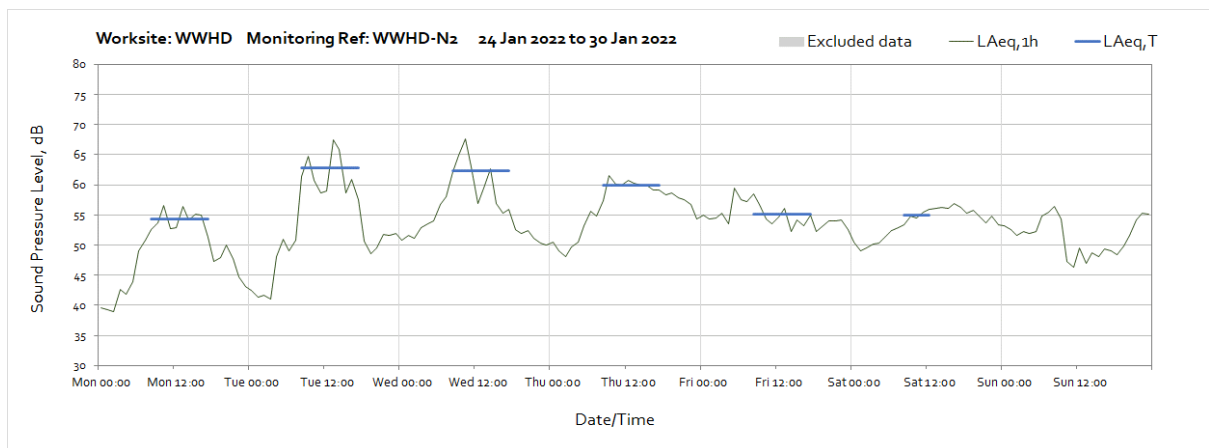
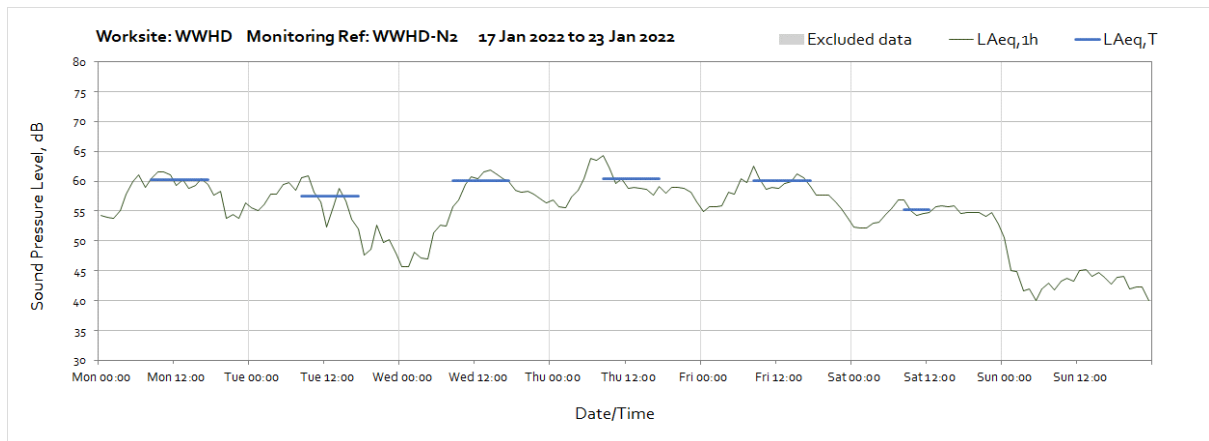
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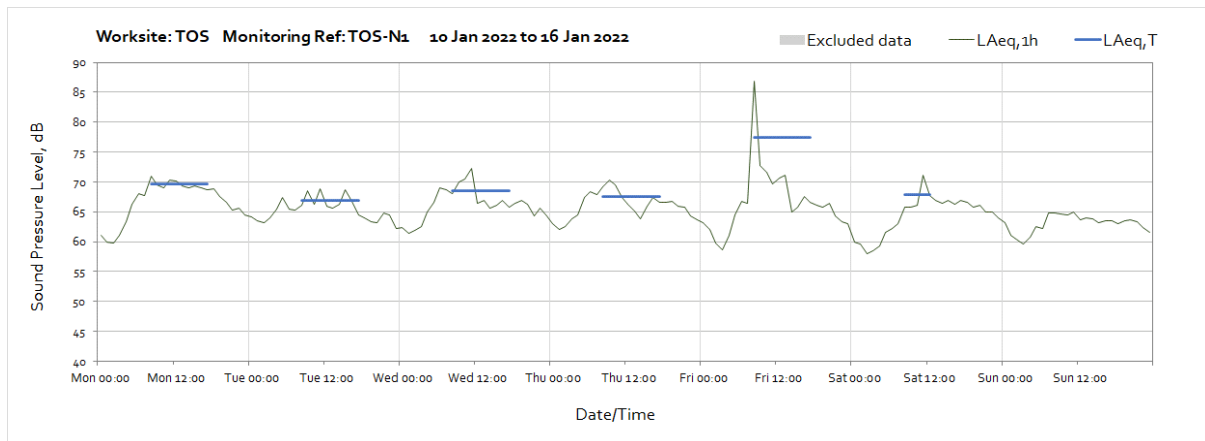
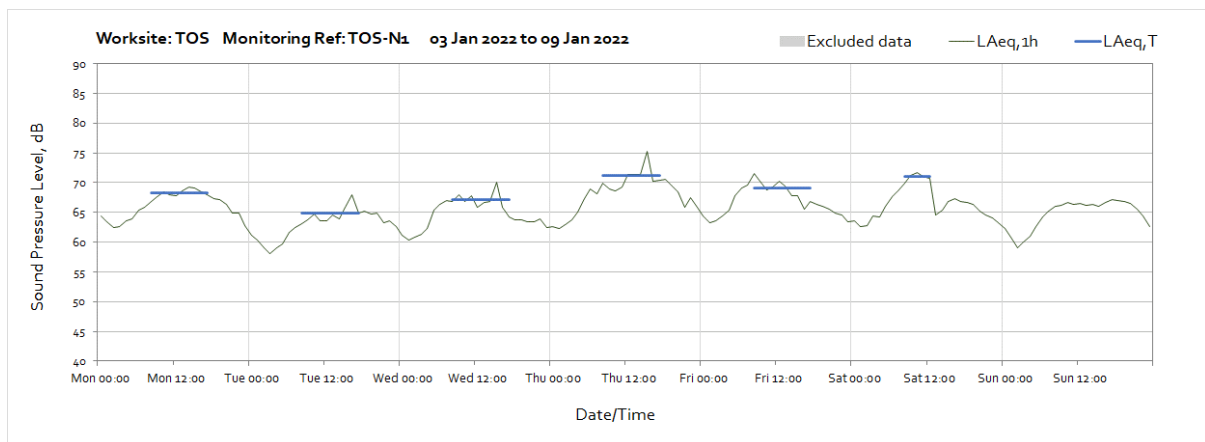
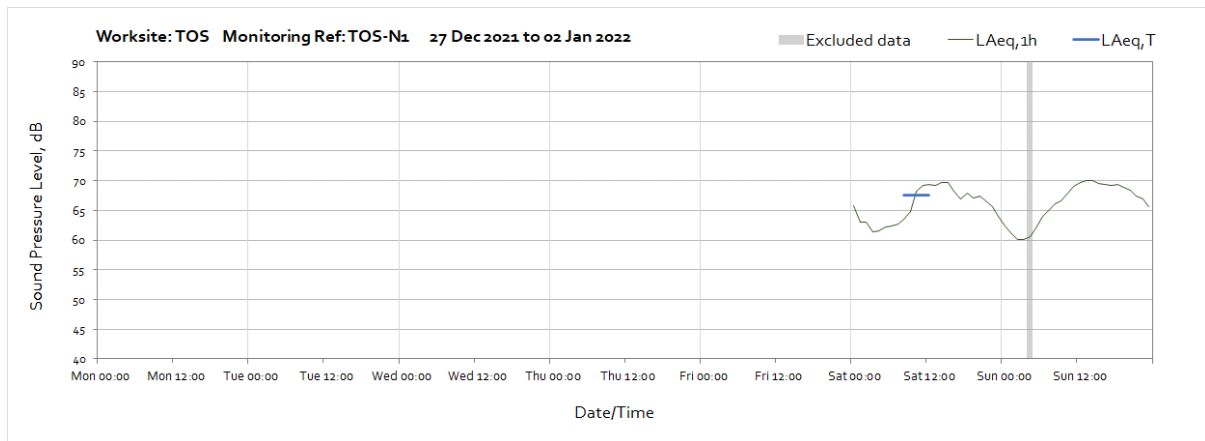
Worksite: Washwood Heath Depot (WWHD) – Monitoring Ref: WWHD-N2



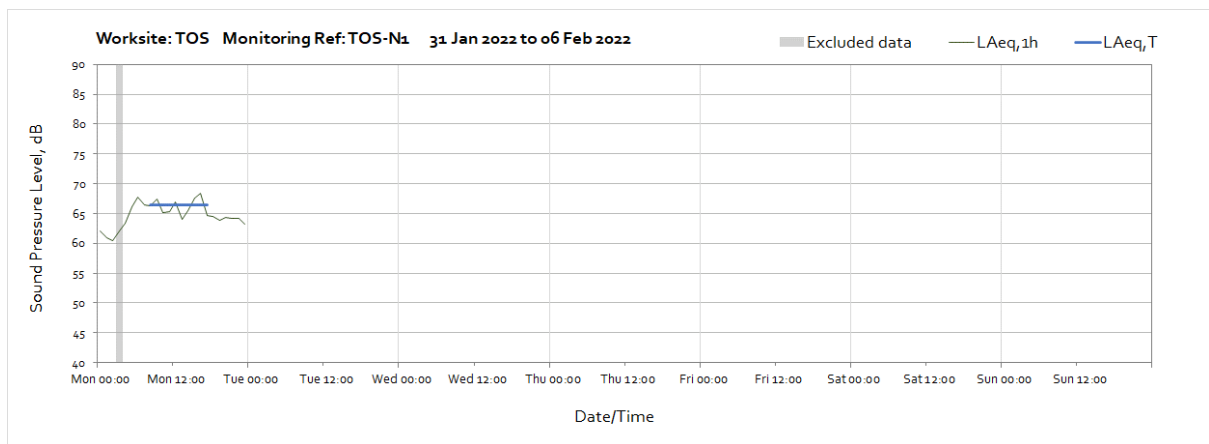
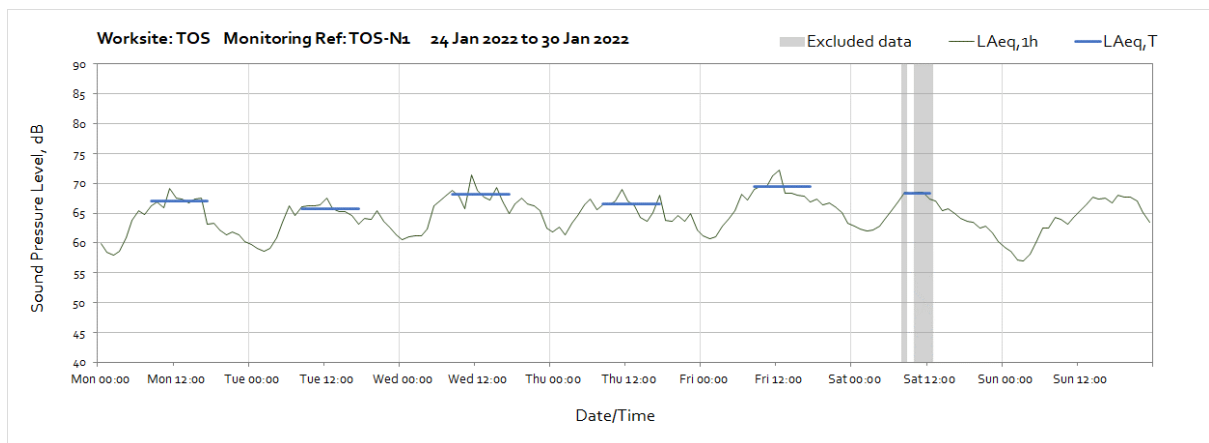
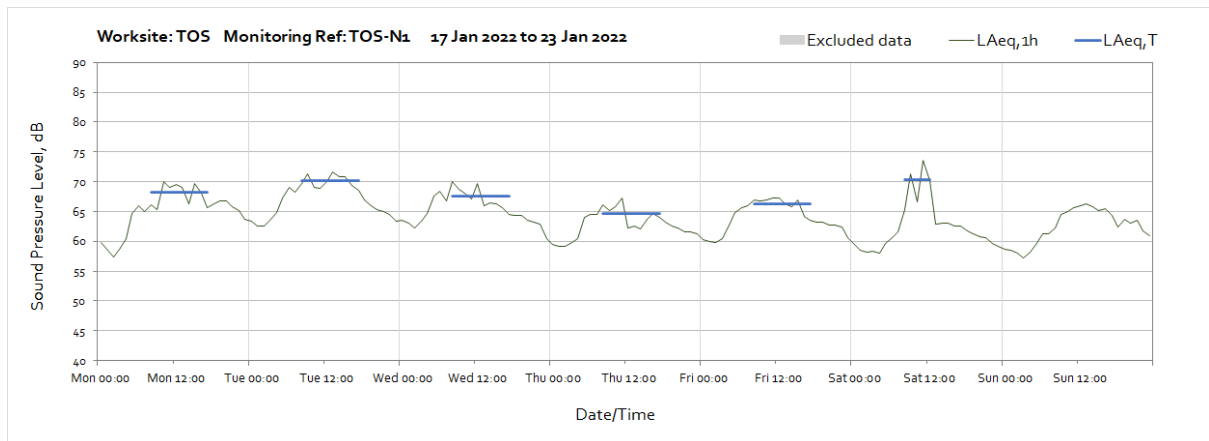
OFFICIAL



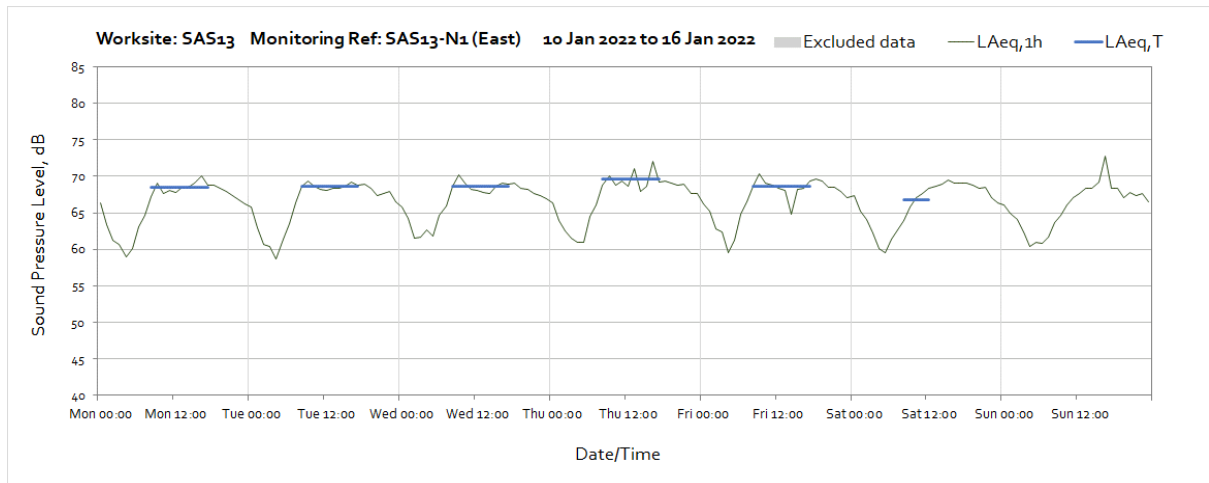
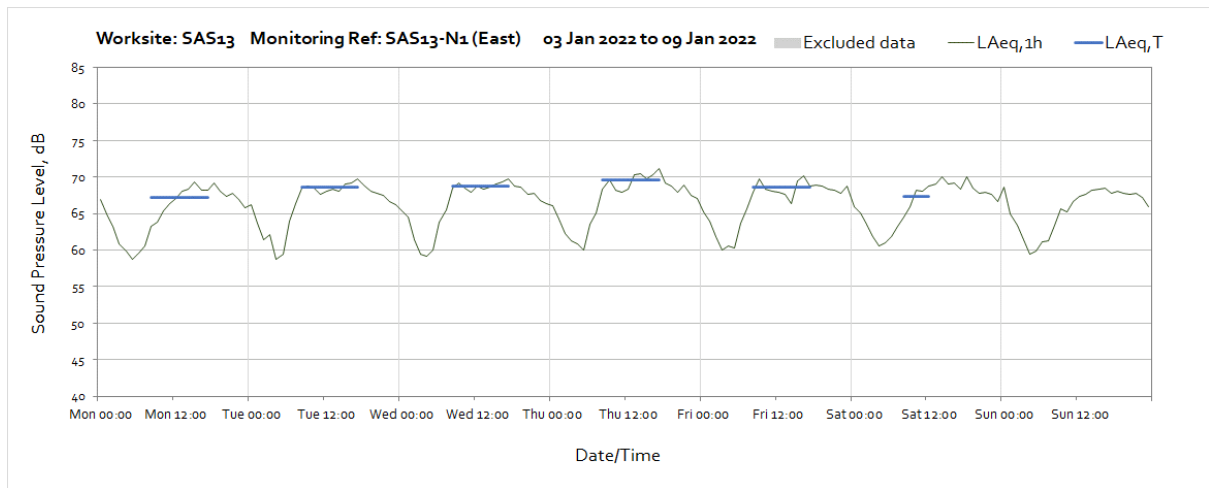
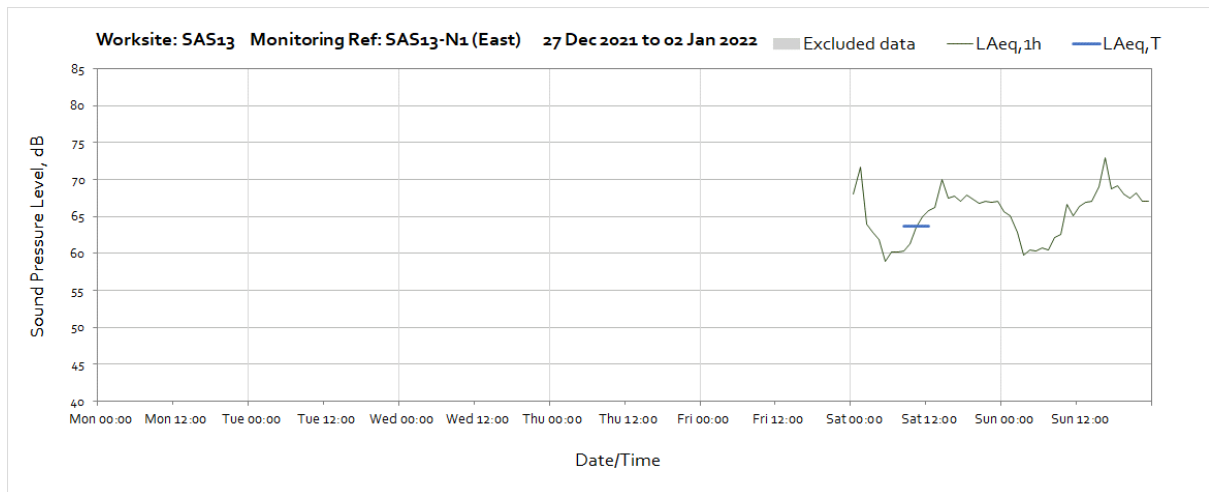
Worksite: Twisted Oak Stables (TOS) – Monitoring Ref: TOS-N1



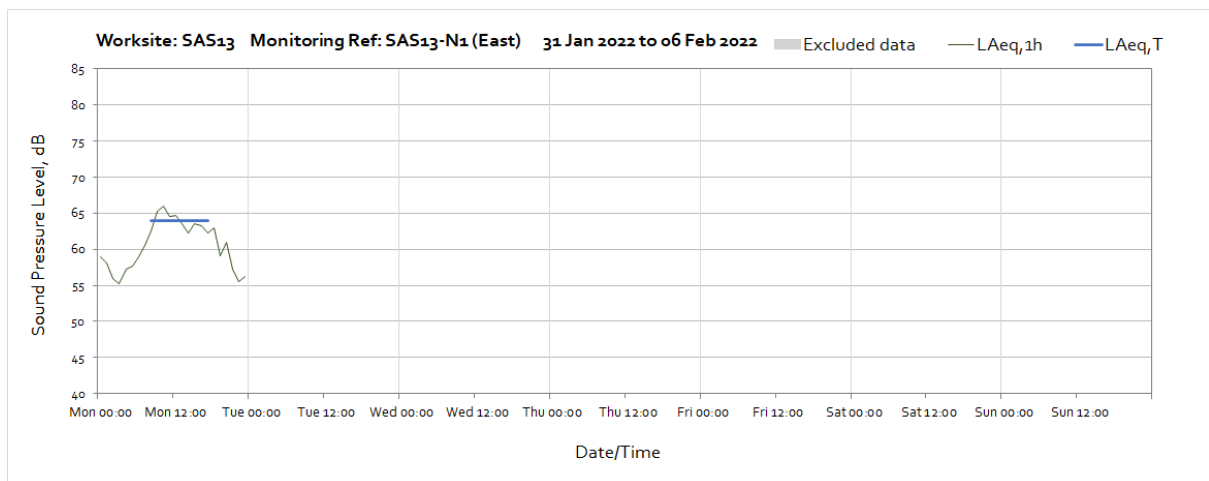
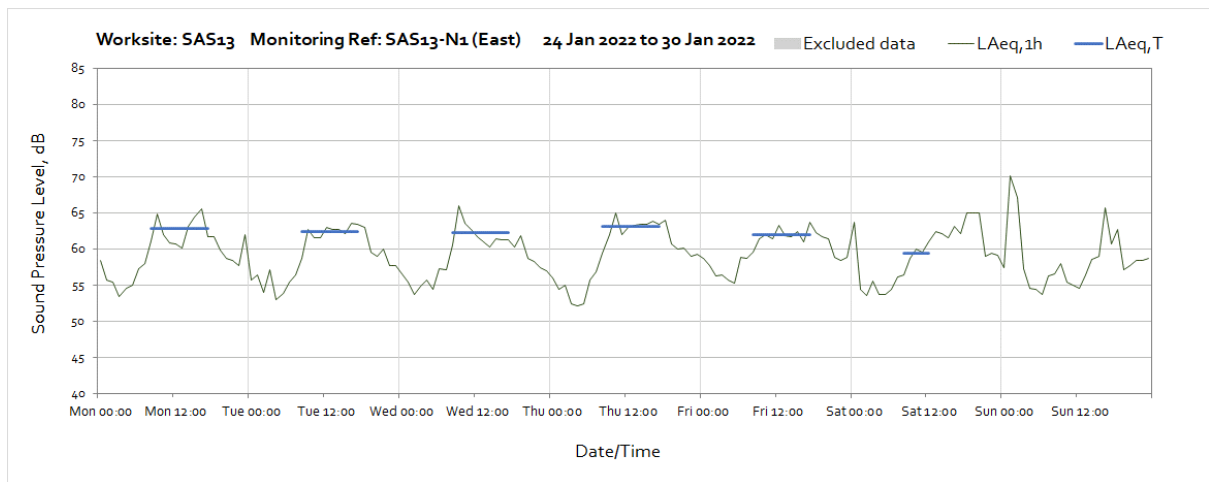
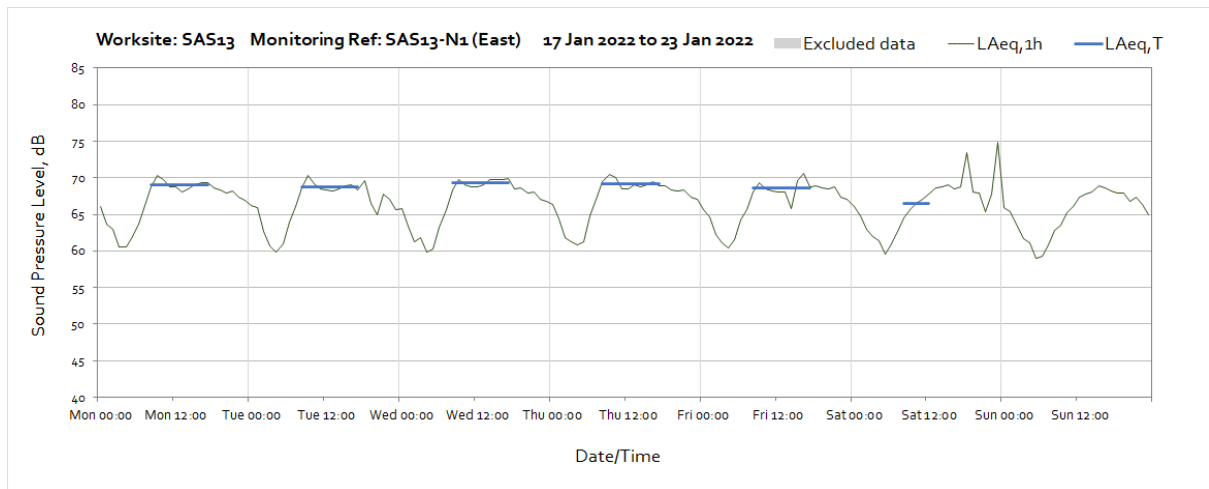
OFFICIAL



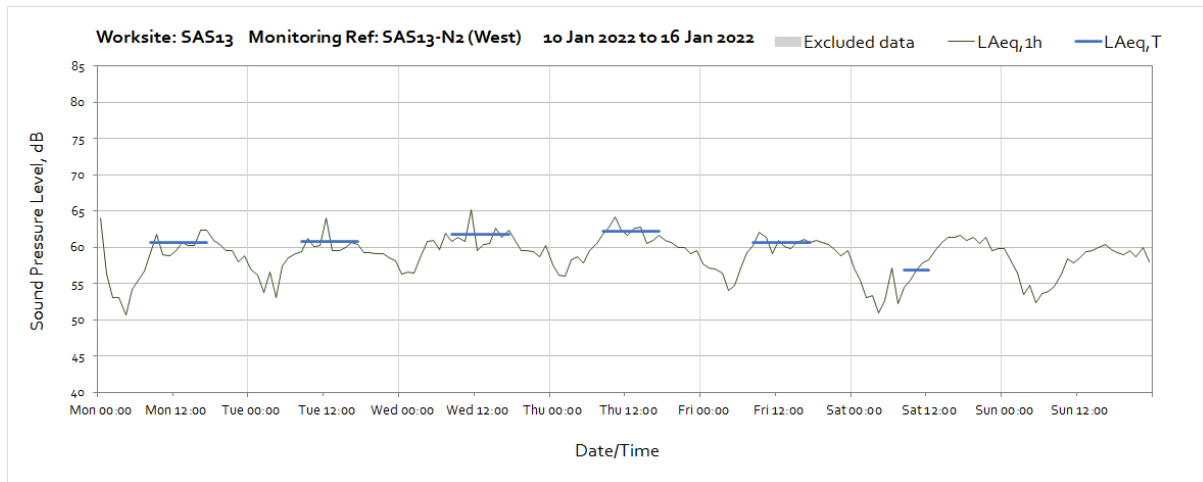
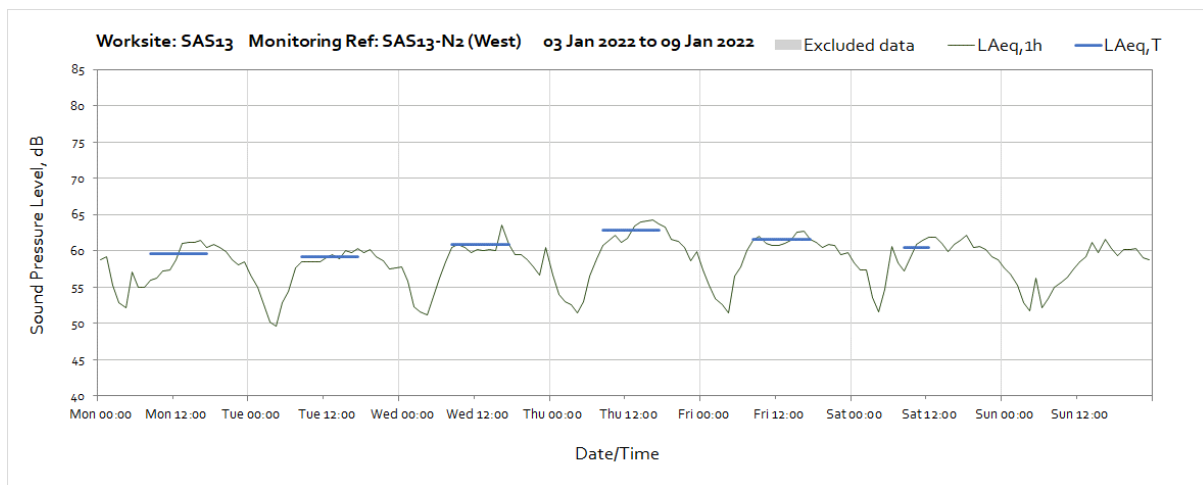
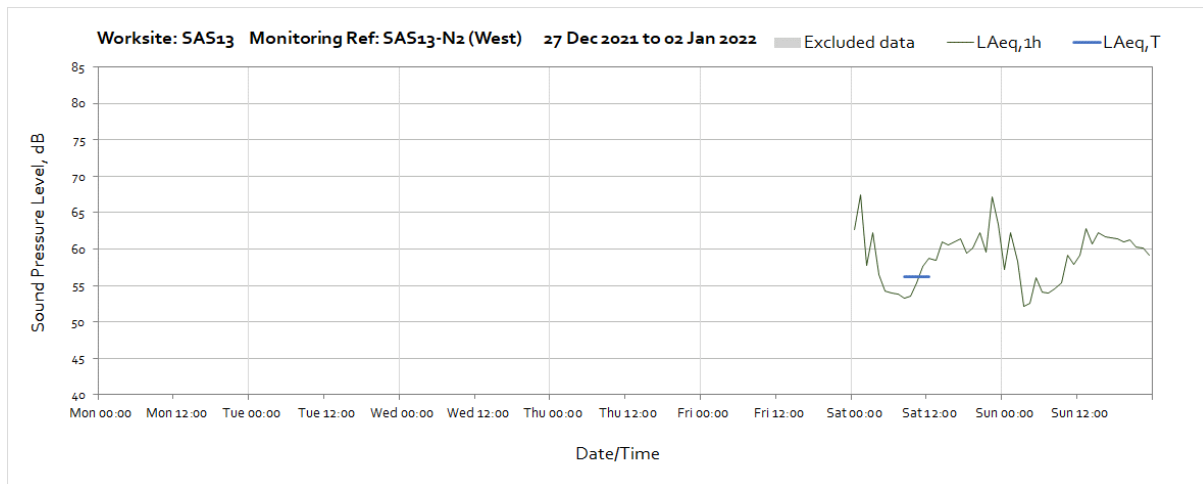
Worksite: SAS13 Bridge Replacement (SAS13) – Monitoring Ref: SAS13-N1



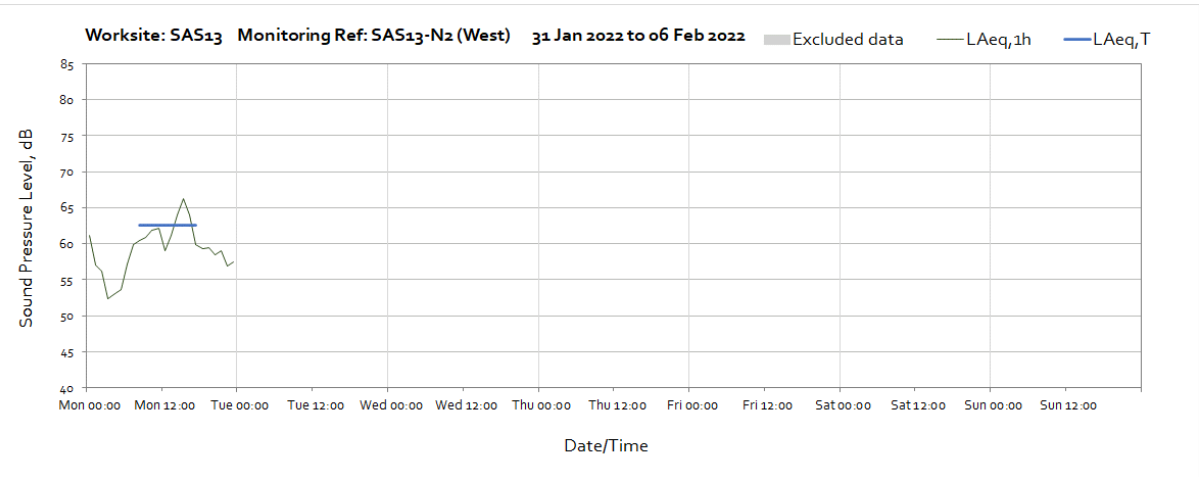
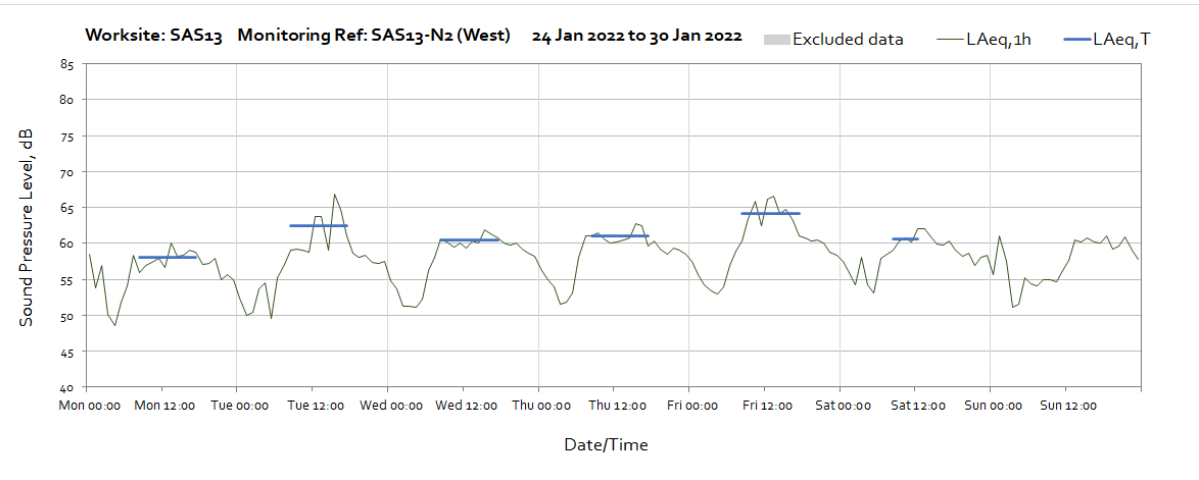
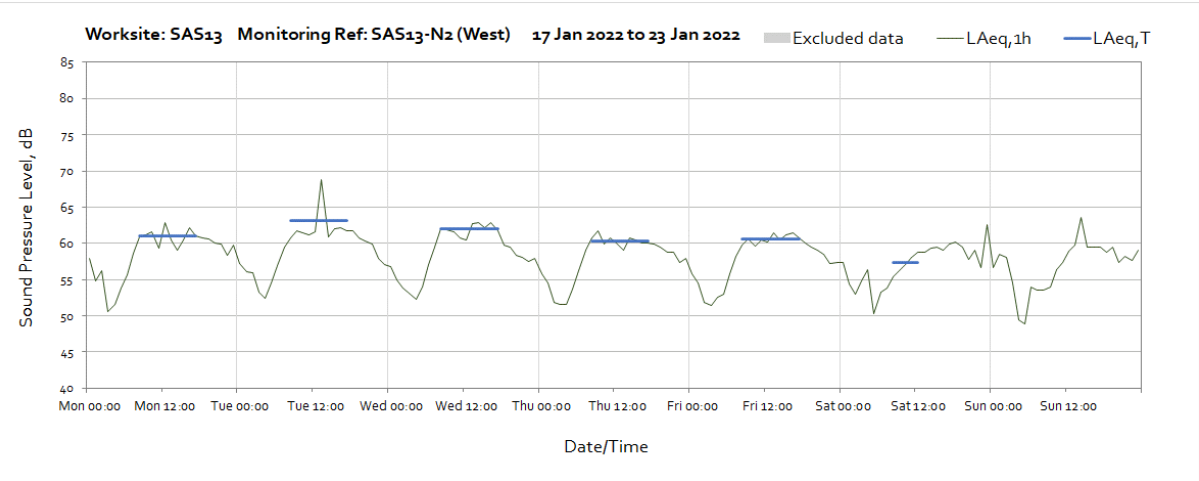
OFFICIAL



Worksite: SAS13 Bridge Replacement (SAS13) – Monitoring Ref: SAS13-N2



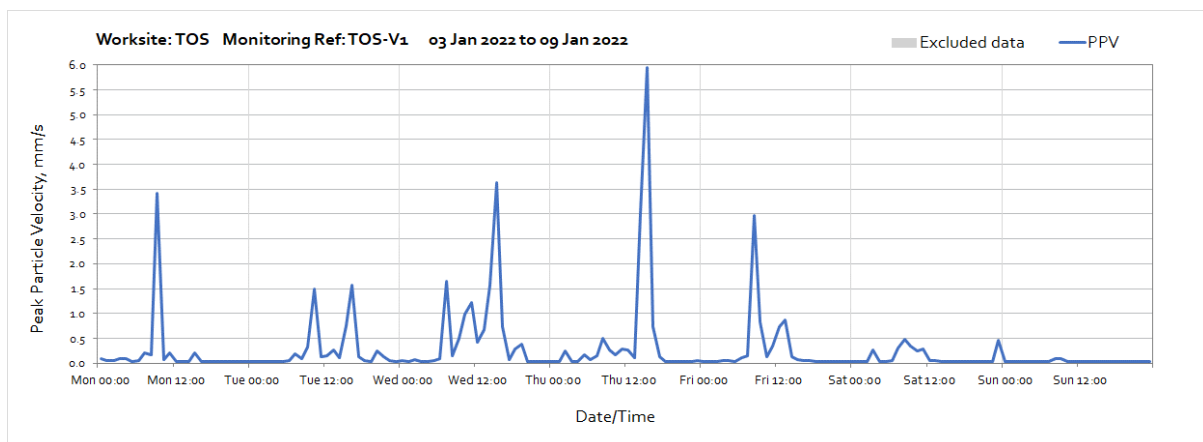
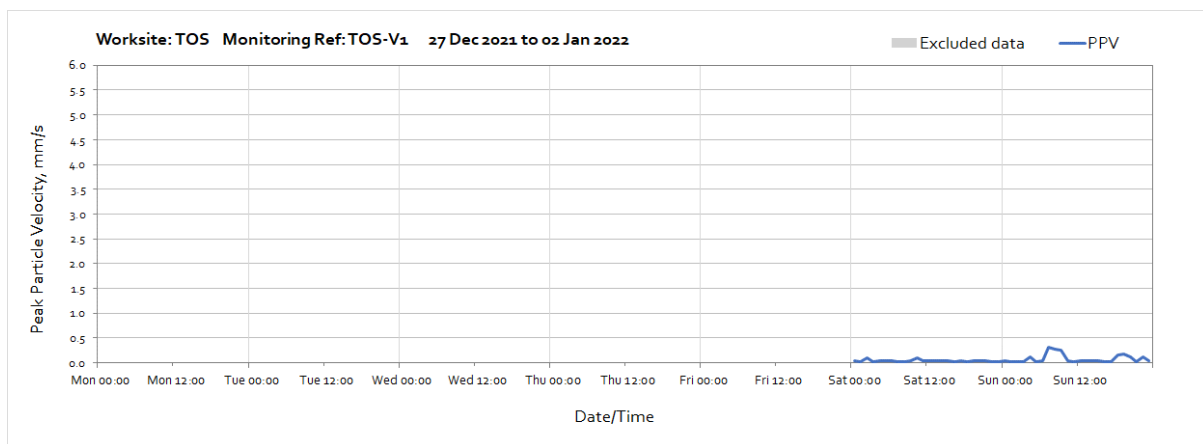
OFFICIAL



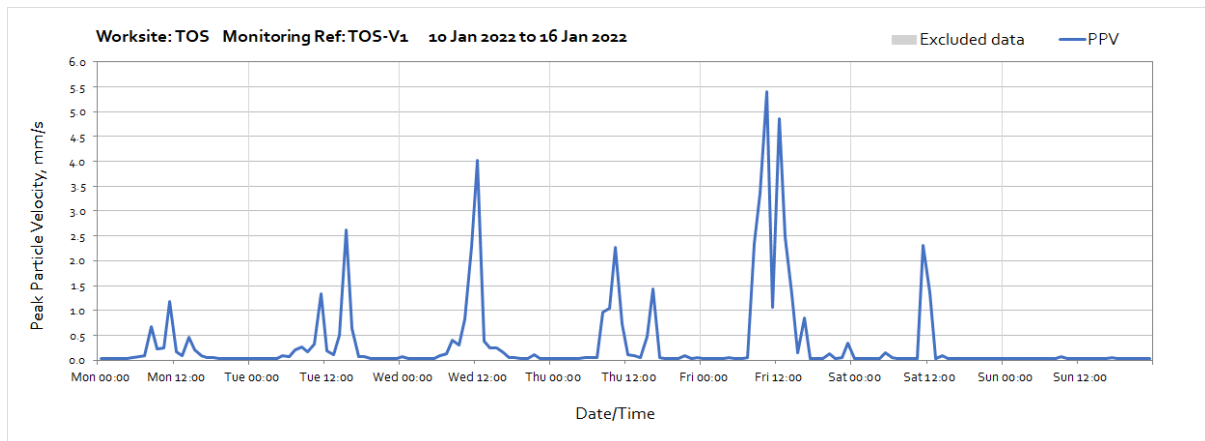
Vibration

The following graphs show the hourly measured peak particle velocity PPV recorded during the monitoring period. The graphs show the highest PPV of the three orthogonal axis x, y and z. Where high values of PPV were caused by local interference with the vibration monitor, which are not representative of HS2 construction works, these values have been greyed out in the following charts and have been excluded to calculate values in Table 4 of the main report.

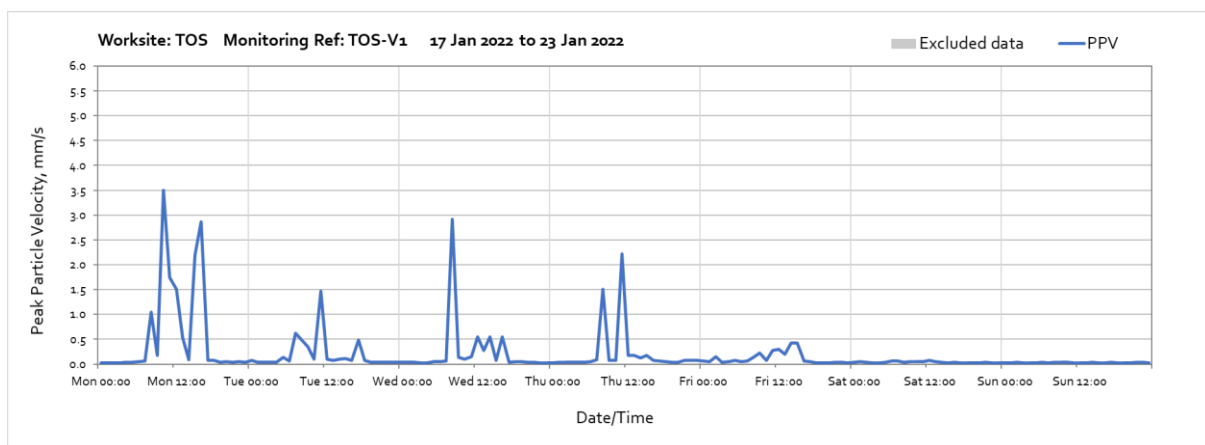
Worksite: Twisted Oak Stables (TOS) – Monitoring Ref: TOS-V1



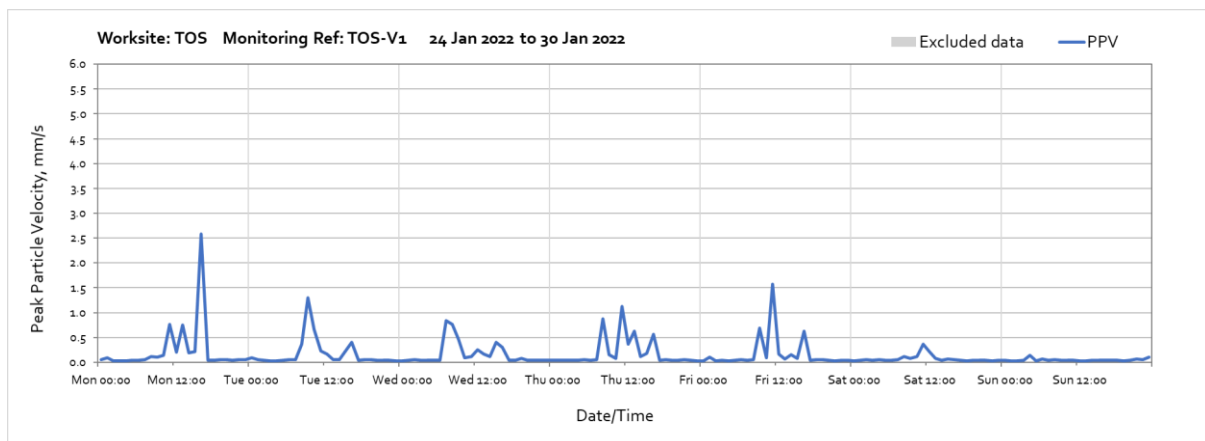
Note: Higher vibration levels measured across the week were due to asphaltting works of the site haul road undertaken close to the monitoring location. The nearest receptor is further away and therefore vibration levels will be lower at the receptor location.

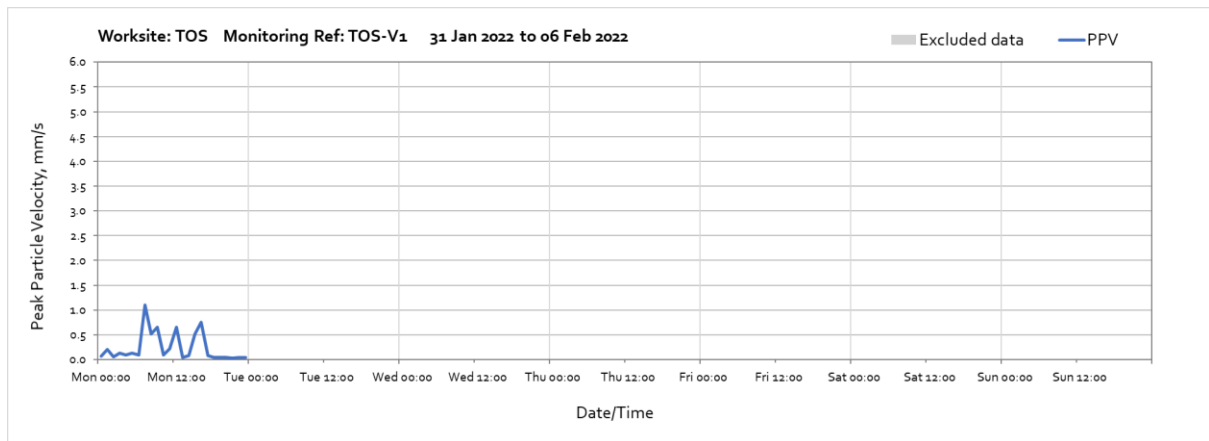


Note: Higher vibration levels measured across the week were due to asphaltting works of the site haul road undertaken close to the monitoring location. The nearest receptor is further away and therefore vibration levels will be lower at the receptor location.

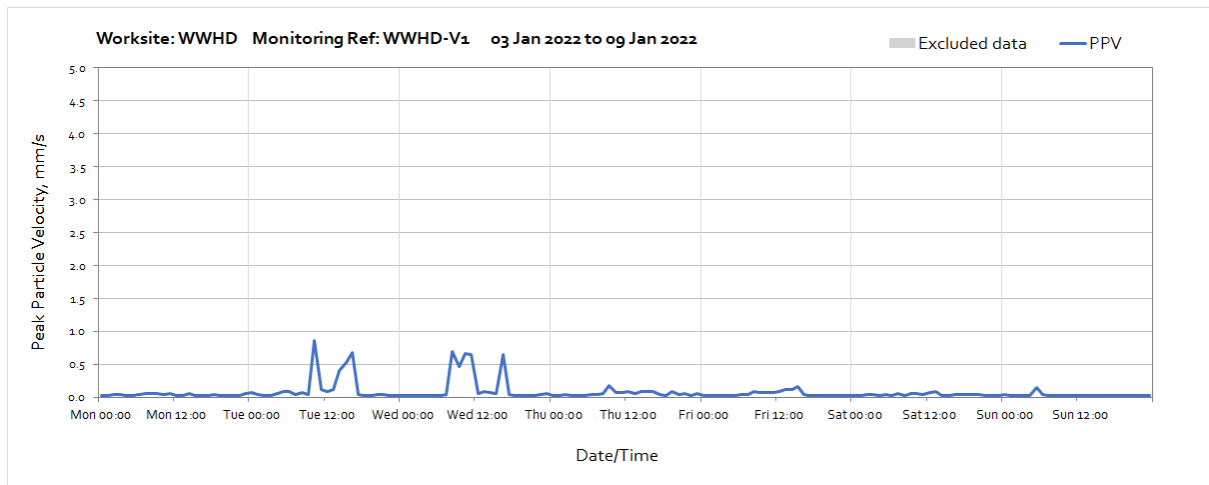
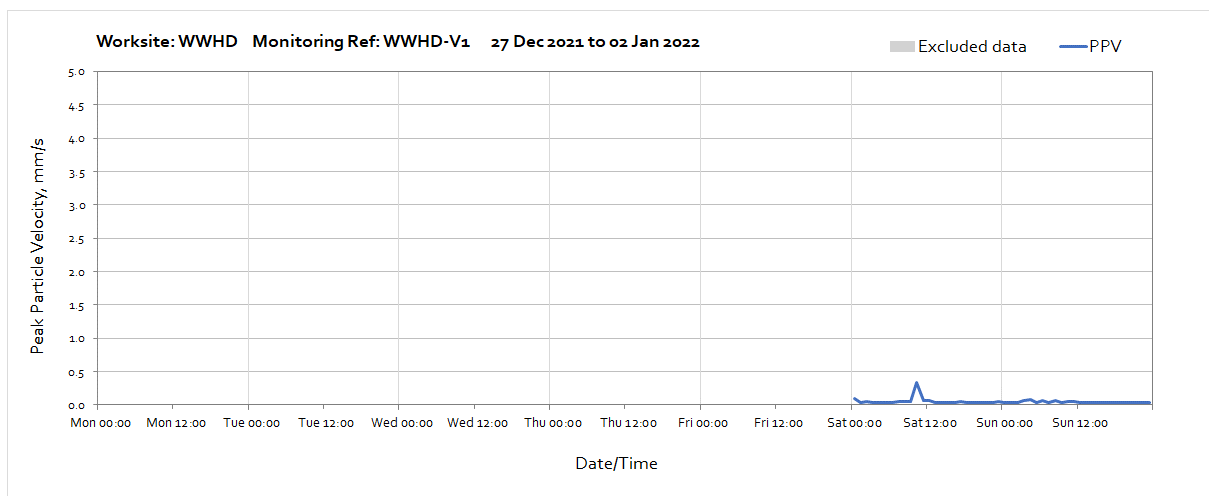


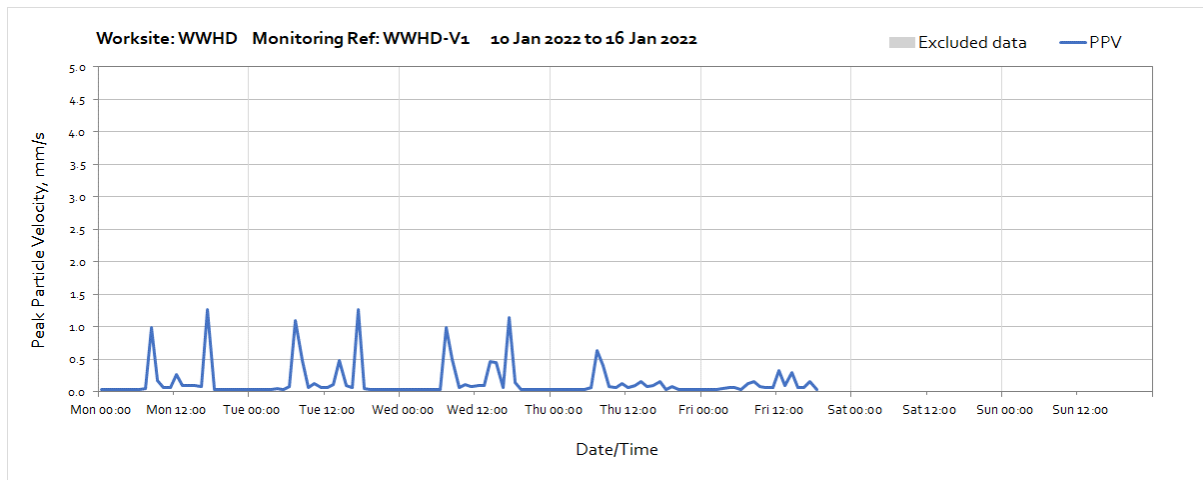
Note: Higher vibration levels measured across the week were due to asphaltting works of the site haul road undertaken close to the monitoring location. The nearest receptor is further away and therefore vibration levels will be lower at the receptor location.



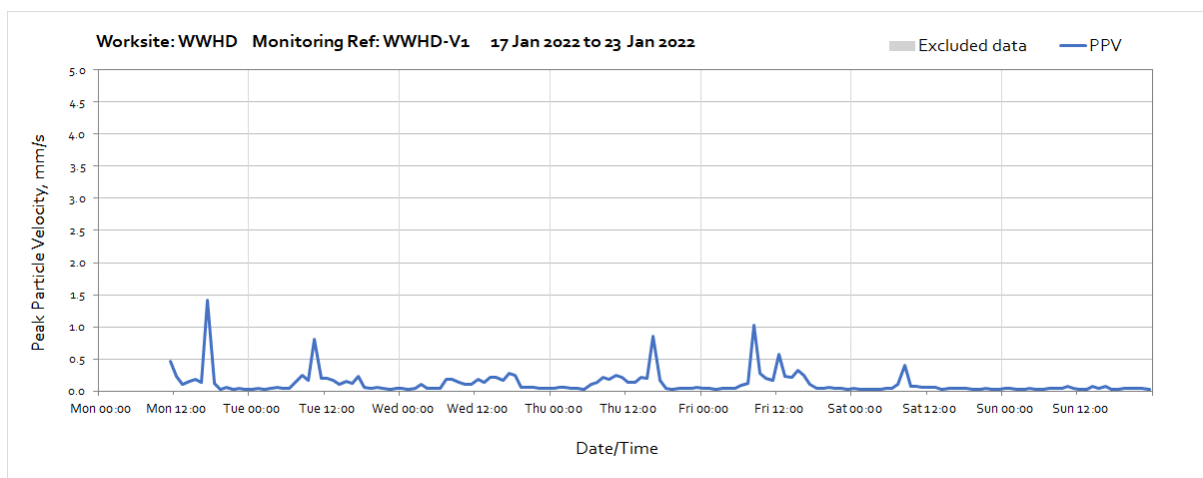


Worksite: Washwood Heath Depot (WWHD) – Monitoring Ref: WWHD-V1

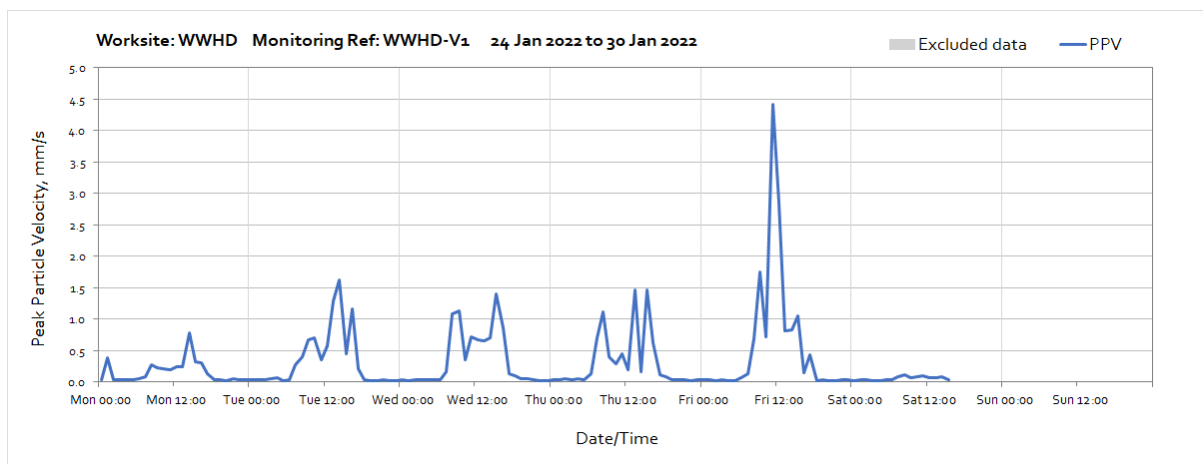




Note: Missing data between 19:00 on Friday 14th and 11:00 on Monday 17th January 2022 was due to battery falling below required voltage limit caused by prolonged insufficient sunlight.

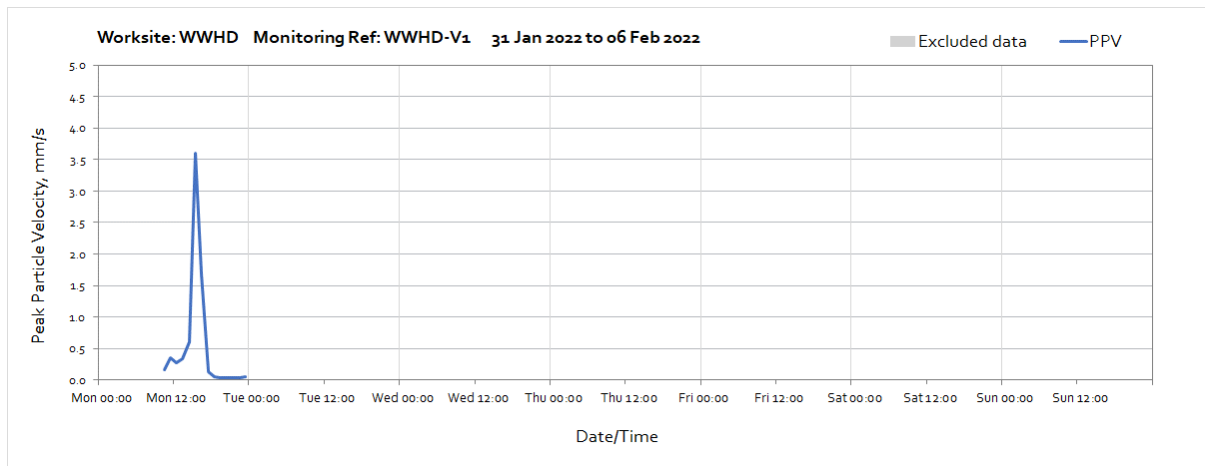


Note: Missing data between 19:00 on Friday 14th and 11:00 on Monday 17th January 2022 was due to battery falling below required voltage limit caused by prolonged insufficient sunlight.



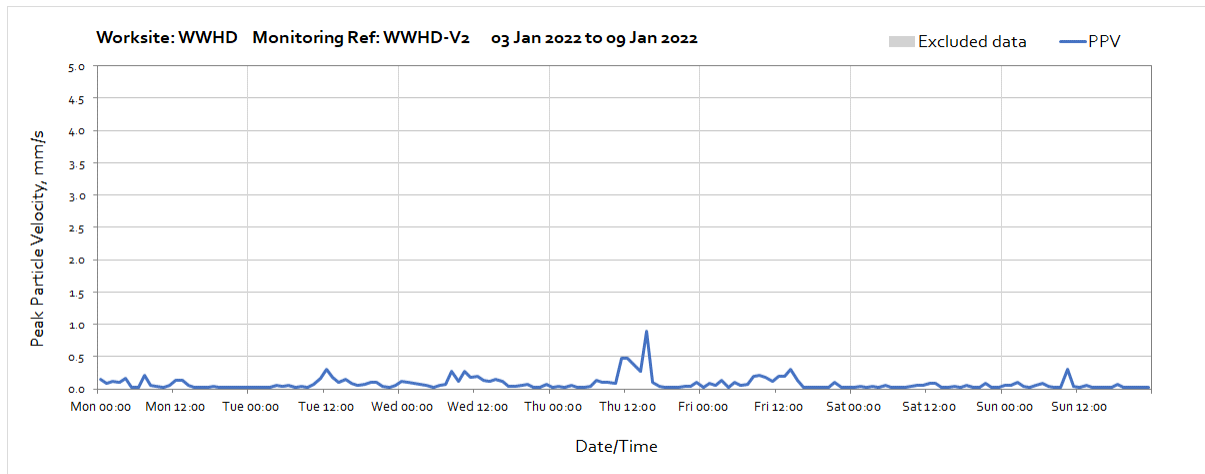
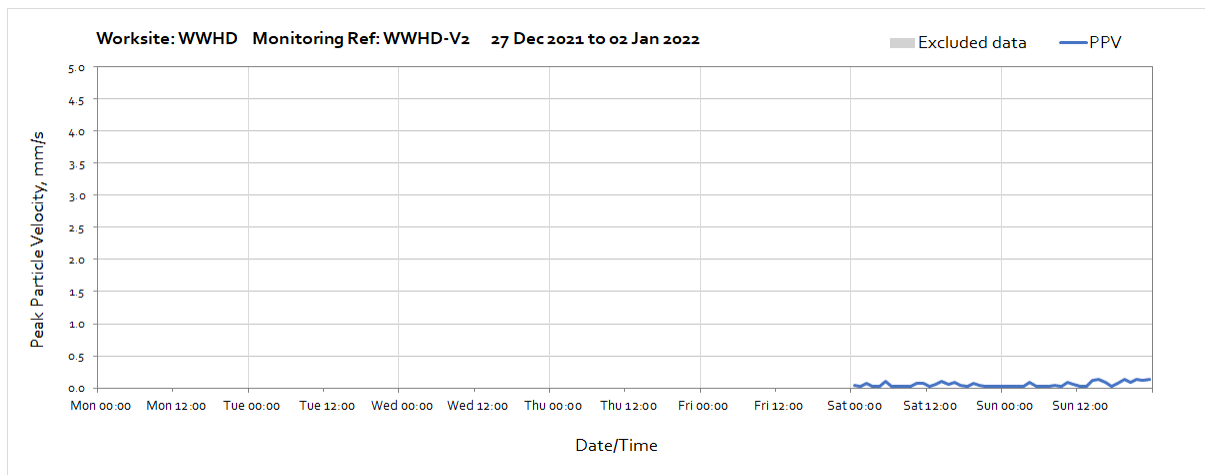
Note: High vibration levels measured during the week were due to plant movements and piling works. Missing data between 16:00 on Saturday 29th and 09:00 on Monday 31st January 2022 was due to battery falling below required voltage limit caused by prolonged insufficient sunlight.

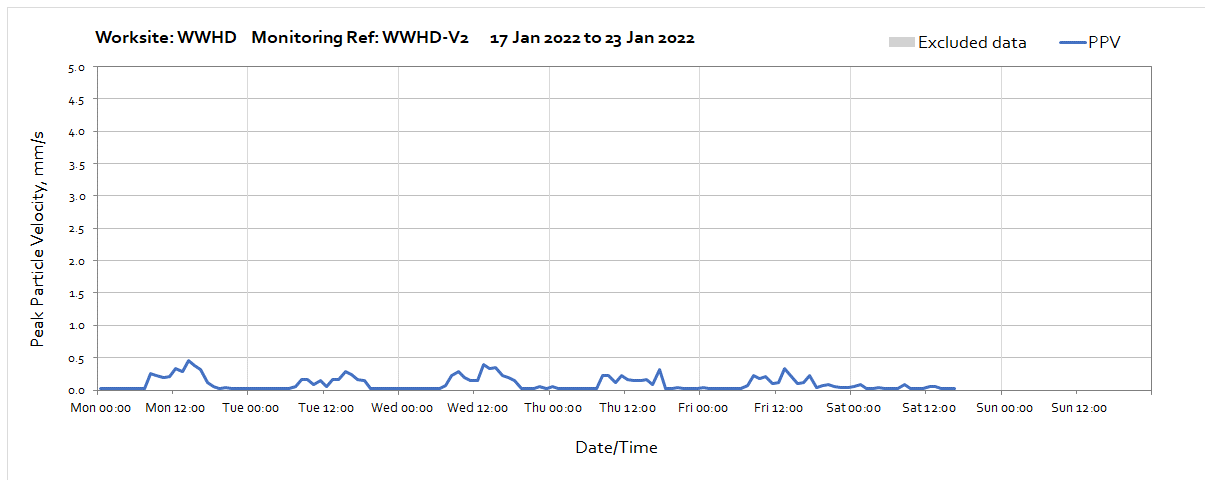
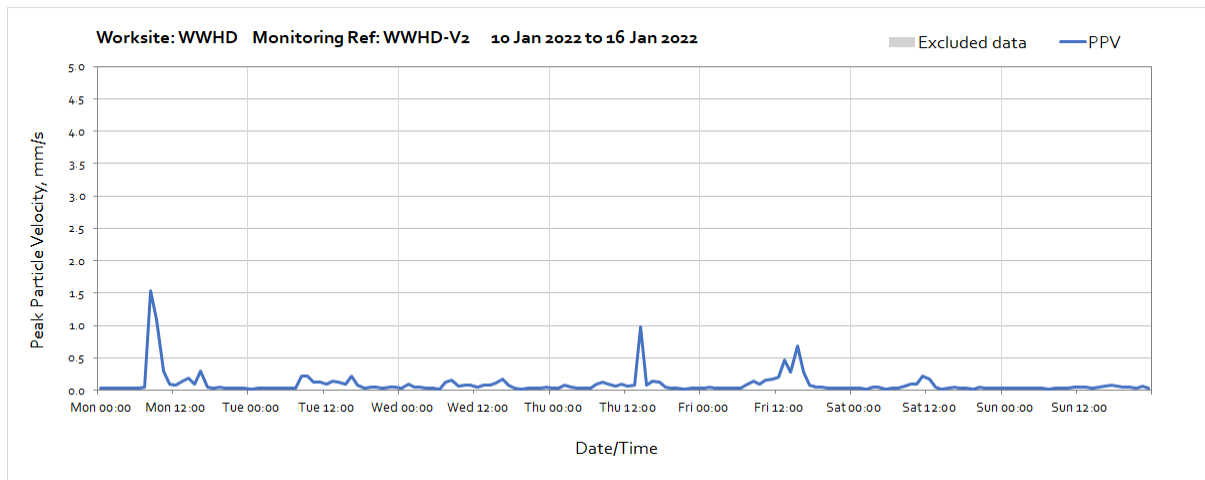
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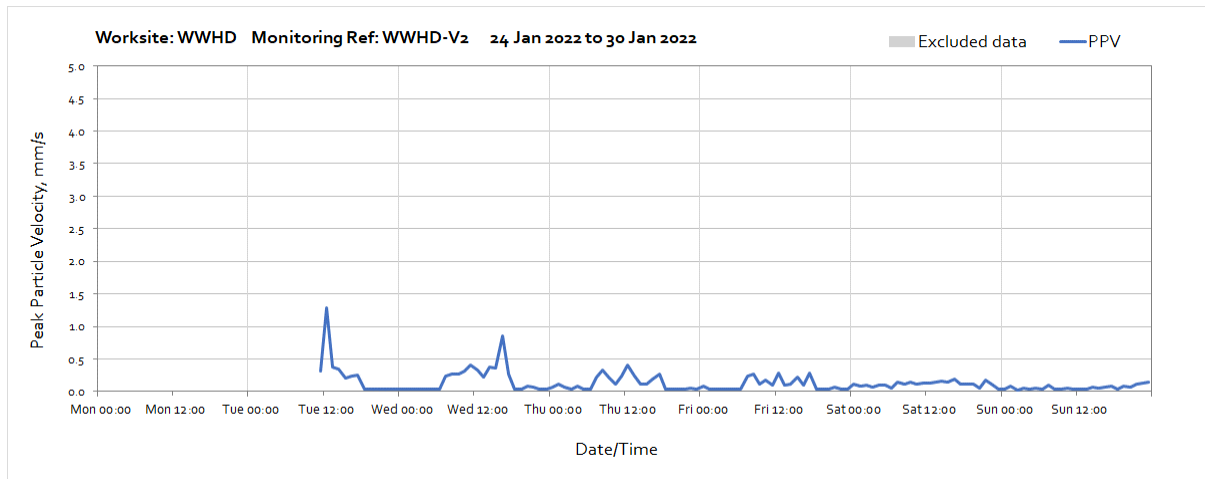
Note: Higher vibration levels measured during the week were due to plant movements and piling works. Missing data between 16:00 on Saturday 29th and 09:00 on Monday 31st January 2022 was due to battery falling below required voltage limit caused by prolonged insufficient sunlight.

Worksite: Washwood Heath Depot (WWHD) – Monitoring Ref: WWHD-V2

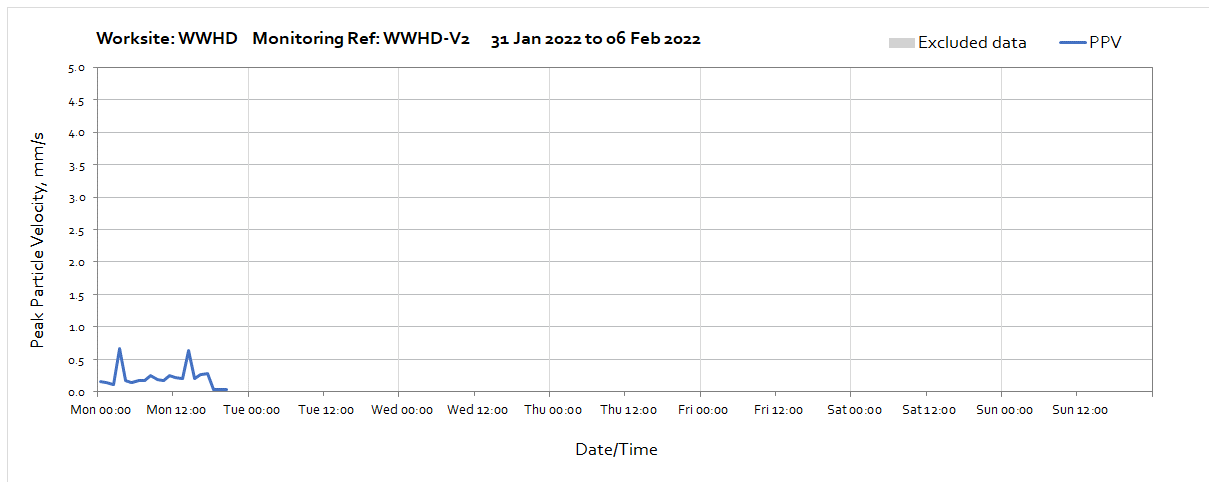




Note: Missing between 17:00 on Saturday 22nd and 11:00 on Tuesday 25th January 2022 were due to a firmware glitch.



Note: Missing between 17:00 on Saturday 22nd and 11:00 on Tuesday 25th January 2022 were due to a firmware glitch.



Note: Missing data from 21:00 on Monday 31st January 2022 onwards was due to a fence falling on the cable of the monitor.