

Fokker F27 Mark 500, G-CEXA, 6 May 1997

AAIB Bulletin No: 12/1997

Ref: EW/C97/5/1 Category: 1.1

Aircraft Type and Registration:	Fokker F27 Mark 500, G-CEXA
No & Type of Engines:	2 Rolls Royce Dart 532-7 turboprop engines
Year of Manufacture:	1974
Date & Time (UTC):	6 May 1997 at 0711 hrs
Location:	Runway 27, Jersey Airport
Type of Flight:	Public Transport (Freight)
Persons on Board:	Crew - 2 - Passengers - None
Injuries:	Crew - None - Passengers - N/A
Nature of Damage:	Substantial to nose landing gear, fuselage, both engines and propellers
Commander's Licence:	Airline Transport Pilot's Licence
Commander's Age:	63 years
Commander's Flying Experience:	15,486 hours (of which 5,168 were on type) Last 90 days - 71 hours Last 28 days - 17 hours
First officer's Age:	24 years
First officer's Flying Experience:	502 hours (of which 10 hours were on type) Last 90 days - 10 hours Last 28 days - 10 hours

Synopsis

The aircraft was operating on a scheduled freight service carrying newspapers from Bournemouth to Jersey. The commander, a training captain working part time for the company, was training a new first officer on his first line-training sector. The flight, which was delayed due to poor weather

and strong cross winds at Jersey, departed nearly three hours behind schedule at 0638 hrs with the first officer as the handling pilot. He flew for most of the sector but the commander briefed that he would probably take control for the landing. The aircraft was radar vectored for an ILS approach to Runway 27 at Jersey where the weather had moderated to give a surface wind of 330°/24 to 34 kt with a visibility of 30 km and a cloud base of 1,600 feet. The first officer continued to fly the aircraft as it descended on the glide path with the commander taking control 4 seconds before touchdown. The aircraft landed heavily nose wheel first distorting the nose wheel assembly rearwards into the aircraft structure. The aircraft bounced, and after a second heavy impact, the main landing gear retracted allowing the fuselage to contact the runway. The aircraft slid several hundred metres along the runway before departing the paved surface coming to rest on the grass close to the airfield boundary. There was no fire and the crew vacated the aircraft without injury.

History of the flight

The first officer, who was relatively inexperienced and new to type, had just completed his initial line check. He had reached an acceptable standard and was considered ready for line training. He had been given extra base training because of an initial inability to appreciate flight path deviations and descent rates during the final approach and landing phase.

His first line training flight was rostered to be the early morning flight from Bournemouth to Jersey departing at 0345 hrs. He reported a little earlier than required in order to acquaint himself with the paperwork and produce an initial load sheet for the flight.

The commander, who worked for the operator on a part-time basis, reported for duty at 0245 hrs. Having checked that the first officer was in possession of all the necessary paperwork he checked the Jersey weather to find that it was raining and that the wind was at 90° to Runway 09/27 and outside the F27 crosswind limits of 29 kt on a dry runway and 15 kt when wet. The flight was therefore delayed pending an improvement in the conditions.

By 0620 hrs the rain had ceased and the wind had abated slightly to 340°/25 to 37 kt thus favouring Runway 27. The aircraft departed 'off chocks' at 0634 hrs and was airborne at 0644 hrs. On the suggestion of the commander the first officer was the handling pilot. The commander had briefed that there was a strong possibility that he would take control for the landing as the wind was close to the crosswind limits.

The aircraft departed from Bournemouth and routed direct to the reporting point ORTAC. After establishing in the cruise at FL 100 the crew were advised by ATC that they would be making an ILS approach to Runway 27 at Jersey. The commander set up the navigation aids for the route, briefed the first officer about the landing, and stated that he would let the first officer fly the aircraft until he, the commander, felt that the crosswind was becoming a problem. At this stage the first officer set his speed bug to 95 kt for the landing. When the first officer requested the descent checks the commander actioned them but did not employ the usual challenge and response technique.

At 0700 hrs the aircraft was cleared to 6,000 feet and was in the descent when the commander carried out the approach checks. These again were actioned individually by the commander alone. After clearance was obtained to descend to 3,000 feet the commander set up both ADFs and the ILS receiver on his side for the final approach and landing. He also requested the surface wind at Jersey which was given by ATC as 330° to 340° and 20 kt to 26 kt.

The Jersey approach controller vectored the aircraft initially onto a heading of 170°M. The commander noticed that the first officer had turned onto 160°M and restated the correct heading which the first officer then followed. The commander also set up the first officer's ILS receiver for the landing. The controller then instructed the crew to descend to 1500 feet on the QNH of 994 mb and turn right onto 245°M to intercept the localiser. Three minutes before landing the aircraft crossed the runway extended centreline on a heading of 220°M still in the turn onto 245°M. The commander advised the approach controller that the aircraft had flown through the localiser and was continuing the turn onto 300°. ATC suggested a heading of "315°OWN NAVIGATION REPORT ESTABLISHED". The commander selected the first stage of flap just prior to localiser capture and was instructed by the approach controller to call Jersey tower. One and a half minutes before landing the aircraft began the final descent and made a left turn onto the runway heading. The first officer called for the landing checks which the commander performed on his own, the only comments from the first officer being 'six greens' confirming that the landing gear was down and locked.

At 0710 hrs the tower controller transmitted "...CLEAR TO LAND RUNWAY 27 SURFACE WIND 330 DEGREES 27 KNOTS". The commander acknowledged the clearance and shortly after this exchange the aircraft's Ground Proximity Warning System (GPWS) 'GLIDE SLOPE' alert sounded. The commander then said "OH, IGNORE THAT FOR A MINUTE... JUST COCK YOUR NOSE UP A BIT TO STOP THE ROW... BECAUSE YOU'VE GOT THREE REDS" (indications from the runway Precision Approach Slope Indicators (PAPIs)). In total, six 'GLIDE SLOPE' warnings sounded before the warning ceased 30 seconds before touchdown.

Forty seconds before touchdown the commander, without prompting from the first officer, selected full flap (40°) whilst the first officer maintained an airspeed of 106 kt to 111 kt with an average descent rate of 650 ft/min. Five seconds before the landing the commander stated that he was taking control. This was acknowledged by the first officer. For the next three and a half seconds the rate of descent reduced and airspeed decayed to between 97 kt to 104 kt. In the final one and a half seconds before touchdown both airspeed and rate of descent increased. The aircraft struck the runway at a speed of 106.8 kt and a normal acceleration of +3.7g was recorded on the Digital Flight Data Recorder (DFDR). During this impact the Cockpit Voice Recorder (CVR) recorded the intermittent sound of the gear unsafe warning horn. The aircraft became airborne again for 2.6 seconds and airspeed decayed to 95 kt before it landed on the runway for a second time and registered a normal acceleration of +3.0g. At the second impact the gear unsafe warning horn was again activated and became continuous.

For the next 15 seconds the aircraft slid along the runway with the lower surface of the fuselage in contact with the paved surface. Sounds of a propeller striking the ground were recorded on the CVR. Another large vertical acceleration peak was recorded on the DFDR coincident with an increased audio level on the CVR as the aircraft departed the runway and slid for a further five seconds. It eventually came to rest on the grass area mid-field between the runway and the boundary fence. The commander and first officer vacated the aircraft uninjured. Fire service personnel who were on 'weather standby', witnessed the landing and were in attendance within thirty seconds. The airfield which was closed after the accident was reopened 5:45 hours later at 1256 hrs.

The pilot of a Trislander aircraft, who landed on Runway 27 some 16 minutes before the F27, stated that for his approach there had been only light turbulence with no appreciable fluctuations in airspeed. Furthermore the DFDR from the F27 gave no evidence of variations in the recorded airspeed during the landing.

Eye witnesses

Many people witnessed the later stages of the approach and the landing. One eye witness, a policeman situated in police accommodation overlooking the runway, stated that he could clearly see the landing gear was down before touchdown. He reported that 'at a point where he would have expected the nose of the aircraft to rise he saw it maintain its nose down attitude and moreover appeared to become steeper in attitude to a point where it would make a nose wheel first landing'. A second policeman stated that 'the nose wheel hit runway, he heard a bang, the aircraft settled onto its main wheels and then bounced some 10 to 15 feet in height before settling onto the runway nose wheel first'.

A fireman positioned in the Fire Station reported that 'the aircraft's descent seemed to become abnormally steep before it impacted heavily nose wheel first, bouncing back onto the main landing gear then onto the nose gear again. As the nose wheel lifted for a second time he heard a bang and saw the nose wheel flapping from side to side.'

Weather

The UK low level forecast issued by the Meteorological Office at 2130 hrs on 5 May 1997 and valid between 0000 hrs and 0600 hrs on 6 May 1997 showed an occluded front lying from the Cherbourg peninsular to the Hook of Holland moving south-east at 20 kt. This was giving rise to a visibility of generally 12 km in nil weather with an occasional reduction to 7 km in rain and isolated thunderstorms and heavy rain with a reduction in visibility to 3,000 metres near the front. It also forecast cloud on the hills, moderate icing and moderate turbulence in cloud and moderate with isolated severe turbulence below 6,000 feet north of the front. In the area behind the front the forecast showed an improvement to 20 km visibility reducing to 8 km in isolated rain showers and 3,000 metres in isolated thunderstorms. The outlook to 1200 hrs was for showers developing more widely over land, otherwise little change.

This forecast corresponded to the actual conditions recorded at Jersey during the early hours of the morning of the accident. The 0520 hrs observation gave a visibility of 6 km in rain with broken cloud at 700 feet and broken cloud at 1,100 feet with a surface wind of 350°/26 to 40 kt. At the time of the accident the weather had moderated to a visibility of 30 km, nil weather, few clouds at 800 feet, broken cloud at 1,600 feet and a surface wind of 330°/24 to 34 kt.

Crew Resource Management (CRM)

The first officer reported for duty earlier than required on the morning of the accident in order to familiarise himself with the pre-flight preparation. One of his duties was to produce an aircraft load sheet reflecting the expected load of 4,500 kg of newspapers. The commander arrived at 0245 hrs, one hour before the scheduled time of departure, and checked the first officer's preparation and the weather conditions. At approximately 0305 hrs both the commander and first officer left Operations to go to the aircraft. This was a little earlier than normal in order to give the first officer sufficient time to complete the internal aircraft pre-flight checks. With the checks complete the commander re-checked the Jersey weather and, discovering that the wind was still outside the cross-wind limits, returned with the first officer to operations to await an improvement.

It could not be determined exactly what the activities of the two crew members were during the delay. The commander did not however have much contact with the first officer. He did not discuss in any detail the forthcoming sector, which was to be the first officer's first line training flight, nor did he check the calculations and presentation of the load sheet that had been prepared earlier. The load sheet was in fact completed in error with some fundamental mistakes being made on the

calculation of the aircraft's centre of gravity. The commander had signed the load sheet as being correct anyway.

The CVR recording provided an insight into how the flight was conducted. It was the operator's common practice for a new first officer undergoing training to operate as the non-handling pilot for at least the first two sectors in order for them to settle into normal first officer duties. Only after this settling in period do they act as the handling pilot. The commander had decided that on this occasion that the first officer would handle the aircraft.

The commander was an experienced F27 pilot who had flown the sector to Jersey on many occasions. The procedure to him appeared routine to the point of being mundane. The first officer was new to type, inexperienced yet keen to please and perform well. The cross-cockpit gradient was therefore extremely steep.

Evidence from the CVR indicates that the commander did not allow the first officer, as the handling pilot, to truly 'operate' the aircraft. He did not coax the first officer by suggesting, in advance, the methods for good flight deck and time management. He pre-empted all the decision making and actioned all the checklist items unprompted and in isolation. Instead of allowing the first officer to brief for the approach the commander rushed through his own brief, paying scant regard to the first officer's understanding. On several occasions the first officer tried to enter into normal conversation with the commander. His attempts at this however were met with uncharacteristic dismissal.

The commander had carried out CAA approved CRM training in November 1993 and a refresher in June 1996. The first officer was to settle into the position before undergoing CRM training.

The commander's schedule

The commander's activities on the seven days preceding the accident were examined in detail. On Tuesday 29 May 1997 he had operated a flight from Coventry going off duty at 0400 hrs the next morning. The remainder of that day and the next three days were free from duty.

At 1200 hrs on Sunday 4 May he travelled by car from his home in Coventry to Bournemouth in order to position for a forthcoming flight on the Monday. He spent Sunday afternoon with friends near Bournemouth before 'checking in' at a local hotel. He arrived at the hotel at 2100 hrs and was asleep by 2245 hrs. On Monday 5 May 1997 he awoke at 0200 hrs to operate the 0345 hrs flight from Bournemouth to Jersey and return. He reported 'on duty' at 0245 hrs and went off duty after the flight at 1205 hrs. That afternoon he met with friends to play squash and enjoy an evening supper. At 1800 hrs he took two extra strong non-prescription pain killers to combat toothache. He returned to his hotel at 2015 hrs and took a further two extra strong pain killers. He went to bed at 2045 hrs but did not sleep until 2330 hrs due to aggravation from the sore tooth. At 0215 hrs on the day of the accident he awoke to report for duty by 0245 hrs.

Crew records

The commander joined the operator in April 1994 having flown the F27 with a previous operator, holding the positions of Base Manager and line pilot. The Flight Operations Manager of his new operator was satisfied that the training given by the previous operator was acceptable and a certificate to that effect was signed in April 1994. The Operations Manual included the commander's name as an authorised Line Training Captain (F27). The commander terminated his employment

with the operator with effect from 31 January 1997 but agreed to work, freelance on a part-time basis, flying on Mondays and Tuesdays only. The Operations Manual did not reflect his freelance status at the time of the accident.

Training

The entry in the Operations Manual, Section 3 paragraph 6 titled 'Line Training' states that:

'The purpose of Line Training is twofold. Firstly it will enable the new converted pilot to settle down to his duties on the new type, in the company of an experienced and qualified pilot specially designated for the purpose and to turn to him for advice if necessary. Secondly, it will enable the training staff to assess and verify the adequacy of the conversion training and to ensure that proper operating standards are achieved at the outset, in the course of normal and varied operations.'

It also states that:

Co-pilots should have 'a minimum of 20 sectors/30 hours under supervision of a Line Training Captain. At least 8 sectors should be flown by the Co-pilot as P1 under supervision. A covering Co-pilot will be carried until released by the Line Training Captain.'

The commander stated that he had not found out about the First Officer's early difficulties in appreciating flight path deviations and descent rates during the approach and landing. He had not sought the First Officer's training records prior to the flight. Although a covering co-pilot had been rostered for the flight, he had been re-tasked to fly on an air test.

Glide slope warning

The F27 Non-Normal Check list includes an entry titled 'GLIDE SLOPE WARNING'. The associated procedure states: 'Adjust flight path to regain Glide slope. Note: In certain circumstances the warning provided by the GPWS may be very late, so recovery action should be both prompt and positive'.

The Operations Manual (Section 16.1.1) states in the section 'FOKKER F27 TRAINING PROCEDURES' - GROUND PROXIMITY WARNING SYSTEM', that 'Activation of Mode 5 - Excessive deviation below the ILS glide slope - requires immediate action to regain the glide slope or a go-around initiated.' Evidence from the CVR showed that the reaction of the commander to the glide slope warning during the later stages of the approach appeared to be casual and less than helpful to his trainee.

Operations conclusions

In summary, although the commander had been rostered for the required periods of rest before the accident he had in fact slept for only had 8 hours, due in part to a toothache, in the 48 hours preceding the accident. It could not be determined whether the non-prescription pain killers had any detrimental effect on his performance. Nevertheless these factors probably combined to degrade his performance and reaction times on the day of the accident.

Engineering investigation

Ground marks

The first set of ground marks were on the runway centreline, some 200 metres from the Runway 27 threshold and corresponded to the impact of the aircraft's nosewheel. The second set were close to the centreline, some 125 metres further along the runway. These marks matched the damage to the aircraft's nose landing gear leg. From a point 90 metres further along the runway the marks became continuous, showing that the fuselage was now in contact with the runway. At this point evidence showed that the right-hand propeller was cutting into the runway surface. Further runway marks showed that, as the aircraft continued, it veered to the right side of the runway and slithered onto the level grass surface. The aircraft came to rest about 90 metres from the edge of the runway, slewed through some 80°. Between the first set of impact marks and coming to rest the aircraft had travelled approximately 690 metres.

Structural damage

The aircraft had been severely damaged both by its two impacts with the ground and the subsequent slide along the runway and over the grass. Furthermore the vertical speed at impact had significantly exceeded the levels required to be demonstrated for type certification.

The damage to the propellers matched the groundmarks, showing the propeller blades to be in fine pitch during the ground slide, and the damage to the skins and frames of the lower fuselage matched the marks on the runway and grass.

The nose area was extensively disrupted in the two impacts with structural damage extending through the forward pressure bulkhead up to the flight deck. The tyre on the nosewheel had burst showing 'overload' characteristics typical of a high energy arrival and the lugs carrying the lower end of the nose leg damper had also failed under the high vertical loads on the nosewheel. The nose leg had then folded rearwards with its airframe attachments, fracturing the lower attachment of the retraction ram. This ram had subsequently retracted along with the main landing gear legs, leaving the nose leg with its down lock engaged.

Landing gear system examination

After the accident it was found that both main landing gear legs were undamaged and had retracted and were fully engaged in their 'up locks'. During the recovery operation, with the airframe partly supported by a crane, the landing gear control handle could not be moved from the intermediate position in which it was found and so the main landing gear legs were lowered using the Emergency landing gear control handle. The legs lowered easily and were locked down.

The three Fokker F-27 landing gear legs are retracted and extended pneumatically, using a 1,000 psi pneumatics supply and this same supply powers the up locks. Pressure to the pneumatic rams is controlled by a selector valve, moved by the landing gear control handle by a simple 'Teleflex' cable, routed under the cockpit floor. The landing gear control handle is mounted behind the instrument panel and is prevented from moving upwards, when the aircraft is on the ground, by a solenoid which moves a locking pawl. This locking pawl physically blocks any UP movement of the landing gear control handle while the solenoid is in its 'relaxed' position; only when the solenoid is energised by movement of the ground-flight switch (on the left-hand main landing gear leg) may the landing gear control handle be moved upwards. There is no actual 'detent' at either the UP or DOWN positions but a small spring-and-slider assembly, attached to the handle, acts in an 'over-centre' manner to retain the handle in its selected position.

The landing gear control system was examined in detail. The system was intact, appeared correctly rigged and the handle itself was seized in a position approximately 75% to the fully UP position. This handle position corresponded to the position of the input lever on the pneumatic selector valve. The Teleflex cable between the two units was still intact, with the outer sheath complete. The disruption of the lower fuselage had introduced extra bends into the cable and one of these bends, where the cable passed through a horizontal member at the level of the flight deck floor, was of sufficiently small radius to jam the cable core.

The landing gear warning system activates a warning horn on the flight deck if any of the landing gear legs are not fully locked down and either the flaps are extended beyond 25° or at least one of the throttle levers is at a position corresponding to less than 10,500 RPM. With the flaps still at their fully extended (40°) position electrical power was applied and the warning system tested. The horn sounded correctly both with closure of the test switch and either of the main landing gear down lock switches.

Engineering conclusions

The process by which the landing gear was able to retract during the landing sequence was examined in detail. The flight crew stated that they did not move, and had no reason to move, the landing gear lever after they had confirmed "six greens" on the final approach.

As all three gear retraction rams had acted together they must have been in receipt of a common signal from the selector valve. This was confirmed by the position of the selector valve input lever which corresponded to the position of the landing gear handle on the flight deck. During the structural repair of the aircraft, it was confirmed that the Teleflex cable linking the landing gear handle and the landing gear selector valve was intact but had become jammed due to airframe distortion just below the level of the flight deck floor. There was no distortion or damage in the area of the selector valve and the UP signal was, therefore, as a result of movement of the landing gear handle, before the Teleflex cable was distorted and jammed.

The CVR showed that the steady tone of the landing gear warning horn commenced 0.5 seconds after the second impact. Tests on two different F27 aircraft showed that, with flaps deployed or throttles at idle, the horn would generally sound some 0.5 seconds after a sharp movement of the landing gear handle to the 'UP' position. The sounding of the landing gear warning horn would therefore have been consistent with movement of the handle in the second impact.

It is therefore possible that the landing gear handle had rotated upwards within its bracket during the second impact, by contact with the bottom of its slot within the instrument panel. There was evidence that the instrument panel, which is mounted on anti-vibration mountings, had moved upwards by some 10 mm at some point during the impact and it is possible that this movement, combined with deflection of the bracket from deformation of the forward pressure bulkhead, had moved the handle upwards against the damping friction of the Teleflex cable and the 'over-centre' spring.

Duplicate main landing gear indicators (green lights)

The normal method of determining whether the landing is down and locked, in the event of a landing gear malfunction, is visual inspection of the main landing gear legs from within the cabin. Access to the cabin windows for a visual inspection, however, is sometimes not possible due to bulk loads carried within the compartment. The crew are therefore provided with an independent means

of ensuring that the legs were down and locked in the form of a second set of green 'down and locked' lights positioned on the flight deck.

It was noted during the investigation that the second indicating system was not truly independent as both systems were actuated by the same set of micro switches. However, a review of FAR Part 25, BCAR Section D and JAR 25 indicates that the provision of an independent indication system, provided in most large aeroplanes, is not a part of these airworthiness codes.

Flight Recorders

Digital Flight Data Recorder (DFDR)

The aircraft was fitted with a DFDR which recorded, amongst other parameters, the aircraft's height, magnetic heading, IAS, flap position and normal acceleration. Pertinent data from these parameters is included in the history of flight section above.

DFDR installation

The DFDR was of a type that had built-in transducers for airspeed and barometric altitude. To use these transducers the DFDR would have been pneumatically coupled to the pitot/static system of the aircraft. The position of these two parameters in the recorded data stream and the algorithms required to convert the raw data back to engineering units are well documented in the DFDR Maintenance Manual. However, this aircraft had been fitted with two separate transducers as part of a draft modification introduced by the organisation that was responsible for the maintenance of the flight data recording system. As the new transducers were of a different type and were electrically connected to the DFDR, the airspeed and altitude values from them had different conversion algorithms and were recorded in different positions in the DFDR data stream. Part of the introduction of the draft modification required the amendment of the Aircraft Maintenance Manual (AMM) to reflect the changes in data stream position and parameter conversion. At the time of the accident the AMM had been amended to reflect the new data positions but the conversions, in the form of acceptable data ranges, were incorrect for the transducers fitted.

The draft modification was embodied on the accident aircraft early in 1996. The installation was required to be checked functionally and calibrated to the requirements of the amended AMM and the DFDR was to be removed for a mandatory readout by a separate company. Both of these requirements were stamped as having been completed by the maintenance personnel responsible. The readout company performed the DFDR replay in April 1996 but treated the DFDR as one which was connected pneumatically, not electrically. The altitude and airspeed recorded parameter values were thus taken from the DFDR internal transducers which, although functioning, were not connected to the aircraft's pitot/static system. The company then alerted the maintenance organisation to the fact that airspeed was not being recorded correctly in that no variation of the replayed trace from zero knots was observed. Variation in barometric altitude was seen but, because the DFDR was mounted in a pressurised part of the aircraft, this parameter was effectively recording the cabin altitude and not the altitude of the aircraft.

Upon receipt of the notification, the maintenance organisation discovered an error in the draft modification wiring diagram for the new transducers. This error was interpreted to be the reason that the airspeed parameter was inoperative. The error was corrected and the modification raised to issue 1. The embodiment of the modification on the aircraft was raised in line.

No further relevant work was conducted on the DFDR installation until December 1996 when the next mandatory DFDR readout and calibration was scheduled. The calibration of the DFDR installation was conducted against the amended AMM containing the wrong airspeed and altitude conversion ranges and the worksheet was stamped as complete by maintenance personnel.

The FDR readout was conducted by the same organisation that carried out the previous one. Although there was no evidence found at either the maintenance or readout organisation to advise that the DFDR airspeed and altitude transducers were electrically connected, the DFDR was read out using the correct data stream parameter positions and no anomalies were observed. The readout consisted of traces of a flight with all parameters plotted in raw data units. It was, therefore, impossible to assess visually whether the data would have fallen within the limits of 'reasonableness', ie low airspeed when on the ground etc. A snapshot of data during the cruise phase of the flight was converted to engineering units, but, without knowledge of the flight details such as cruise airspeed, altitude and heading, no degree of certainty that the correct conversion algorithms were used could have been inferred.

In an attempt to establish the algorithms required to convert the airspeed and altitude raw DFDR data to engineering units, AAIB requested a calibration check of airspeed and altitude recording on the accident aircraft. This was carried out and a successful conversion for airspeed was derived. However, the calibration of the recording of altitude showed erroneous values due to damage sustained during the accident. A calibration of altitude was successfully performed on an identical, undamaged aircraft, when it became available, which provided a generic conversion algorithm for the type but was not specific to the accident aircraft. A final calibration of the accident aircraft was not possible until significant repair action had been implemented. This caused a delay of many weeks before absolute validation of the data recorded by the DFDR during the accident was possible. Since the accident the maintenance organisation has corrected the errors in the calibration ranges of the airspeed and altitude set out in the AMM and has included provision for recording parameter values observed during the calibration of the DFDR installation.

Cockpit Voice Recorder (CVR)

The aircraft was fitted with a 30 minute continuous loop tape CVR. As the commander gave his landing briefing there was evidence of loud audio interference on the two crew channels for a period of five seconds. The level of the interference was slightly higher than that of the audio level of crew conversation and rendered the crew speech partially unintelligible. The interference occurred on two further occasions on the CVR recording but only on the commander's audio channel and when he was not speaking. Neither crew member was aware of the interference being caused. The crew are provided with a company mobile telephone which is stored on the flightdeck. This phone, however, was switched off and the source of the interference was subsequently confirmed to be from the commander's own personal mobile telephone which was active and located on the flightdeck.

As mobile cellular telephones move from one cell to another they transmit an identifying code to the new cell. This occurs even if the telephone is not being used to make a call. The CAA have already identified this problem and issued an Aeronautical Information Circular (AIC 96/1993) emphasising that the use of cellular telephones in aircraft even in the 'standby mode' is prohibited by the Air Navigation (No 2) Order.

Recording systems discussion

There are several specifications concerning the use of flight recording systems. The requirements and the equipment specifications are currently covered by the Air Navigation (No 2) Order and CAA Specifications 10 and 10A respectively. However, as the trend to European harmonisation continues, these will be superseded by JAR OPS and Eurocae ED-55. It should be noted that ED-55 is already in operation for the certification of new designs and installations. The requirements governing maintenance practices are contained within JAR 145 but there is no requirement for organisations that conduct mandatory readouts as a part of scheduled maintenance activity to hold JAR 145 approval for the task. In order to address the ability of readout organisations to assess recorded data adequately as part of a scheduled mandatory readout and to allow the regulatory authority to ensure an adequate assessment it is recommended that:

Recommendation 97-60

The CAA should require that organisations which conduct scheduled mandatory readouts of digital flight data recorders are approved to JAR 145.

Recommendation 97-61

The CAA should require that an aircraft operator maintains, for each recorder installation type, a data frame layout document which contains; details of all parameters recorded, the layout of the recorded data and the algorithms required to convert that data to engineering units. The layout of the document should be of a format standard to be stipulated by the CAA.

Recommendation 97-62

The CAA should require that, prior to a scheduled mandatory flight data recorder readout being conducted, the aircraft operator shall ensure that the facility conducting the readout is provided with a copy of the data frame layout document applicable to the installation to be assessed.

Recommendation 97-63

The CAA should require that an organisation conducting scheduled mandatory readouts from a digital flight data recorder has procedures in place to ensure that all information, within a data frame layout document, is correctly interpreted, used for a scheduled mandatory readout of the relevant recording installation and that any assessment is conducted only on data that has been converted to engineering units. Furthermore any report issued by the organisation shall reference, both by document number and issue status, the data frame layout document against which the readout was performed.