

# How to comply with your environmental permit.

Additional guidance for:

Groundwater risk assessment for treated effluent discharges to infiltration systems

Annex J5: Infiltration Worksheet User Manual v2.0



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## Summary of changes

Below is a summary of changes made to this Annex since the launch in February 2011.

Annex version	Date	Change	Template version
1.2	Nov 2011	Reformatting to respond to general issues raised in the 2010 H1 public consultation. Minor review of text and layout.	H1 April 2011
2.0	Dec 2014	Infiltration worksheet tool amended to represent drainage layer	H1 April 2011
		Error in dilution factor calculation fixed	
		Minor review of text, layout and references	

### Introduction

#### Infiltration Worksheet user manual v2.0

We have prepared this user manual to assist users of our Infiltration Worksheet v2.0 (InfWS). This document describes the functionality of the InfWS and gives guidance on its use including some simple tips for using and interpreting the results.

The InfWS provides a means of carrying out some of the calculations behind the framework on *Annex J4 Groundwater risk assessment for treated effluent discharges to infiltration systems* (Environment Agency, 2011a), which forms a technical annex to our H1 Environmental Risk Assessment: *Annex J groundwater* (Environment Agency, 2011b).

More general information on our approach to risk assessment and the underlying regulatory context and our position are set out in the following documents:

- <u>Groundwater Protection: Principles and practice</u> (GP3) (Environment Agency, 2013 or as updated).
- <u>Guidelines for environmental risk assessment and management</u>. The Stationery Office (DETR *et al*, 2000).

We strongly recommended that you read and become familiar with the relevant sections of these documents before using the InfWS.

We have developed the InfWS to help determine the risk to groundwater from discharges of treated sewage effluent via infiltration systems (such as a drainage field designed to British Standards) and it should only be used in this context. It is appropriate to use the InfWS for larger discharges (15m³/day or more) or those which have been identified as needing to progress to a higher level of assessment (Level 2 prior examination).

The InfWS should only be used by suitably experienced hydrogeologists or those fully conversant with our approach to groundwater risk assessment and the relevant legislation and guidance.

The InfWS can also be used as a tool to help refine the location of the discharge, the design of the structure and the level of treatment of the effluent prior to discharge. This can be supported by the use of sensitivity analysis.

The previous version of the InfWS (version 1.2) has been updated as follows:

1. The drainage blanket within an infiltration system / drainage field is now represented, which allows attenuation in the drainage blanket and unsaturated zone to be considered separately. This modification was based on research by the Irish

- Environment Protection Agency<sup>1</sup> that suggests attenuation mainly occurs within the drainage blanket.
- 2. A check has been added to flag any inconsistency between the area of the drainage field entered or calculated in the 'Infiltration' sheet and the area calculated in the 'Dilution' sheet (see Table 3.4).
- 3. An appendix has been added which gives guidance on input values.
- 4. The equation used to calculate the dilution factor has been corrected. This may have resulted in minor errors.

### Obtaining and installing the InfWS

You can download the InfWS version 2.0 from the <u>Horizontal guidance: environmental</u> permitting on the gov.uk website.

We have prepared and tested the InfWS in Microsoft Excel 2002<sup>TM2</sup> on the Microsoft 95/2000/XP<sup>TM</sup> operating systems. The file comprises about 570 KB and should not require any significant additional computing capability beyond that needed to run Microsoft Excel 2002<sup>TM</sup>.

We recommend that a blank copy is saved as a master file and that each simulation is saved as a distinct file.

In order to enable the InfWS, a number of capabilities are required in Microsoft Excel 2002<sup>TM</sup> that may not automatically be set. The InfWS calculates error functions and complimentary error functions. Before use, you will need to add these capabilities by clicking the following from the pull-down Tools menu:

Tools ⇒Add-Ins ⇒ Analysis ToolPak and Analysis ToolPak-VBA.

You must also **Enable Macros** when prompted to do so.

If you are working in Microsoft Excel 2007 $^{\text{TM}}$ , you will need to add these capabilities by clicking the Office Button and then the following from the pull-down Tools menu:

Excel Options ⇒Add-Ins ⇒ Analysis ToolPak and Analysis ToolPak-VBA.

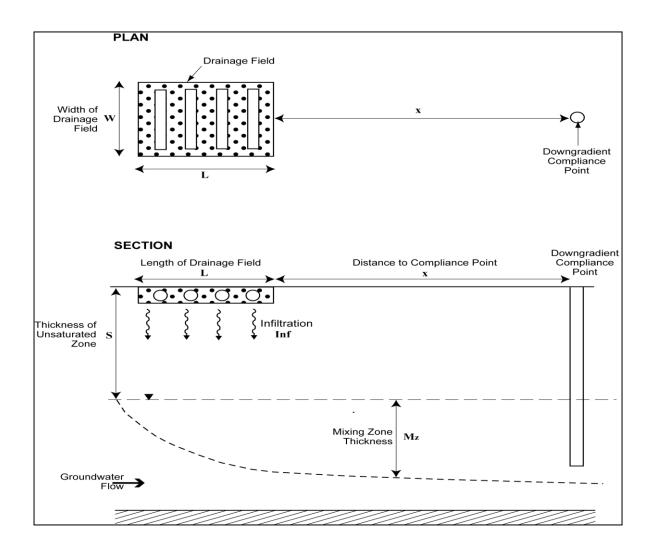
<sup>&</sup>lt;sup>1</sup> Irish Environment Protection Agency, 2005. An investigation into the performance of subsoils and stratified sand filters for the treatment of wastewater from on-site systems. Final Report for project 2000-MS-15-M1 (The Hydraulic Performance and Efficiencies of Different Subsoils and the Effectiveness of Stratified Sand Filters) Environmental RTDI Programme 2000-2006.

<sup>&</sup>lt;sup>2</sup> The worksheet is currently being tested for use on later versions of Microsoft Excel<sup>TM</sup> and other Microsoft<sup>TM</sup> operating systems

### 1.0 Overview

An illustration of a typical setting for which the InfWS could be used is given in Figure 1.1

Figure 1.1 Discharge of treated effluent to infiltration systems and application of the InfWS



You can use the InfWS to:

- calculate the area of the drainage field;
- calculate the average infiltration rate over the drainage field;
- determine attenuation within the drainage blanket and the unsaturated zone and calculate the concentration of the substance of concern at the water table;

- determine the dilution factor for non-hazardous pollutants and calculate their concentration in groundwater immediately down-gradient of the drainage field;
- determine attenuation within the saturated zone for non-hazardous pollutants and calculate their concentration at a point down-gradient of the drainage field; and
- determine provisional discharge limit values.

Box 1.1 contains a definition of some of the main terms used in this document.

Box 1.1 Definition of standard terms							
Term	Definition						
Compliance point	A compliance point is a suitable point along the substance pathway between the source and a receptor at which a compliance value can be set. The compliance point may be a virtual point (for the purpose of predictive assessments) or it may be a physical monitoring point such as a borehole. In some cases the compliance point may be the receptor itself.						
Compliance value	This is a concentration at the compliance point that should not be exceeded. Depending on the level of assessment, a compliance value may take account of some or all of the dilution and attenuation processes along the substance pathway to the receptor(s). The purpose of the selected compliance value is to provide protection to a down-gradient receptor – provided the compliance value is met the relevant environmental standard for the receptor(s) should also be met.						
Discharge limit value	A discharge limit value is a value set as a condition in the permit to control a specified substance in the discharge with the aim of preventing the input of hazardous substances to groundwater or pollution due to the input of non-hazardous pollutants.						
Dilution factor	The dilution factor describes the amount of dilution of the discharge by groundwater flow and is calculated from the ratio of groundwater below the drainage field and the discharge to the drainage field.						
Attenuation factor (drainage blanket)	The attenuation factor in the drainage blanket can be calculated as the ratio between the concentration of the substance in the treated effluent and the predicted concentration at the base of the drainage blanket.						
Attenuation factor (unsaturated zone)	The attenuation factor in the unsaturated zone can be calculated as the ratio between the concentration of the substance at the base of the drainage blanket and the predicted concentration at the base of the unsaturated zone.						
Attenuation factor (saturated zone)	The attenuation factor in the saturated zone can be calculated as the ratio between the concentration of the substance in groundwater below the drainage field and the predicted concentration at a point downgradient of the drainage field.						

Box 1.1 contin	nued
Term	Definition
Environmental standard	The environmental standard used to derive the compliance values will depend on (a) whether the substance is a hazardous substance or a non-hazardous pollutant and (b) the use of the receptor (for example, a potable abstraction or surface water). Examples of environmental standards are:
	<ul> <li>Limits of detection or where applicable a Minimum Reporting Value (MRV), MRVs are typically used to assess the discernibility of hazardous substances as a basis for deciding whether their input has been prevented;</li> </ul>
	<ul> <li>Natural background (up-gradient) quality. This might be used to assess the discernibility of hazardous substances where background concentrations are higher than detection limits or the MRV. Alternatively it might be used for non-hazardous pollutants where the natural background concentration exceeds the relevant standard such as a drinking water standard (DWS) or environmental quality standard (EQS).</li> </ul>
	DWS (Drinking Water Standard) or EQS (Environmental Quality Standard). In some cases it will be appropriate to use lower concentrations than the DWS or EQS to provide satisfactory protection to a receptor. For example, it may be suitable to apply a safety factor to provide greater security to an existing drinking water supply (such as 0.75 x DWS). In other cases where the DWS or EQS represents a significantly higher concentration than the natural background quality, use of such values might represent a significant level of deterioration (for example, a DWS of 250 mg/l of chloride compared to a background concentration of for example, 30 mg/l). In these cases you may need to discuss this with us and derive a more suitable value between the MRV or background concentration and the EQS or DWS.

# 2.0 The risk assessment approach and the site conceptual model.

The tools selected to model a site should be appropriate to the conceptual model and the quality of the available data. Guidance on these issues is provided in:

- Guide to good practice for the development of conceptual models and the selection and application of mathematical models of contaminant transport processes in the subsurface. National Groundwater and Contaminated Land Centre report NC/99/38/2, Solihull (Environment Agency, 2001a).
- Benchmarking and guidance on the comparison of selected groundwater riskassessment models. National Groundwater and Contaminated Land Centre report NC/00/14, Solihull (Environment Agency, 2001b).

You should only employ the InfWS where a robust conceptual model has been developed and you are satisfied that the calculations performed are relevant to the processes described within that conceptual model.

The development of a robust conceptual model is perhaps the most important aspect in the process of successfully estimating and evaluating environmental risks. The use of any mathematical modelling tool without first developing a robust conceptual model is likely to result in meaningless output and poor decision-making.

The conceptual model should be supported by valid data. Good quality site specific data is always preferred. If you use generic data it should be reliable and relevant to the site. You should document the provenance and relevance of all data included in an assessment using the InfWS and include this in any report(s) submitted to us for consideration. The InfWS should only be used when adequate site-specific data have been obtained. For further guidance on sources of information and which site-specific data are required the reader should refer to Environment Agency (2011a and 2011b).

The following guidance on reviewing assessments may also be of use in preparing reports for submission as part of any application:

 Guidance on the assessment and interrogation of subsurface analytical contaminant fate and transport models. National Groundwater and Contaminated Land Centre report NC/99/38/1, Solihull (Environment Agency, 2001c).

### 2.1 Discharge limit values

Box 2.1 contains a summary of the basic calculations to determine the concentration of a substance at different points along the contaminant pathway (Figure 1.1). Box 2.2 illustrates how the discharge limit values are derived.

## Box 2.1 Summary calculations for determining the concentration at different compliance points

#### Concentration at compliance point.

The concentrations of substances at different points along the pathway can be calculated as follows:

(i) Water table (attenuation in unsaturated zone only):

$$C_{wt} = C_e / (AF_{u1} . AF_{u2})$$
 (Equation 1)

(ii) Borehole adjacent to infiltration system (attenuation in unsaturated zone and dilution)

$$C_{gw} = C_e / (AF_{u1} \cdot AF_{u2} \cdot DF)$$
 (Equation 2)

(iii) Down-gradient borehole (attenuation in unsaturated and saturated zone and dilution - non hazardous pollutants only)

$$C_{dcp} = C_e / (AF_{u1} \cdot AF_{u2} \cdot AF_s \cdot DF)$$
 (Equation 3)

where:

 $C_{dcp}$ = Concentration at down-gradient compliance point (mg/l). Concentration should be below compliance value

 $C_{qw}$  = Concentration immediately down-gradient of drainage field point (mg/l)

 $C_{wt}$  = Concentration at base of unsaturated zone (mg/l)

 $C_e$  = Concentration of substance in treated effluent discharge (mg/l)

 $AF_{u1}$  = Attenuation factor (drainage blank et)

 $AF_{u2}$  = Attenuation factor (unsaturated zone)

DF = Dilution factor

 $AF_s$  = Attenuation factor (saturated zone)

### Box 2.2 Discharge limit values

Discharge limit values (DCL) can be calculated as follows:

(i) Attenuation in drainage layer and unsaturated zone only.

$$DCL_1 = AF_{u1} \cdot AF_{u2} \cdot C_c$$
 (Equation 4)

(ii) Attenuation in unsaturated zone and dilution

$$DCL_2 = DF \cdot DCL_1$$
 (Equation 5)

(iii) Attenuation in unsaturated and saturated zone and dilution (non hazardous pollutants only)

$$DCL_3 = AF_s$$
.  $DCL_2$  (Equation 6)

Where.

 $DCL_{1-3}$  = Discharge limit value (these will vary depending on whether compliance point is: ( $DCL_1$ ) base of unsaturated zone; ( $DCL_2$ ) groundwater immediately down-gradient of drainage field; ( $DCL_3$ ) groundwater down-gradient of drainage field.

DF = Dilution factor

 $AF_{u1}$  = Attenuation factor (drainage blank et)

 $AF_{u2}$  = Attenuation factor (unsaturated zone)

 $AF_s$  = Attenuation factor (saturated zone)

 $C_c$  = Compliance value (mg/l) (for example, water quality standard or MRV)

You should regard any discharge limit values that are calculated using the InfWS as provisional. We may need to take additional information (such as, variability of leachate quality, type of treatment process, and assumptions in choice of parameter values) into account in defining the discharge limit values that will be specified as part of the environmental permit.

### 3.0 Using the individual worksheets

### 3.1 General

The InfWS incorporates 10 worksheets, which have the following functions:

**Table 3.1 Function of worksheets** 

Title of worksheet	Function of worksheet
Introduction	Brief instructions, entry of site details, assessor details, substance and environmental standard used (and its origin) to derive the compliance value for transfer to subsequent sheets
Infiltration System	Data entry for infiltration system including infiltration rate and area of drainage field
Attenuation_unsatzone	Data entry for calculating attenuation in the drainage layer and the unsaturated zone
Dilution	Data entry for calculating dilution factor and substance concentration in groundwater immediately down-gradient of the drainage field
Attenuation_satzone	Data entry for calculating attenuation factor in the saturated zone and substance concentration in groundwater down-gradient of the drainage field
Summary	Summary of results of calculations of impact of the discharge on groundwater and provisional discharge limit values
Additional calculations	Data entry and computation of simple hydrogeological calculations
Ammonium calculator	Data entry and conversion for different laboratory analysis of ammonium
Porosity calculator	Data entry and calculation of water-filled porosities
Attenuation calc_sat_zone	Calculation of attenuation factor in the saturated zone

Data entry is only possible in eight of the worksheets (as highlighted in blue in Table 3.1). Each of these eight worksheets also presents the results of each calculation. The calculations themselves are carried out in the remaining worksheets which are provided for reference.

Each worksheet is password protected and data may only be entered in specific cells. The cells are colour-coded as detailed in Table 3.2.

Table 3.2 Colour scheme for the worksheets

Blue cells require data to be entered, to either perform a specified calculation, or to record site details. Data may take the form of either site details as text (on the Introduction sheet) or values for identified parameters (on all other sheets). All blue cells must be completed for each assessment type
<b>Brown cells</b> are pull-down menus where options can be selected to allow the assessor to select a predefined option
Yellow cells should be used to record the origin or source of any data used in the worksheet. Although failure to populate the 'Source of parameter value' cells with appropriate text will not affect the spreadsheet calculations, it is good practice to complete this task. We will expect submitted reports to include these details
Grey cells contain the results of each simulation
Green cells contain information derived from another part of the worksheet

If you move the cursor over the red triangles at the corner of certain cells, further information is revealed on the data required or equations solved. Please also refer to Figure 3.2.

### 3.2 Introduction worksheet

When starting a new assessment, you must complete details on the Introduction worksheet first (Figure 3.1). This worksheet is displayed for all assessment options.

Data required (in blue boxes) on the Introduction worksheet include:

- name and address of the site being assessed;
- name of assessor, date that assessment was completed, and run version number;
- name of substance;
- environmental standard used to derive the compliance value; and
- basis for environmental standard (for example, EQS, DWS, MRV, background quality).

You must complete all blue cells on the Introduction worksheet before moving onto any other worksheets. Data entered for the substance name, environmental standard, site name, assessor's name, date of assessment and identifying run number are automatically transferred to each of the subsequent data entry sheets. These details cannot be amended

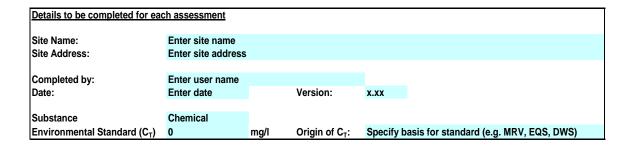
within the subsequent worksheets, and can only be modified by changing the entry on the Introduction worksheet.

The Introduction worksheet also includes brief instructions on the use of the worksheet and a reminder that Microsoft Excel 2002<sup>TM</sup> Tools must be enabled to allow it to calculate error functions and complimentary error functions. The worksheet will not calculate attenuation factors, unless Microsoft Excel<sup>TM</sup> is set-up to calculate these mathematical functions.

It is necessary to undertake a separate simulation for each substance in the treated effluent.

You can find guidance on selecting an appropriate environmental standard, which are typically based on background water quality, Minimum Reporting Values (MRVs), drinking water standards (DWS) or environmental quality standards (EQS), in Environment Agency 2011a and 2011b. See also Box 1.1.

Figure 3.1 Data entry required on Infiltration Introduction Worksheet



### 3.3 Infiltration System worksheet

The Infiltration System worksheet (Figure 3.2) allows you to specify the concentration of the substance in the treated effluent and to enter details of the infiltration system.

Project information data (site and pollutant details) are automatically transferred to this worksheet from the Introduction worksheet.

The Infiltration System worksheet provides the following options (brown cells):

- **1. Specify the type of treatment plant.** Four options are provided:
  - Septic tank.
  - 2. Package treatment plant.
  - 3. Treatment plant.
  - 4. Other.

For septic tanks and package treatment plants you can input the following information:

- Number of persons (p). Number of individuals served by the system. This information is used to calculate total discharge and the area of the drainage field.
- Water use (litres/person/day). Typical rates of sewage generation (in litres per person per day) are given in British Water Flows and Loads 4 (British Water, 2014).
- Percolation rate (Vp). The percolation rate should be taken from percolation tests undertaken according to BS6297:2007 + A1:2008. This rate is used together with the number of persons to calculate the area of the drainage field (See Box 3.1).

#### **2. Discharge rate.** Two options are provided:

- 1. Enter the discharge rate
- 2. Calculate discharge rate (this option is only available for septic tanks and package treatment plants (see Box 3.1).

### **3. Area of drainage field.** Two options are provided:

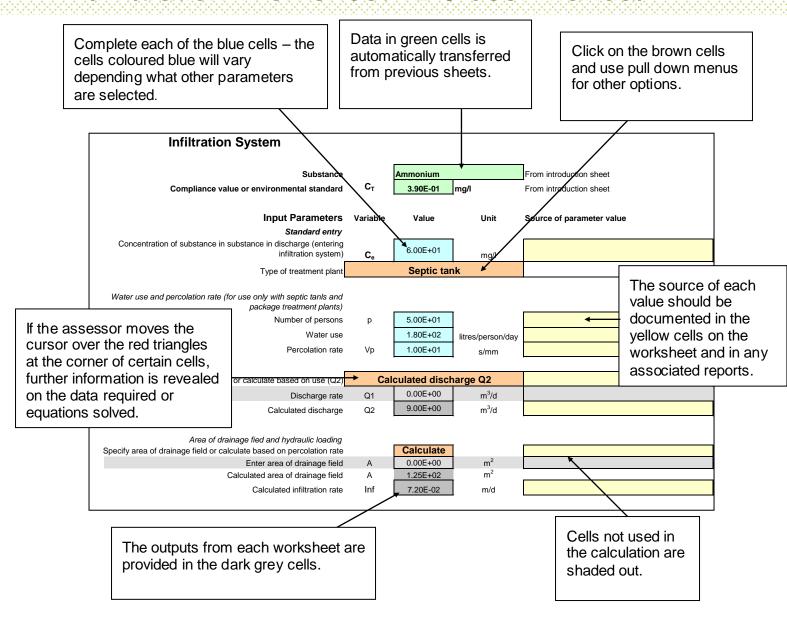
- 1. Enter the area of the drainage field.
- 2. Calculated area of the drainage field (this option is only available for septic tanks and package treatment plants (see Box 3.1).

A summary of the data requirements (blue cells) for this worksheet is given in Table 3.3. Depending on the options selected the worksheet will automatically grey out cells for which data entry is not required.

The Infiltration System worksheet calculates the following results:

- **Discharge rate** (m³/day) based on the number of persons and water use (this option is only available for septic tanks and package treatment plants);
- Area of the drainage field (m²) based on the number of persons and percolation rate derived from testing (this option is only available for septic tanks and package treatment plants);
- Infiltration rate (m/day) over the discharge area. This rate is used in subsequent calculations.

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**Figure 3.2 Examples of the main functionality.** The Infiltration System worksheet (which has been used as an example here) calculates the discharge and infiltration rates. It can also calculate the Area of the Drainage Field (depending on what option is selected).

### Box 3.1 Standard equations for the Infiltration System worksheet

The **hydraulic loading or infiltration rate (Inf)** is calculated from:

$$Inf = \frac{Q}{A}$$
 (Equation 1)

where:

Inf = Infiltration rate through the infiltration system (m/d)

Q = discharge rate to drainage field (m<sup>3</sup>/d).

A =area of drainage field (m<sup>2</sup>) (see below)

Note: The infiltration rate (*Inf*) should not exceed the maximum infiltration rate from BS 6297:2007 + A1:2008. This would indicate re-design of the drainage field was necessary. For some infiltration systems the design may include for storage to deal with peak flows, in these cases the infiltration rate should be set as the maximum infiltration rate.

The **discharge rate (Q)** is calculated as follows:

$$Q = p.W$$
 (x 1 000: m³/day to litres) (Equation 2)

where:

Q = discharge rate to drainage field (m<sup>3</sup>/d).

p = number of people served by the septic tank or package treatment plant

W = water use per person (litres/person/day)

The **area of a drainage field (A)** for domestic premises is calculated from (BS 6297:2007 + A1:2008):

$$A = (0.25) p.V_p$$
 for septic tanks (Equation 3)

$$A = (0.20) p.V_p$$
 for package treatment plants (Equation 4)

where:

A =area of drainage field (m<sup>2</sup>)

p = number of people served by the septic tank or package treatment plant

 $V_p$  = percolation rate determined from percolation tests undertaken according to BS6297:2007 + A1:2008 (sec/mm)

Table 3.3 Summary of data requirements for the Infiltration System worksheet

Input parameter		Units	Comment	Other	
Concentration of substance in treated effluent discharge	C <sub>e</sub>	mg/l	Measured or taken from an agreed reference	Must be input	
Number of persons	p		Number of people served by the septic tank or package treatment plant	Dependent	
Water use		litres/person/day	Information on typical rates of sewage generation can be obtained from British Water (2014)	on option selected	
Percolation rate	V <sub>p</sub>	sec/mm	Rate should be determined as set out in BS6297:2007 + A1:2008		
Discharge rate	Q <sub>1</sub>	m <sup>3</sup> /day	Measured or calculated based on number of persons or water use	Dependent on option selected	
Area of drainage field	A	m <sup>2</sup>	Measured or calculated based on number of persons and percolation rate	Dependent on option selected	

#### 3.4 Attenuation in Unsaturated Zone worksheet

The Attenuation in Unsaturated Zone worksheet (Figure 3.3) allows you to:

- calculate an attenuation factor (if degradation occurs) for the drainage layer (if present);
- calculate an attenuation factor (if degradation occurs) for the unsaturated zone;
- determine the concentration of the substance at the base of the unsaturated zone;
   and
- calculate a provisional discharge limit value. This limit may be superseded if dilution and attenuation in the saturated zone are taken into account.

Project information data (such as, site and substance details and infiltration rate) are automatically transferred to this worksheet.

The Attenuation in Unsaturated Zone worksheet provides the following options (brown cells):

- 1. **Degradation**. Three options are provided:
  - 1. No degradation occurs. In this case the attenuation factor will be set as 1.
  - Degradation occurs in the dissolved phase only (degradation measured in the
    aqueous phase such as in aqueous laboratory experiments) and the user will
    need to enter a half life for degradation. This half life is likely to overestimate the
    rate of degradation in groundwater and therefore it is corrected by multiplying it
    by the retardation factor.
  - 3. Degradation occurs in the dissolved and sorbed phase (degradation measured from field observations or laboratory experiments of the whole system that is both the dissolved and sorbed phases) and the user will need to enter a half life for degradation. This half life will be used in the calculation of an attenuation factor.

This option applies to the drainage layer and the unsaturated zone.

It is essential that you should be able to support the case for degradation. Please refer to Section 5.0. If no evidence for degradation is provided, you should select the option: 'No degradation occurs.'

- 2. Soil-water partition coefficients. Two options are provided:
  - 1. Specify partition coefficient (typically used for inorganics such as metals and ammonium).
  - 2. Calculate partition coefficient (non-polar organic substances only) based on fraction of organic carbon and organic carbon partition coefficient (see Box 3.2).

This option applies to the drainage layer and the unsaturated zone.

A summary of the data requirements (blue cells) for this worksheet is given in Table 3.3. Depending on the options selected, the worksheet will automatically grey out cells for which data entry is not required.

The worksheet will calculate the following (see also Box 3.2):

- Attenuation factor for the drainage layer;
- Attenuation factor for the unsaturated zone:
- Concentration of substance at base of the unsaturated zone; and
- Provisional discharge limit value (DL<sub>1</sub>).

Additionally the worksheet will calculate:

- Dispersivity (taken as 10% of the thickness of the unsaturated zone);
- Decay rate for degradation;
- Soil-water partition coefficient (for non-polar organics);
- Retardation factor;
- Unretarded travel time of substance through the drainage layer and unsaturated zone, with no dispersion;
- Unretarded and retarded travel time through the drainage layer and unsaturated zone, with dispersion.

Figure 3.3 Attenuation in Unsaturated Zone worksheet

Attenuation unsaturated zone				
Contaminant		Ammonium		From introduction sheet
Compliance value or environmental standard	CT	5.00E-01	mg/l	From introduction sheet
Concentration of substance in substance in discharge (entering infiltration system	Ce	2.30E+01	mg/l	From infiltration sheet
Input Parameters	Variable	Value	Unit	Source of parameter value
Drainage Layer Infiltraton rate	Inf	9.00E-02	m/d	Frominfiltration sheet
Thickness ofdrainage layer		2.00E+00	m	
Water filled porosity	θ1	1.00E-01	fraction	
Bulk density		1.80E+00	g/cm <sup>3</sup>	
Calculated dispersivity		2.00E-01	m	calculated
Option to select degradation		Degradation occurs - sorbed and dissolved p	hases	
Halflife for degradation of substance	t1/2	7.30E+02	days	
Calculated decay rate	λ1	9.50E-04	days <sup>-1</sup>	calculated (very low value set if no degradation)
Entermethod of defining partition co-efficient (using pull down list)		User specified value for partition coefficie	nt	
Entry if specify partition coefficient (option				
Soil water partition coefficien  Entry for organic chemicals (option,	Kd1	1.00E+00	l∕kg	
Fraction of organic carbon (in soil) Organic carbon partition coefficien		1.00E-02 1.00E+01	fraction Vkg	
Soil water partition coefficient used in assessmen	Kd1	1.00E+00	Vkg	Specified value
Retardation factor		1.90E+01	•	
Unretarded travel time (no dispersion)		2.22E+00	d	
Unretarded travel time (with dispersion) Retarded travel time (with dispersion)		2.00E+00 3.80E+01	d d	
Attenuation factor		1.04E+00	ď	
Unsaturated Zone				
Thickness of unsaturated zone below drainage field Water filled porosity	S <sup>2</sup> θ <sup>2</sup>	1.00E+01 1.00E-01	m fraction	
Bulk density of unsaturated zone		1.80E+00	g/cm <sup>3</sup>	
Calculated dispersivity		1.00E+00	m	calculated
Option to select degradation		Degradation occurs - sorbed and dissolved p	hases	
Half life for degradation of substance	t1/2	7.30E+02	days	
Calculated decay rate	$\lambda^2$	9.50E-04	days <sup>-1</sup>	calculated (very low value set if no degradation)
Fraction of rapid flow through unsaturated zone	В	0.00E+00	fraction	
Entermethod of defining partition co-efficient (using pull down list)		User specified value for partition coefficie	nt	
Entry if specify partition coefficient (option, Soil water partition coefficien	Kd <sup>2</sup>	1.00E+00	l/kg	
Entry for organic chemicals (option,			9	
Fraction of organic carbon (in soil) Organic carbon partition coefficien		1.00E-02 1.00E+01	fraction I/kg	
Soil water partition coefficient used in assessment		1.00E+00	Vkg	Specified value
Retardation factor		1.90E+01		
Unretarded travel time (no dispersion) Unretarded travel time (with dispersion)		1.11E+01 1.00E+01	d d	
Retarded travel time (with dispersion)		1.90E+02	d	
Attenuation factor	AFu <sup>2</sup>	1.22E+00		
Total unretarded travel time	tu1+tu2	1.33E+01	d	
Total retarded travel time	tr1+tr2	2.53E+02	d	
Attenuation factor and discharge consent limit				
Drainage layer attenuation factor		1.04E+00		
Unsaturated zone attenuation factor  Concentration at base of drainage layer		1.22E+00 2.21E+01	mg/l	
Concentration at base of unsaturated zone		1.82E+01	mg/l	
				I
Discharge limit value		and 6.33E-01		

A Summary of data requirements for the Attenuation in the Unsaturated Zone worksheet is provided in Table 3.3

Table 3.3 Summary of data requirements for the Attenuation in the Unsaturated Zone worksheet (blue cells)

Input parameter		Units	Comment	
Drainage layer thickness and unsaturated zone thickness (below the drainage field)	S <sub>1</sub> , S <sub>2</sub>	m	Essential to have site specific measurement.	Must be input
Water filled porosity of the drainage layer and the unsaturated zone	$\theta_{w1}, \\ \theta_{w2}$	fraction	Expressed as a fraction between 0 and the total porosity value. The water filled porosity value can be derived from water or moisture content measurement and density measurements.	Must be input
Dry bulk density of drainage layer and unsaturated zone material	$\rho_1, \rho_2$	g/cm <sup>3</sup>		Must be input
Half life for degradation of substance	t <sub>1/2</sub>	days <sup>-1</sup>	See Section 5.0. Separate entry for drainage layer and unsaturated zone	Dependent on option selected
Percent rapid flow through the unsaturated zone	В	fraction	Set as 0 if no by-pass.	Must be input
Fraction of organic carbon for the drainage layer and unsaturated zone	foc <sub>1</sub> , foc <sub>2</sub>		Expressed as a fraction between 0 and 1.	Must be input when non-polar organic chemicals option is selected
Organic carbon partition coefficient of substance	Koc <sub>1</sub> , Koc <sub>2</sub>		Contaminant specific value which describes the partitioning of a substance between organic matter and water.	Must be input when non-polar organic chemicals option is selected
Soil water partition coefficient for movement of contaminant through drainage layer and unsaturated zone	Kd₁, Kd₂		Describes the partitioning of a substance between water and the soil matrix in the unsaturated zone. Soil water partition coefficients will typically be derived from literature sources,	Dependent on option selected

Input parameter	Units	Comment	
		laboratory column experiments, or field data where comparison with a conservative tracer is possible. If a literature source is used it is important to ensure that it is relevant to the unsaturated zone material. For conservative contaminants the Kd value should be set at zero	

Box 3.2 gives an overview of the standard equations used in the Attenuation in the Unsaturated Zone worksheet.

## Box 3.2 Standard equations for Attenuation in Unsaturated Zone worksheet

**Decay rate** ( $\lambda$ ) is calculated from:

 $\lambda = \ln(2)/H$  (Equation 1)

where:

 $\lambda$  = drainage layer or unsaturated zone decay constant (d<sup>-1</sup>)

H = Half life for degradation of substance (d)

**Vertical dispersivity** ( $\alpha$ ) in the drainage layer and unsaturated zone is calculated from:

 $\alpha = 0.1.S$  (Equation 2)

 $S = \text{thickness of drainage layer } (S_1) \text{ or unsaturated zone } (S_2) \text{ below the drainage field } (m)$ 

**Soil-water partition coefficient (Kd)** is calculated for non-polar organics from:

$$K_d = K_{oc} \cdot f_{oc}$$
 (Equation 3)

where:

Koc = Organic carbon partition coefficient (I/kg)

foc = fraction of organic carbon

### Box 3.2 continued

Retardation Factor in the drainage layer or unsaturated zone (*Rfu*) is calculated from:

$$Rfu = 1 + Kd.\rho/\theta_{W}$$
 (Equation 4)

where:

 $\theta_w$  = water filled porosity of the drainage layer ( $\theta_{w1}$ ) or unsaturated zone ( $\theta_{w2}$ )(fraction) p = dry bulk density of the drainage layer ( $p_1$ ) or unsaturated zone ( $p_2$ )(g/cm<sup>3</sup>)

The **unretarded travel time** (*tu*) through the drainage layer or unsaturated zone is calculated from:

 $tu = S.\theta / Inf$  (Equation 5)

where:

*Inf* = Infiltration rate through the infiltration system (m/d)

The retarded travel time (tr) through the drainage layer or unsaturated zone is calculated from:

$$tr = tu.Rfu$$
 (Equation 6)

The above calculation for unretarded travel times ignores dispersion; if dispersion is taken into account the travel time is calculated from:

$$tu = (S - \alpha)\theta / Inf$$
 (Equation 7)

An attenuation factor (AFu) for the drainage layer or unsaturated zone can be calculated from:

$$AFu = 1/\exp\left[\frac{S}{2\alpha} - \left\{\frac{S}{2\alpha}\sqrt{1 + \left(4a\lambda/v_{ur}\right)}\right\}\right]$$
 (Equation 8)

where:

 $v_{ur}$  = retarded contaminant velocity through the drainage layer or unsaturated zone (m)

$$v_{ur} = \left( Inf / \theta_{v} \right) / R$$
 (Equation 9)

a = longitudinal dispersivity (m)

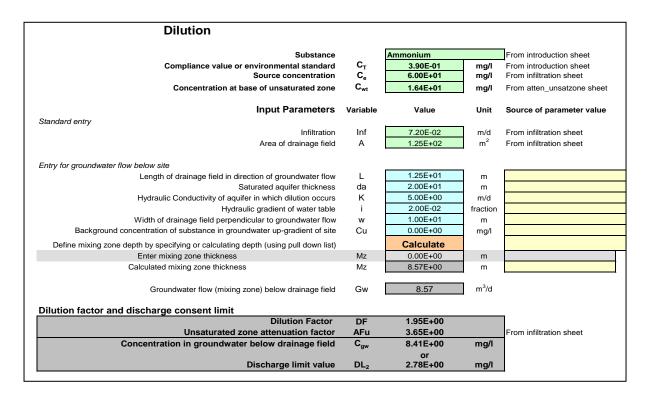
#### 3.5 Dilution worksheet

The Dilution worksheet (Figure 3.4) allows users to:

- Calculate a dilution factor to account for dilution by groundwater flow below the drainage field (Box 3.3);
- Determine the concentration of the substance in groundwater immediately downgradient of the drainage field; and
- calculate a provisional discharge limit value. This limit may be superseded if attenuation in the saturated zone is taken into account (Section 3.6).

Project information data (for example, site and substance details, and unsaturated zone attenuation factor) are automatically transferred to this worksheet.

Figure 3.4 Dilution worksheet



The worksheet provides the following option (brown cells):

#### Mixing Zone thickness. Two options are provided:

- 1. Specify the thickness of the mixing zone.
- 2. Calculate thickness of the mixing zone (see Box 3.3).

A summary of the data requirements (blue cells) for this worksheet is given in Table 3.4. Depending on the options selected the worksheet will automatically grey out cells for which data entry is not required.

The Dilution worksheet will calculate the following (see Box 3.3):

- Dilution factor, to account for dilution by groundwater flow below the drainage field;
- Concentration of substance in groundwater immediately down-gradient of the drainage field; and
- Provisional discharge limit value (DL<sub>2</sub>).

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### Box 3.3 Standard Equations for the Dilution worksheet

The **dilution factor (DF)** for groundwater below the drainage field can be calculated from:

$$DF = \frac{(G_w + Inf.A).C_t - (G_w.C_u)}{Inf.A.C_t}$$
 (Equation 1)

and

 $G_w = K.i.w_d.M_z$  (Equation 2)

where:

Gw = groundwater flow (mixing zone) below drainage field (m<sup>3</sup>/d)

K = hydraulic conductivity (m/day)

*i* = hydraulic gradient

 $w_d$  = width of disposal field perpendicular to flow direction (m)

 $M_z$  = mixing zone thickness (m)

Inf = infiltration rate (m/day)

A =area of drainage field (m<sup>2</sup>)

 $C_t$  = Environmental standard used to derive compliance value (mg//l)

 $C_u$  = background concentration of substance in groundwater immediately up-gradient of discharge field (mg/l)

The mixing zone thickness can be calculated as follows:

$$M_z = \sqrt{0.0112L^2 + da} \left[ 1 - \exp\left(\frac{-L.Inf}{K.i.da}\right) \right]$$
 (Equation 3)

where:

L = length of drainage field parallel to groundwater flow (m)

da = aquifer thickness (m)

Table 3.4 Summary of data requirements for the Dilution worksheet (blue cells)

Input parameter		Units	Comment	
Length of drainage field in direction of groundwater flow	L	m	See comment on width of drainage field	Must be input
Saturated aquifer thickness	da	m		Must be input
Hydraulic conductivity of aquifer in which dilution occurs	K	m/d		Must be input
Hydraulic gradient of water table	i	fraction		Must be input
Width of drainage field perpendicular to groundwater flow	W <sub>d</sub>	m	The worksheet automatically multiplies L.Wd and compares this with the area of the drainage field. If they are the same the worksheet flags this (w * L does not equal area (A) of drainage field - check parameters used). This may be OK if drainage field is at angle to flow direction and no change in input parameters may be necessary	Must be input
Background concentration of substance in groundwater up hydraulic gradient of the site	Cu	mg/l		Must be input
Mixing zone thickness of saturated aquifer below drainage field	M <sub>z</sub>	m	The thickness of the mixing zone cannot exceed the saturated thickness of the aquifer. If a value greater than the saturated aquifer thickness is entered, the worksheet posts a warning that "mixing zone exceeds saturated thickness".  Generally, the full thickness of the aquifer will not be available for mixing of contaminants, and a lesser thickness may be derived from evidence of high permeability zones from borehole logs, annual water table fluctuation from	Dependent on option selected

Input parameter	Units	Comment	
		hydrographs, or local experience. Many UK aquifers are layered systems with significant vertical heterogeneity that limits the potential for vertical mixing.	

#### 3.6 Attenuation in the Saturated Zone worksheet

The Attenuation in Saturated Zone worksheet (Figure 3.5) allows users to:

- Calculate an attenuation factor for the saturated zone (if degradation occurs) (see Box 3.4);
- Determine the concentration of the substance at a compliance point located downgradient of the drainage field (see Box 3.4); and
- Calculate a provisional discharge limit value (see Box 2.2).

Project information data (such as, site and substance details and dilution factor) are automatically transferred to this worksheet from the previous sheets (green cells).

The worksheet provides the following options (brown cells):

- **Degradation**. Three options are provided:
  - 1. No degradation occurs. In this case the attenuation factor will be set as 1.
  - Degradation occurs in the dissolved phase only (degradation measured in the
    aqueous phase such as in aqueous laboratory experiments) and the user will
    need to enter a half life for degradation. This half life is likely to overestimate the
    rate of degradation in groundwater and therefore it is corrected by multiplying it
    by the retardation factor.
  - 3. Degradation occurs in the dissolved and sorbed phase (degradation measured from field observations or laboratory experiments of the whole system that is both the dissolved and sorbed phases) and the user will need to enter a half life for degradation. This half life will be used in the calculation of an attenuation factor.

It is essential that you should be able to support the case for degradation. Please refer to Section 5.0. If no evidence for degradation is provided, you should select the option: 'No degradation occurs.'

- **2 Partition coefficients.** Two options are provided:
  - Specify partition coefficient (typically used for inorganics such as metals and ammonium).

- 2. Calculate partition coefficient (non-polar organic substances only) based on fraction of organic carbon and organic carbon partition coefficient (see Box 3.2).
- 3 **Dispersivity**. Three options are provided:
  - 1. Enter user defined dispersivity values.
  - 2. Calculate dispersivity based on length of flow path (see Box 3.4).
  - 3. Calculate dispersivity using Xu and Eckstein (1995) (see Box 3.4).
- 4 **Time**. Two options are provided:
  - 1. Steady state. Use this to determine discharge limit values.
  - 2. Enter time. Use this to validate the assessment if monitoring data are available.

A summary of the data requirements (blue cells) for this worksheet is given in Table 3.5. Depending on the options selected the worksheet will automatically grey out cells for which data entry is not required.

### 3.7 Calculated parameters

The Attenuation in the Saturated Zone worksheet will calculate the following:

- Attenuation factor for the saturated zone:
- Concentration of substance at a compliance point located down hydraulic gradient from the drainage field; and
- Provisional discharge limit value (DL<sub>3</sub>).

#### Additionally:

- Decay rate for degradation;
- Hydraulic gradient (the hydraulic gradient entered in the previous worksheet is corrected to ensure that groundwater fluxes up and down-gradient of the drainage field balance):
- Soil-water partition coefficient (for non-polar organics);
- Retardation factor;
- Groundwater flow velocity and rate of contaminant flow due to retardation:
- Graph (Figure 3.6) showing variation in contaminant concentrations down-gradient of the source. It may be necessary to manually change the graph axes by clicking on the graph and selecting for format selected axes option (scale) in Excel; and
- Table giving calculated concentrations in groundwater between the source and the compliance point.

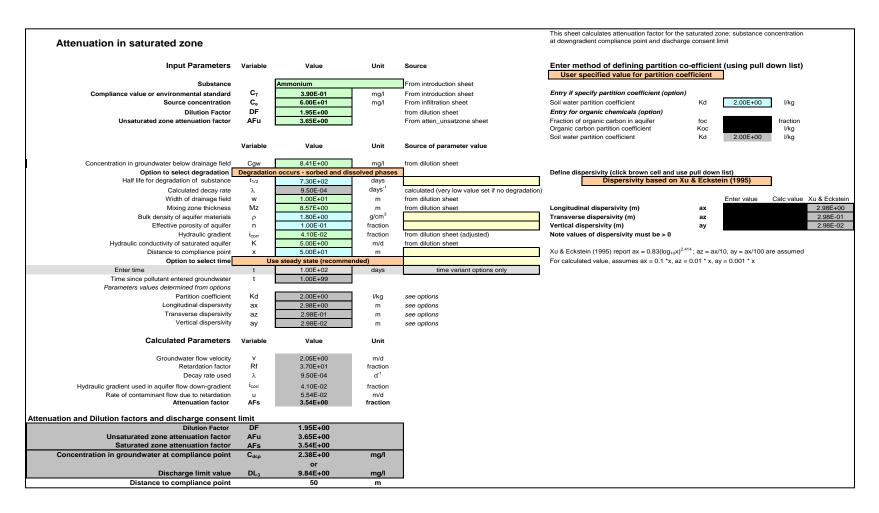


Figure 3.5 Attenuation in Saturated Zone worksheet

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Table 3.5 Summary of data requirements for Attenuation in Saturated Zone worksheet (blue cells)

Input parameter		Units	Comment	
Distance to compliance point	X	m	The distance from the source to the point at which compliance with an environmental standard is required.	Must be input
Effective porosity of the aquifer	$\theta_{\sf w}$	fraction	In fissured and dual porosity aquifers, the effective porosity may be assumed to be the fissure porosity.	Must be input
Dry Bulk density of the aquifer material	ρ	g/cm <sup>3</sup>		Must be input
Half life for degradation of substance	t <sub>1/2</sub>	days	See Section 5.0.	Dependent on option selected
Time	t	days	Time since substance entered groundwater.	Dependent on option selected
Soil water partition coefficient	K <sub>d</sub>		Contaminant specific value, K <sub>d</sub> , which describes the partitioning of a substance between the aquifer matrix and surrounding water. Soil water partition coefficients will typically be derived from laboratory column experiments or field data where comparison with a conservative tracer is possible. If a substance is conservative (for example, it does not sorb to aquifer materials), the Kd value should be set to zero.	Dependent on option selected
Fraction of organic carbon	foc		Expressed as a fraction between 0 and 1.	
Organic carbon partition coefficient	Koc		Contaminant specific value which describes the partitioning of a substance between organic matter and water.	

Table 3.5 continued

Input parameter		Units	Comment	
Longitudinal, transverse and vertical dispersivity	a, a <sub>y</sub> , a <sub>z</sub>	m	Values for dispersivity may be obtained from tracer testing or experience of local hydrogeological conditions.	Dependent on option selected
			A check should be undertaken to ensure that the modelled effects of vertical dispersion are not so great as to simulate a plume that extends beyond the base of the aquifer. The worksheet will post a warning if this occurs "Dispersed plume thickness exceeds aquifer thickness! Reduce vertical dispersivity". In these cases the value for vertical dispersivity should be reduced. This can only be achieved under the option to enter dispersivity values.	

Box 3.4 gives an overview of the equations used in the Attenuation in the Saturated Zone worksheet.

## Box 3.4 Standard equations for Attenuation in Saturated Zone worksheet

#### **Decay rate** ( $\lambda$ ) is calculated from:

$$\lambda = \ln(2)/H$$
 (Equation 1)

where:

 $\lambda$  = unsaturated zone decay constant (d<sup>-1</sup>)

 $H = t \frac{1}{2}$  (half life(days)

### Soil water partition coefficient (Kd) is calculated from:

$$K_d = K_{oc} \cdot f_{oc}$$
 (Equation 2)

where:

Koc = Organic carbon partition coefficient (I/kg)

foc = fraction of organic carbon of aquifer material

#### **Retardation Factor (***Rf***)** in the saturated zone is calculated from:

$$Rf = 1 + Kd.n/\rho$$
 (Equation 3)

where:

n = effective porosity of aquifer material (fraction) (if fissure porosity used the partition coefficient should be set as 0)

 $p = \text{dry bulk density of aquifer (g/cm}^3)$ 

#### Values for dispersivity are calculated using either:

1. Xu and Eckstein

$$a_x = 0.83(\log x)^{2.414}$$
 (Equation 4)

 $a_z = 0.01x$  and  $a_y = 0.001x$  or

2.

$$a_x = 0.1x$$
 and  $a_z = 0.01x$  and  $a_y = 0.001x$  (Equation 5)

where:

 $\alpha_{\rm x}$ ,  $\alpha_{\rm z}$   $\alpha_{\rm v}$  = longitudinal, transversal and vertical dispersivity (m)

x =distance to down-gradient compliance point (m)

#### The worksheet adjusts the hydraulic gradient (i) as follows

$$i_{adjusted} = i \cdot \left\{ \frac{DF}{DF - 1} \right\}$$
 DF = dilution factor. (Equation 6)

This adjustment is undertaken to ensure that groundwater fluxes up and down-gradient of the drainage field balance

### Box 3.4 continued

The **unretarded groundwater velocity** (v) through the saturated zone is calculated from:

v = K.i/n (Equation 7)

The **retarded groundwater velocity** (u) through the saturated zone is calculated from:

$$u = v/R$$
 (Equation 8)

K = hydraulic conductivity of aquifer in which dilution occurs (m/d)

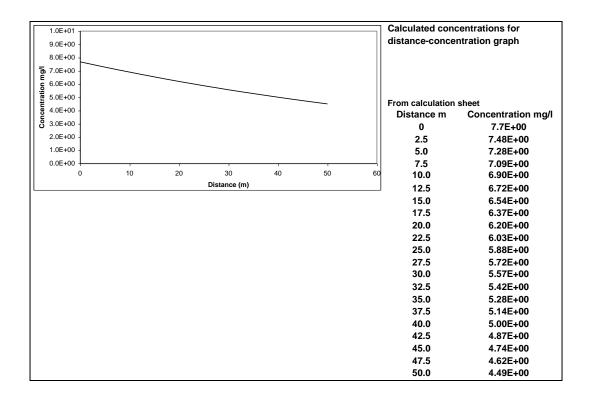
The attenuation factor (AFs) for the saturated zone is calculated from:

$$\begin{aligned} \exp\left\{\frac{x}{2a_{x}}\left(1-\sqrt{\left[1+\frac{4\lambda a_{x}}{u}\right]}\right)\right\} \cdot erfc\left\{\frac{1}{2\sqrt{a_{x}ut}}\cdot\left(x-ut\sqrt{\left[1+\frac{4\lambda a_{x}}{u}\right]}\right)\right\} \\ + \exp\left\{\frac{x}{2a_{x}}\left(1+\sqrt{\left[1+\frac{4\lambda a_{x}}{u}\right]}\right)\right\} \cdot erfc\left\{\frac{1}{2\sqrt{a_{x}ut}}\cdot\left(x+ut\sqrt{\left[1+\frac{4\lambda a_{x}}{u}\right]}\right)\right\} \\ \cdot \left[erf\left\{\frac{z+\frac{S_{z}}{2}}{2\sqrt{a_{z}x}}\right\} - erf\left\{\frac{z-\frac{S_{z}}{2}}{2\sqrt{a_{z}x}}\right\}\right] \cdot \left[erf\left\{\frac{y+S_{y}}{2\sqrt{a_{y}x}}\right\} - erf\left\{\frac{y-S_{y}}{2\sqrt{a_{y}x}}\right\}\right] \end{aligned}$$

where:

erf and erfc are error function and complementary error functions respectively

Figure 3.6 Calculated concentrations in the Attenuation in the Saturated Zone worksheet



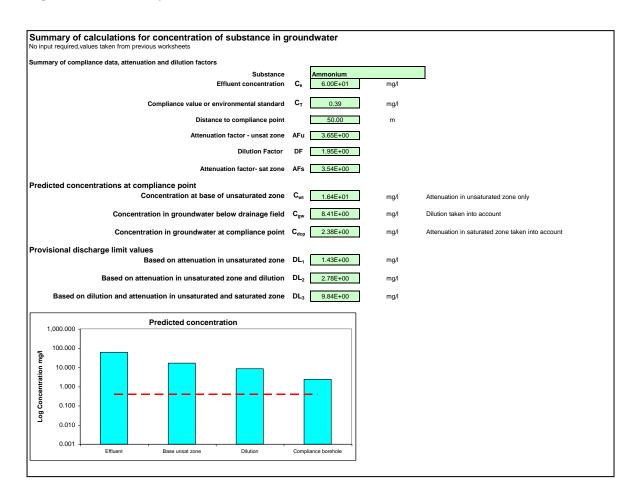
### 3.8 Summary calculations worksheet

The Summary worksheet (Figure 3.7) requires no input as it presents data from previous worksheets and provides:

- A summary of compliance point data, dilution and attenuation factors;
- Calculated substance concentration at different points along the pathway (base of unsaturated zone, groundwater immediately down-gradient of drainage field, and groundwater down-gradient of the drainage field);
- Provisional discharge limit values for different points along the pathway.

The Summary worksheet also includes a chart that summarises calculated concentrations between the source and the down-gradient compliance point.

Figure 3.7 Summary calculations worksheet



#### 4.0 Additional worksheets

#### 4.1 Hydrogeological Calculations worksheet

The hydrogeological calculations worksheet (Figure 4.1) allows you to calculate a range of standard calculations that are frequently used by hydrogeologists.

Data requirements for some of the calculations are described in the comments boxes, noted by a red tick in the corner of relevant cells. The calculations performed are summarised below:

**Table 4.1 Hydrogeological calculations**. These are independent of the worksheet calculations.

Calculation	Equation	
Groundwater flow velocity	v <sub>GW</sub> = (K . i) / n	
Time for GW to reach to receptor	$t_{GW} = (n \times distance) / (K . i)$	
Volume of GW flowing through aquifer	$Q = K \cdot A \cdot \times I$ (where $A = b \cdot x$ )	
Retardation factor, R <sub>f</sub>	$R_f = 1 + [(K_d . \rho) / n]$	
Contaminant flow velocity	$v_{contam} = (K . i) / (n . R_f)$	
Time for contaminant to reach receptor	$t_{contam} = (n . R_f . distance) / (K . i)$	

Figure 4.1 Hydrogeological calculations worksheet.

Parameter	symbol	-	unit	justification	
Hydraulic conductivity	K	1.00E+01	m/d		
Hydraulic gradient	i	1.00E-02	unitless		
Effective porosity of aquifer	n	1.00E-01	fraction		
Thickness of saturated aquifer	b	5.00E+01	T <sub>m</sub>		
Width of aquifer perpendicular to flow	w	5.00E+01	m		
Distance to receptor	x	1.00E+02	m		
Bulk density of aquifer materials	î	1.80E+00	g/cm <sup>3</sup>		
Soil-water partition co-efficient	Kd	1.00E+00	I/kg		
Retardation factor of pollutant	R	19	l/kg		
· ·			-	<u></u>	
Groundwater flow velocity	v(GW)	1.16E-05	m/s	1.00E+00 m/day	3.65E+02 m/year
Time for groundwater to reach receptor	t(GW)	8.64E+06	seconds	1.00E+02 days	2.74E-01 years
Rate of groundwater flow through aquifer	Q	2.89E-03	m³/s	2.50E+02 m <sup>3</sup> /day	9.13E+04 m <sup>3</sup> /year
Contaminant flow velocity	v(contam)	6.09E-07	m/s	5.26E-02 m/day	1.92E+01 m/year
Time for contaminant to reach receptor	t(contam)	1.64E+08	seconds	1.90E+03 days	5.21E+00 vears

#### 4.2 Ammonium Conversion worksheet

This Ammonium Conversion worksheet allows conversion between different laboratory analyses of ammonium.

The ammonium ion (NH<sub>4</sub>) is typically the dominant ion at neutral pH. However, in more alkaline water the ammonia (NH<sub>3</sub>) ion becomes increasingly dominant.

Laboratories may report the analysis for ammonium as  $(NH_4)$  or as  $N(NH_4-N)$ . In some cases the laboratory may have reported the result as Total ammonia (as  $NH_3$ ) or as Total ammonia as N. Total ammonia is likely to include ammonium  $(NH_4)$  and ammonia  $(NH_3)$ . In this case  $NH_4$  may be converted to  $NH_3$ .

#### 4.3 Porosity Calculator worksheet

Water filled porosities can be difficult parameters to measure directly at a site area but can be estimated from soil bulk density (wet or dry), particle density and moisture content. The calculations presented in the Porosity Calculator worksheet (Box 4.1) are suitable for inclusion within the Attenuation in the Unsaturated Zone worksheets but not the effective porosity as used in the Attenuation in the Saturated Zone worksheet.

#### Box 4.1 Standard Equations for Porosity Calculator worksheet

The water filled porosity is calculated from:

$$\theta_W = (\theta_T) - (\theta_R)$$
 (Equation 1)

where:

$$\theta_T = 1 - \frac{\rho}{d}$$
 (Equation 2)

$$Vr = \frac{d}{\rho} - 1$$
 (Equation 3)

$$\theta a = \frac{(100 - S) * \theta r}{100}$$
 (Equation 4)

$$S = \frac{MC * d}{Vr}$$
 (Equation 5)

where:

 $\theta_w$  = water filled porosity (fraction)

 $\theta_a$  = air filled porosity (fraction)

 $\theta_T$  = total porosity (fraction)

p = dry bulk density of unsaturated zone (g/cm<sup>3</sup>)

d = particle density (g/cm<sup>3</sup>)

MC = moisture content (% weight)

S = initial saturation (%)

Vr = void ratio (fraction)

It is important to note that these equations cannot be used to calculate the effective porosities used for the saturated zone attenuation assessment worksheet.

#### 5.0 Degradation

The rate of degradation used for the unsaturated and saturated zone is likely to have a significant influence on calculated concentrations in groundwater and calculated discharge limit values. Guidance on the selection of degradation rates is given in Environment Agency (2011b) and additional information on transformation rates for ammonium is given in Environment Agency (2003).

Contaminant decay is modelled as a first order reaction and degradation is defined by a half-life expressed in days. Decay rates should be based on field observation of contaminant destruction in groundwater or on conservative literature values where their application is supported by field data. Any literature used must relate to the behaviour of the chemical under similar environmental conditions (for example, redox, pH, contaminant concentrations, temperature, presence of other substances, etc.). Guidance on assessing contaminant attenuation is given in Environment Agency R&D Publication 95 *Guidance on the assessment and monitoring of natural attenuation of contaminants in groundwater* (Environment Agency, 2000). If you are assessing contaminants that are not subject to degradation, such as heavy metals (non-radioisotopes) and chloride, or there is no evidence of degradation from field data, you should select the 'No degradation occurs' option.

For preference, you should obtain the degradation rates from studies which give a degradation rates that apply to both water and soil. If you have derived degradation rates from laboratory experiments based on water as the only phase this will overestimate the rate of degradation in groundwater, in which case you should select either the option 'No degradation occurs' or 'Degradation occurs in the dissolved phase only'.

#### 5.0 Interpretation of results

There are a number of critical factors for which there can be limited supporting literature or field data. In such cases the user is recommended to consider the following factors:

- Dilution Factors (DF) would be expected to be in the range 1 to 2; if higher values are calculated then you should check the thickness of the mixing zone and the hydraulic conductivity to see if they are reasonable. Dilution factors of greater than 10 should be treated with caution.
- Attenuation Factor AFu<sub>1</sub> (drainage blanket) values in range 1 to 5 are reasonable; higher values indicate degradation rates may be too rapid and input values should be checked.
- 3. Attenuation factor AFu<sub>2</sub> (unsaturated zone) values in range 1 to 3 are reasonable; higher values indicate degradation rates may be too rapid and input values should be checked, although may be reasonable if there is a thick unsaturated zone.
- 4. Attenuation factor AFs (saturated zone) values in range 1 to 3 are reasonable; higher values indicate degradation rates may be too rapid and input values should be checked. Higher values may be associated with higher porosity aquifers and/or where distances to the compliance point of greater than 100m have been used.
- 5. Have **conservative attenuation rates** been used (particularly for the unsaturated and saturated zone)? Half lives of less than 2 years should be treated with caution if justification is not provided, half lives of 2 to 5 are likely to be reasonable and half lives of greater than 5 years are likely to be precautionary.
- 6. **Dispersion co-efficients** for intergranular aquifers the Xu and Eckstein option is recommended, for fractured aquifers, the 10% option is recommended. For small drainage fields then lateral dispersion may be significant and in this case sensitivity testing is recommended (See Section 6).
- 7. **Predicted concentrations at the compliance** point should be compared with the target concentration as this may help to establish whether the discharge represents a significant risk or that further analysis would help to ascertain whether simple modifications to the design or location if the drainage field may reduce the risk to an acceptable level.
- 8. For **degradation**, the option "Degradation occurs sorbed and dissolved phases" should only be used where there is field evidence to support the degradation rates used. Where there is limited or no evidence, no attenuation should be assumed.

See Appendix A for further advice on the selection of appropriate input values.

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#### 6.0 Sensitivity analysis

The InfWS uses a deterministic approach in the calculation of contaminant concentration and discharge limit values; they assign a single value for each parameter, which implies a high degree of confidence in that value. In practice, there will be uncertainty. Sensitivity analysis is therefore recommended as part of the risk assessment process, especially where there is not a high degree of confidence in the single value assigned for each parameter. It is also useful in cases where the initial assessment indicates that the proposed permit limit for a substance is lower than its concentration in the treated effluent. Such testing may help to inform whether: further data collection is warranted, the site should be relocated or the design modified.

Understanding how the magnitude of risks varies with changes in input parameter values is essential to understanding the certainty that can be placed on any prediction.

By varying selected input parameters in turn and observing the effect on the calculated concentrations, you can determine which parameters have the greatest effect on the results. If you then consider the likely range of values that apply to those parameters you can assess whether more data is needed to reduce uncertainty in the final result. The alternative is to adopt conservative values for the sensitive parameters and accept that this may result in higher calculated discharge limit values. Whichever approach is taken you should ensure that your assumptions are sufficiently protective of the environment.

Another common means of taking account of parameter variability is the use of probabilistic methods, such as Monte Carlo analysis. This InfWS is password protected and this may prevent the use of common commercial tools, such as Crystal Ball<sup>TM</sup> and @Risk<sup>TM</sup>, to undertake Monte Carlo analysis. If Monte Carlo analysis is required, it is recommended that an alternative assessment tool, such as ConSim (Environment Agency, 2004) is used.

Further guidance on assigning values to uncertain parameters in subsurface contaminant fate and transport modelling is provided in Environment Agency (2001d).

Factors to be considered in a sensitivity analysis are:

- 1. **Degradation rates.** Where sensitivity testing shows the derived permit limit is highly sensitive to the degradation rate the use of a half life of less than 2 years shows there is a need for robust justification to support the assessment.
- 2. **Thickness of the unsaturated zone.** For example relocating the drainage field, if practical (new discharges), to an area characterised by a thicker unsaturated zone may result in an acceptable reduction in risk.
- 3. **Thickness of the drainage blanket.** Changing the design of the drainage blanket may result in an acceptable reduction in risk.
- 4. Investigate the area (dimension) and orientation of the drainage field in relation to groundwater flow. Increasing the area of the drainage field will decrease the rate of infiltration which may increase the potential for attenuation (for example, increased travel time through the unsaturated zone) and dilution at the water table. Changing the dimensions of the drainage field and or its orientation to groundwater flow, for example increasing the length (L) of drainage field in direction of groundwater flow will increase

dilution, although a check should be made that the dimensions are consistent with the area of the drainage field.

For some sites the model results may be insensitive to these changes (for example where there is a thin unsaturated zone or low groundwater flow rates) and other factors may need to be considered (for example relocating drainage field, reviewing distance to compliance point, increasing the thickness of drainage layer). It should be noted that in some cases, increasing L may reduce the influence of lateral dispersion on the model results and may lead to the model calculating lower permit limits which can be counter intuitive. In these cases the sensitivity of the model to dispersion should be investigated including the choice of the Xu and Eckstein option or dispersivity based on pathway length.

- 5. **Distance to the compliance point**. In some cases the analysis may indicate that changing the distance by  $\pm$  10 m may result in an acceptable concentration at the compliance point and therefore the current location may be reasonable.
- 6. **Hydraulic conductivity.** This parameter will influence the dilution and attenuation factors in the saturated zone. Site specific data are unlikely to be available and sensitivity analysis will be help to establish whether this is a key input parameter.
- 7. **Effluent concentration**. This may help to establish whether additional treatment should be considered.
- 8. **Dispersion co-efficient.** For small drainage fields, the model results can be sensitive to lateral and vertical dispersivity. Therefore, the influence of changing these parameters should be examined. This can be undertaken by noting the values calculated using the Xu & Eckstein or 10% option and then entering these using the user specified option and then modifying (e.g. ± 20%) as part of the sensitivity analyses.

#### 7.0 Assessment of results

In summary the factors that should be examined in carrying the risk assessment and which will influence our decision to reject or accept the application are:

- Predicted concentration at the compliance point;
- Input parameters and calculated factors (for example, DF, AF) and whether these are reasonable;
- Results of sensitivity testing and whether changes to the design and or location would result in a reduction in risk.

The InfWS can be used through the use of scoping calculations and sensitivity analysis to identify how the proposed discharge could be modified to result in an acceptable discharge (for example, treatment to reduce the concentrations of substances, increasing the area and thickness of the drainage layer or relocating the discharge to an area with a greater unsaturated zone thickness).

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## Appendix A

## Guidance for assessing appropriate input parameters for the InfWS v2.0

Worksheet	Factor/Section	Instructions
Introduction	Information to be completed for each assessment	Enter the site details, chemical, water quality standard (for example, 0.5 mg/l for Ammoniacal $-$ N), user, date, and version. The chemical information is taken through to subsequent sheets.
Infiltration System	Concentration of substance in discharge	For Ammoniacal Nitrogen, input 50 mg/l for septic tanks; 20 mg/l for package treatment plants (PTPs).
	Type of Treatment	Select type from pull down list: 'septic tank', 'package treatment plant', 'treatment plant' or 'other'.
	Specify Discharge Q1 or Q2	Select 'User Specified' if the discharge volume is available from the applicatant, or if not, select 'Calculated' from the list. If using the latter, input Number of Persons, Water Use (litres/person/activity/day using Flows and Loads 4) and Percolation Rate, Vp (to be provided by applicant from Percolation Test to British Standard BS 6297 2007 + A1 2008). If you wish to proceed with the assessment whilst waiting for the Percolation Test to be done, assume $Vp = 50$ .
	Area of Drainage Field and Hydraulic Loading	Use the pull down to select 'Calculated' or 'Specified'. If the applicant has a design for the drainage field and can specify the area (Map provided by applicant together with NGR in Section 2c), select Specified and entervalue into 'Enter Area of Drainage Field'. To calculate the area, Vp and Number of Persons will be required from previous step.
Attenuation Unsatzone	Drainage Layer	
	Infiltration Rate	This is carried through automatically from Infiltration System worksheet.
	Thickness of drainage field	May be indicated by applicant. For a British Standard, use a value of 0.3 m.
	Water filled porosity	Suggest a value of between 20 and 30%.
	Bulk density of drainage material	Suggest a value of 1.75 g/cm <sup>3</sup> .
	Option to Select Degradation (pull dow n)	Select 'Degradation Occurs – Solid and Dissolved Phases'. Although for an initial conservative assessment suggest select 'No degradation' option.
	Half Life for Degradation of Substance (days)	Suggested half life of 1 to 2 years for ammonium.
	Soil-Water Partition Coefficient	For Ammoniacal Nitrogen, suggest value between 0.5 and 2 l/kg.
	Unsaturated Zone	
	Thickness of unsaturated zone below drainage field	Enter thickness between drainage field base and water table (Figure 1).
	Water filled porosity	Enter using local know ledge or literature values (examples: sandstone 0.15 [15%]; chalk 0.02 [2%]).
	Bulk density of Unsaturated Zone	Enter literature values (suggest value of 1.75 g/cm³).
	Option to Select Degradation (pull dow n)	Select 'Degradation Occurs – Solid and Dissolved Phases'. Although for an initial conservative assessment suggest select 'No degradation' option.
	Half Life for	Suggest half life of 2 to 5 years for ammonium.

Degradation of Substance (days)

Fraction of Rapid Flow through unsaturated zone

For most sites assume no by-pass.

Soil-Water Partition Coefficient For Ammoniacal Nitrogen, suggest value between 0.5 and 2 l/kg.

Dilution

Concentration at base of

unsaturated zone

This is brought through automatically from Attenuation\_unsatzone worksheet.

Length of drainage field in direction of groundwater flow (L) Specify from applicant's design if this is provided.

Saturated Aquifer Thickness (m)

Assumed based on know ledge of aquifer (for example, 25-30 m for chalk; 5-10 m for sandstone).

Hydraulic Conductivity of Aquifer Enter using local know ledge or literature values (examples: sandstone 0.5-4 m/d; chalk 1 to 30 m/d) (see also Aquifer Properties Manual.

Hydraulic gradient of water table Measure in GIS if Area groundwater contour shape files are available, or assume 0.005.

Width of drainage field perpendicular to groundwater flow Check w hether w \* L is equivalent to the area of the drainage field, although they may differ if the drainage field is at an angle to the flow direction.

(w)
Background
concentration of
substance in
groundwater

For Ammoniacal Nitrogen assume 0, unless there is a known sewage discharge up-gradient and you have confidence in anticipated background concentration. For other substances, refer to Regional GQMN data if appropriate.

Mixing zone thickness

Suggest use option to calculate mixing zone thickness.

Attenuation\_satzone

Concentration in groundwater at base of unsaturated zone

This is brought through automatically from Dilution worksheet.

Option to Select Degradation Select 'Degradation Occurs - Solid and Dissolved Phases'.

Half Life of Substance

Assume 1850 days (5 years) for Ammoniacal Nitrogen. See also Small Sew age Discharges (SSDs) SPZ1 risk assessment approach.

Bulk Density of Saturated Aquifer Materials

Enter using local knowledge or literature values (examples: 1.65 g/cm³ for Chalk).

Effective Porosity of Saturated Zone

Enter using local knowledge or literature values (examples: 0.02 for Chalk; 0.10 for Sherwood Sandstone).

Option to Select Time

Select 'Steady State'.

Soil-Water Partition Coefficient (Cell L9) For Ammoniacal Nitrogen, suggest value between 0.5 and 2 l/kg.

Define Dispersivity For intergranular aquiters select Xu & Eckstein, for fissured aquiters select 10% option.

Distance to Compliance Point This factor is significant in its effect on compliance. If site is inside SPZ1, for sensitivity select 50 m initially to do assessment, then enter the actual distance measured in GIS to the vulnerable receptor (the PWS source, spring or watercourse) based on location provided by applicant (Map provided by applicant

together with NGR in Section 2c of Permit application form,, combined with GIS measurement to nearest receptor).

Concentration at Compliance Point (output of assessment) This will provide the calculated concentration at the compliance point and state whether the application meets or exceeds the threshold.

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